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DYGABCD - A Program for Calculating Linear A, B, C, and D Matrices From a Nonlinear Dynamic Engine Simulation

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DYGABCD - A PROGRAM FOR CALCULATING LINEAR A, B, C, AND D MATRICES FROM A NONLINEAR DYNAMIC ENGINE SIMULATION

by Lucille C. Geyser

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SUMMARY

A digital computer program, DYGABCD, has been developed that will generate linearized, dynamic models of simulated turbofan and turbojet engines. DYGABCD is based on an earlier computer program, DYNGEN, that is capable of calculating simulated nonlinear steady-state and transient performance of one- and two-spool turbojet engines or two- and three-spool turbofan engines.

Most control design techniques require linear system descriptions. For multiple-input/multiple-output systems such as turbine engines, state space matrix descriptions of the system are often desirable. DYGABCD computes the state space matrices, commonly referred to as the A, B, C, and D matrices, required for a linear system description. The report discusses the analytical approach and provides a users manual, FORTRAN listings, and a sample case. NASA TN D-7901, describing DYNGEN, is a necessary adjunct to this report.

INTRODUCTION

Digital computers are more frequently being used to accurately simulate the steady-state and transient performance characteristics of turbojet and turbofan engines. These simulations are capable of modeling these engines over the complete range of power settings and flight conditions. DYNGEN (ref. 1) is one such engine simulation that is generalized to permit the user to model many different engine configurations. It is based on the generalized steady-state engine modeling codes GENENG (ref. 2) and GENENG II (ref. 3). These codes are based on a technique called SMOTE (refs. 4 and 5).

To accomplish the modeling accuracy being demonstrated by DYNGEN and other digital computer engine simulation codes, nonlinear steady-state and transient physical relationships must be included. Most of the analytical design approaches used by control designers, however, require linear descriptions of the steady-state and transient characteristics of the engine. Linear approximations to nonlinear systems can be obtained at a particular operating point (a particular equilibrium condition of power setting and flight condition) for small excursions about that particular point.

For a system as complex as an engine, this linear system description usually consists of a multitude of interdependent linear algebraic and differential equations that can be written in a compact form by using matrix notation. A widely accepted linear dynamic system representation (ref. 6) uses a system matrix A, a control matrix B, an output matrix C, and a feed-forward matrix D. To describe an engine on a linearized basis over its complete operating envelope, however, a whole family of suitably selected linear approximations would be required.

This report, then, describes DYGABCD, a digital computer program that calculates the A, B, C, and D matrices for any turbofan or turbojet engine that is capable of being simulated with the DYNGEN program. DYGABCD can be used (1) exactly as DYNGEN to generate engine steady-state and transient performance characteristics; or (2) to generate the linear model A, B, C, and D matrices. The method of calculation employed in DYGABCD to generate these matrices can easily be used in any transient simulation that uses a backward difference integration technique (ref. 2).

The report first presents (1) the theoretical or analytical bases for linear model approximations to nonlinear systems, (2) a definition of the compact matrix formulation, and (3) a derivation of the equations necessary for determining matrix element values from the transient simulation. Next presented is a users guide for DYGABCD, including complete descriptions of those subroutines that have computational techniques different from DYNGEN. The FORTRAN symbols used are defined in appendix A, complete listings are shown in appendix B, and a sample case is presented in appendix C.

DYGABCD is written in FORTRAN IV and was used on the IBM 360/67 with the time-sharing system (TSS). The program should run equally well with the operating system (OS) on an IBM 360 or 370 series computer.

ANALYTICAL BACKGROUND

The simulation of a complex turbine engine process involves both linear and nonlinear algebraic and differential equations. Multiple equations of this type can generally be expressed in compact vector notation as

$$\dot{\mathbf{x}} = \mathbf{f}(\mathbf{x}, \mathbf{u}) \quad (1)$$

$$\mathbf{y} = \mathbf{g}(\mathbf{x}, \mathbf{u}) \quad (2)$$

where \mathbf{x} is a vector of the time-varying states of the engine, \mathbf{u} is a vector of the system control inputs to the engine, and \mathbf{y} is a vector of the engine's outputs. The vector $\dot{\mathbf{x}}$ represents the time rate of change of each of the engine's states. The following table lists some typical states, inputs, and outputs for a turbine engine system:

States	Inputs	Outputs
Temperatures	Fuel flows	Engine airflows
Pressures	Nozzle area	Thrust
Speeds	Bleeds	Specific fuel consumption
		Fan surge margin
		Compressor surge margin

Since most control design techniques require a linear description of the process to be controlled, a linear approximation to the nonlinear system needs to be developed. At a particular operating point, equations (1) and (2) can be represented by a Taylor series expansion about that point. If the vectors \mathbf{x} and \mathbf{u} are assumed to be single elements (i. e., scalars), equation (1) may be written as follows:

$$\dot{x}_0 = f(x_0, u_0) \quad (3)$$

The Taylor series expansion about the point (x_0, u_0) is

$$\begin{aligned}
\dot{\mathbf{x}} = & f(\mathbf{x}_0, \mathbf{u}_0) + \left. \frac{\partial f}{\partial \mathbf{x}} \right|_{\substack{\mathbf{x}=\mathbf{x}_0 \\ \mathbf{u}=\mathbf{u}_0}} (\mathbf{x} - \mathbf{x}_0) + \left. \frac{\partial f}{\partial \mathbf{u}} \right|_{\substack{\mathbf{x}=\mathbf{x}_0 \\ \mathbf{u}=\mathbf{u}_0}} (\mathbf{u} - \mathbf{u}_0) \\
& + \left. \frac{\partial^2 f}{\partial \mathbf{x}^2} \right|_{\substack{\mathbf{x}=\mathbf{x}_0 \\ \mathbf{u}=\mathbf{u}_0}} (\mathbf{x} - \mathbf{x}_0)^2 + \left. \frac{\partial^2 f}{\partial \mathbf{u}^2} \right|_{\substack{\mathbf{x}=\mathbf{x}_0 \\ \mathbf{u}=\mathbf{u}_0}} (\mathbf{u} - \mathbf{u}_0)^2 \\
& + \text{Other higher order terms}
\end{aligned} \tag{4}$$

If $(\mathbf{x} = \mathbf{x}_0, \mathbf{u} = \mathbf{u}_0)$ is a steady-state operating point, the system is in equilibrium and hence $\dot{\mathbf{x}}_0 = 0$. Thus, by using equations (1) and (3), equation (4) can be rewritten as

$$\begin{aligned}
\dot{\mathbf{x}} = & \left. \frac{\partial \dot{\mathbf{x}}}{\partial \mathbf{x}} \right|_{\text{op}} (\mathbf{x} - \mathbf{x}_0) + \left. \frac{\partial \dot{\mathbf{x}}}{\partial \mathbf{u}} \right|_{\text{op}} (\mathbf{u} - \mathbf{u}_0) \\
& + \left. \frac{\partial^2 \dot{\mathbf{x}}}{\partial \mathbf{x}^2} \right|_{\text{op}} (\mathbf{x} - \mathbf{x}_0)^2 + \left. \frac{\partial^2 \dot{\mathbf{x}}}{\partial \mathbf{u}^2} \right|_{\text{op}} (\mathbf{u} - \mathbf{u}_0)^2 \\
& + \text{Other higher order terms}
\end{aligned} \tag{5}$$

where op denotes operating point.

In a suitable neighborhood of the steady-state operating point $(\mathbf{x}_0, \mathbf{u}_0)$, the higher order terms of equation (4) are negligible, and equation (1) can be approximated by using only the first partial derivative terms. By letting $\Delta \mathbf{x} = \mathbf{x} - \mathbf{x}_0$, $\Delta \mathbf{u} = \mathbf{u} - \mathbf{u}_0$, and $\Delta \dot{\mathbf{x}} = \dot{\mathbf{x}} - \dot{\mathbf{x}}_0$, equation (5) becomes the linear equation

$$\Delta \dot{\mathbf{x}} = \left. \frac{\partial \dot{\mathbf{x}}}{\partial \mathbf{x}} \right|_{\text{op}} \Delta \mathbf{x} + \left. \frac{\partial \dot{\mathbf{x}}}{\partial \mathbf{u}} \right|_{\text{op}} \Delta \mathbf{u} \tag{6}$$

Equation (2) may be linearized in similar fashion for the output \mathbf{y} , resulting in

$$\Delta \mathbf{y} = \left. \frac{\partial \mathbf{y}}{\partial \mathbf{x}} \right|_{\text{op}} \Delta \mathbf{x} + \left. \frac{\partial \mathbf{y}}{\partial \mathbf{u}} \right|_{\text{op}} \Delta \mathbf{u} \tag{7}$$

Definitions of A, B, C, and D Matrices

An actual system with a multitude of states, inputs, and outputs, when linearized about an operating point, can be described by the following linear vector-matrix equations:

$$\Delta \dot{\mathbf{x}} = \mathbf{A} \Delta \mathbf{x} + \mathbf{B} \Delta \mathbf{u} \quad (8)$$

$$\Delta \mathbf{y} = \mathbf{C} \Delta \mathbf{x} + \mathbf{D} \Delta \mathbf{u} \quad (9)$$

where

- $\Delta \mathbf{x}$ n-dimensional vector of state deviations
- $\Delta \mathbf{u}$ c-dimensional vector of system control input deviations
- $\Delta \mathbf{y}$ o-dimensional vector of system output deviations
- \mathbf{A} n- by n-dimensional state system matrix
- \mathbf{B} n- by c-dimensional control input matrix
- \mathbf{C} o- by n-dimensional output matrix
- \mathbf{D} o- by c-dimensional feed-forward matrix
- n number of states
- c number of control inputs
- o number of outputs

The system matrix \mathbf{A} is a matrix of numbers that are the values of particular partial derivatives at a specific operating point. When the partial derivative notation of equations (6) and (7) is used, equations (10) to (13) show the elemental arrangements of the matrices \mathbf{A} , \mathbf{B} , \mathbf{C} , and \mathbf{D} .

$$A = \begin{bmatrix} \left. \frac{\partial \dot{x}_1}{\partial x_1} \right|_{op} & \left. \frac{\partial \dot{x}_1}{\partial x_2} \right|_{op} & \cdots & \left. \frac{\partial \dot{x}_1}{\partial x_n} \right|_{op} \\ \left. \frac{\partial \dot{x}_2}{\partial x_1} \right|_{op} & & & \\ \vdots & & & \\ \left. \frac{\partial \dot{x}_n}{\partial x_1} \right|_{op} & & & \end{bmatrix} \quad (10)$$

$$B = \begin{bmatrix} \left. \frac{\partial \dot{x}_1}{\partial u_1} \right|_{op} & \left. \frac{\partial \dot{x}_1}{\partial u_2} \right|_{op} & \cdots & \left. \frac{\partial \dot{x}_1}{\partial u_c} \right|_{op} \\ \left. \frac{\partial \dot{x}_2}{\partial u_1} \right|_{op} & & & \\ \vdots & & & \\ \left. \frac{\partial \dot{x}_n}{\partial u_1} \right|_{op} & & & \end{bmatrix} \quad (11)$$

$$C = \begin{bmatrix} \left. \frac{\partial y_1}{\partial x_1} \right|_{op} & \left. \frac{\partial y_1}{\partial x_2} \right|_{op} & \text{---} & \left. \frac{\partial y_1}{\partial x_n} \right|_{op} \\ \left. \frac{\partial y_2}{\partial x_1} \right|_{op} & & & \\ \vdots & & & \\ \left. \frac{\partial y_o}{\partial x_1} \right|_{op} & & & \end{bmatrix} \quad (12)$$

$$D = \begin{bmatrix} \left. \frac{\partial y_1}{\partial u_1} \right|_{op} & \left. \frac{\partial y_1}{\partial u_2} \right|_{op} & \text{---} & \left. \frac{\partial y_1}{\partial u_c} \right|_{op} \\ \left. \frac{\partial y_2}{\partial u_1} \right|_{op} & & & \\ \vdots & & & \\ \left. \frac{\partial y_o}{\partial u_1} \right|_{op} & & & \end{bmatrix} \quad (13)$$

Solutions for Full Forms of A, B, C, and D Matrices

It is our intent to take a DYNGEN digital computer simulation with its nonlinear dynamic equations and to develop a method for extracting from it the elements of the A, B, C, and D matrices at particular engine operating points.

Because of the backward finite-difference integration technique required by DYNGEN (SMOTE technique), it is necessary to calculate the inverse of the state system matrix A. To accomplish this, equation (8) can be rewritten as

$$\Delta x = A^{-1} \Delta \dot{x} - A^{-1} B \Delta u \quad (14)$$

To solve for A^{-1} , all system control input deviations Δu from the operating point are set to zero. Thus,

$$\Delta x = A^{-1} \Delta \dot{x} \quad (15)$$

Each element of A^{-1} is then approximated as

$$\left(A^{-1}\right)_{ij} \approx \frac{\Delta x_i}{\Delta \dot{x}_j} \quad (16)$$

where the state derivatives \dot{x}_j are perturbed, one at a time, as described in the following paragraph.

A steady-state vector of the states x is calculated. The state derivatives \dot{x} at this steady-state point are therefore zero. The first \dot{x} is set to some suitable value, $\Delta \dot{x}_1$, with the rest of the \dot{x} 's held to zero. A new state vector x^* is calculated. The difference between x^* and x is the vector Δx associated with this first $\Delta \dot{x}_1$. Each of the other \dot{x} 's is then set to some suitable value, $\Delta \dot{x}_j$, one at a time, with all other \dot{x} 's set to zero each time. A new vector x^* and a new vector Δx are calculated for each $\Delta \dot{x}_j$. A matrix of these Δx column vectors is formed. Each column vector is divided by the $\Delta \dot{x}_j$ that produced it, thereby forming the A^{-1} matrix referred to in equation (16). The A^{-1} matrix is then inverted to obtain the A matrix.

Solve for the control matrix B as follows: Under equilibrium conditions, $\dot{x} = 0$, equation (8) becomes

$$\Delta x = -A^{-1} B \Delta u \quad (17)$$

Each element of $-A^{-1}B$ is then approximated as

$$\left(-A^{-1}B\right)_{ij} \approx \frac{\Delta x_i}{\Delta u_j} \quad (18)$$

where the system control inputs u_j are perturbed, one at a time, as described in the following paragraph.

A steady-state vector of the states x is calculated. The first system control input u is changed by some suitable value Δu with the remainder of the u 's held to their steady-state values. A new state vector x^* is calculated. The difference between x^* and x is the vector Δx associated with this first Δu . Each of the other u 's is then perturbed by some suitable Δu , one at a time, with all other u 's remaining constant each time. A new vector x^* and a new vector Δx are calculated for each Δu . A matrix of these Δx column vectors is then formed. Each column vector is divided by the Δu that produced it, thereby forming the $-A^{-1}B$ matrix approximated by equation (18). This matrix is then premultiplied by $-A$ to obtain the B matrix.

To solve for the output matrix C , substitute the equation for Δx (eq. (14)) in the equation for Δy (eq. (9)), yielding

$$\Delta y = CA^{-1} \Delta \dot{x} - CA^{-1}B \Delta u + D \Delta u \quad (19)$$

When the system control inputs are held fixed, equation (19) becomes

$$\Delta y = CA^{-1} \Delta \dot{x} \quad (20)$$

Each element of CA^{-1} is then approximated as

$$\left(CA^{-1}\right)_{ij} \approx \frac{\Delta y_i}{\Delta \dot{x}_j} \quad (21)$$

where the state derivatives \dot{x}_j are perturbed one at a time, as was done in obtaining A^{-1} .

A steady-state output vector y is calculated. The state derivatives \dot{x} at this steady-state point are therefore zero. The first \dot{x} is set to some suitable value, $\Delta \dot{x}$, with the rest of the \dot{x} 's held to zero. A new output vector y^* is calculated. The difference between y^* and y is the vector Δy associated with this first $\Delta \dot{x}$. Each of the other \dot{x} 's is then set to some suitable value $\Delta \dot{x}$, one at a time, with all other \dot{x} 's

set to zero each time. A new vector y^* and a new vector Δy are calculated for each $\Delta \dot{x}$. A matrix of these Δy column vectors is then formed. Each column vector is divided by the $\Delta \dot{x}$ that produced it, thereby forming the CA^{-1} matrix approximated by equation (21). This matrix is then postmultiplied by A to obtain the C matrix.

Solving equation (9) for the feed-forward matrix D yields the approximation

$$D_{ij} \approx \frac{\Delta y_i}{\Delta u_j} - C \frac{\Delta x_i}{\Delta u_j} \quad (22)$$

where the system control inputs u_j are perturbed, one at a time, as described in the following paragraph.

Two steady-state vectors, x (the state vector) and y (the output vector), are calculated. The first system control input u is changed by some suitable value Δu , with the remainder of the u 's held to their steady-state value. A new state vector x^* is calculated. And a new output vector y^* is calculated. The difference between x^* and x is the vector Δx associated with this first Δu . The difference between y^* and y is the vector Δy associated with this first Δu . Each of the other u 's is then perturbed by some suitable value Δu , one at a time, with all other u 's remaining constant each time. A new vector x^* and a new vector Δx are calculated for each Δu . A new vector y^* and a new vector Δy are also calculated for each Δu . A matrix of the Δx column vectors is then formed, and each column vector is divided by the Δu that produced it. A matrix of the Δy column vectors is also formed, and each column vector is again divided by the Δu that produced it. By substituting these two matrices in equation (22), we can solve for D .

Solutions for Reduced Forms of A , B , C , and D Matrices

Once the complete linear model of the dynamic system is obtained, it may be desirable, for certain reasons, to reduce the complexity of the linear description. For example, the eigenvalues of the full system either may be beyond the frequency range of interest or may have little overall effect on the system dynamic characteristics. This reduction can be done by several methods.

By the method of Weinberg and Adams (ref. 7), equation (14) is rewritten in partitioned form as

$$\frac{\Delta \mathbf{x}_1}{\Delta \mathbf{x}_2} = \left[\begin{array}{c|c} \hat{\mathbf{A}}_{11} & \hat{\mathbf{A}}_{12} \\ \hline \hat{\mathbf{A}}_{21} & \hat{\mathbf{A}}_{22} \end{array} \right] \frac{\Delta \dot{\mathbf{x}}_1}{\Delta \dot{\mathbf{x}}_2} - \left[\begin{array}{c|c} \hat{\mathbf{A}}_{11} & \hat{\mathbf{A}}_{21} \\ \hline \hat{\mathbf{A}}_{12} & \hat{\mathbf{A}}_{22} \end{array} \right] \frac{\mathbf{B}_1}{\mathbf{B}_2} \Delta \mathbf{u} \quad (23)$$

where

- $\Delta \mathbf{x}_1$ r-dimensional part of state deviation vector
- $\Delta \mathbf{x}_2$ (n-r)-dimensioned part of state deviation vector
- $\Delta \mathbf{u}$ c-dimensional system control input deviation vector
- $\hat{\mathbf{A}}_{11}$ r- by r-dimensional upper left partition of \mathbf{A}^{-1} matrix
- $\hat{\mathbf{A}}_{12}$ r- by (n-r)-dimensioned upper right partition of \mathbf{A}^{-1} matrix
- $\hat{\mathbf{A}}_{21}$ (n-r)- by r-dimensional lower left partition of \mathbf{A}^{-1} matrix
- $\hat{\mathbf{A}}_{22}$ (n-r)- by (n-r)-dimensioned lower right partition of \mathbf{A}^{-1} matrix
- \mathbf{B}_1 r- by c-dimensional part of control input matrix
- \mathbf{B}_2 (n-r)- by c-dimensional part of control input matrix
- n total number of states
- r number of states desired
- c number of control inputs

Before calculating the partitioned $\hat{\mathbf{A}}$ matrix, permute the order of the $\Delta \mathbf{x}$'s and the corresponding $\Delta \dot{\mathbf{x}}$'s, so that the $\Delta \mathbf{x}$'s to be retained are all included in $\Delta \mathbf{x}_1$. Those remaining make up the elements of $\Delta \mathbf{x}_2$. The elements of $\Delta \mathbf{x}_2$ are assumed to be negligible in determining the system transient response. Hence, setting $\Delta \dot{\mathbf{x}}_2 = 0$ in equation (23) yields

$$\Delta \mathbf{x}_1 = \hat{\mathbf{A}}_{11} \Delta \dot{\mathbf{x}}_1 - \left(\hat{\mathbf{A}}_{11} \mathbf{B}_1 + \hat{\mathbf{A}}_{12} \mathbf{B}_2 \right) \Delta \mathbf{u} \quad (24)$$

Solving for $\Delta \dot{\mathbf{x}}_1$ gives

$$\Delta \dot{\mathbf{x}}_1 = \left(\hat{\mathbf{A}}_{11} \right)^{-1} \Delta \mathbf{x}_1 + \left(\hat{\mathbf{A}}_{11} \right)^{-1} \left(\hat{\mathbf{A}}_{11} \mathbf{B}_1 + \hat{\mathbf{A}}_{12} \mathbf{B}_2 \right) \Delta \mathbf{u} \quad (25)$$

or

$$\Delta \dot{\mathbf{x}}_1 = \mathbf{A}_R \Delta \mathbf{x}_1 + \mathbf{B}_R \Delta \mathbf{u} \quad (26)$$

where

$$A_R = \left(\hat{A}_{11} \right)^{-1} \quad (27)$$

and

$$B_R = \left(\hat{A}_{11} \right)^{-1} \left(\hat{A}_{11} B_1 + \hat{A}_{12} B_2 \right) \quad (28)$$

Note that it is necessary to compute only the upper left quadrant of the A^{-1} matrix (the r -by- r \hat{A}_{11}) and then to invert it to obtain A_R . The quantity $\hat{A}_{11} B_1 + \hat{A}_{12} B_2$ consists of the first r rows of the $A^{-1}B$ matrix from equation (18). Thus, only the first r rows of $-A^{-1}B$ need to be calculated. These rows are then premultiplied by $-A_R$ to obtain B_R .

In solving for a reduced C matrix and the D matrix used with the reduced A , B , and C matrices, there is no simple discarding of rows and columns. Starting with equation (23), if $\Delta \dot{x}_2$ is zero, then

$$\Delta x_2 = \hat{A}_{21} \Delta \dot{x}_1 - \left(\hat{A}_{21} B_1 + \hat{A}_{22} B_2 \right) \Delta u \quad (29)$$

Substituting equations (25) and (27) into equation (29) yields

$$\Delta x_2 = \hat{A}_{21} A_R \Delta x_1 + \left(\hat{A}_{21} A_R \hat{A}_{12} - \hat{A}_{22} \right) B_2 \Delta u \quad (30)$$

The partitioned form of equation (9) is

$$\Delta y = \left[C_1 \mid C_2 \right] \frac{\Delta x_1}{\Delta x_2} + D \Delta u \quad (31)$$

where

- Δy o -dimensioned output deviation vector
- Δx_1 r -dimensioned part of state deviation vector
- Δx_2 $(n-r)$ -dimensioned part of state deviation vector
- Δu c -dimensioned system control input deviation vector
- C_1 o - by r -dimensioned part of output matrix

C_2 o- by (n-r)-dimensioned part of output matrix

D o- by c-dimensioned feed-forward matrix

Equation (31) yields

$$\Delta y = C_1 \Delta x_1 + C_2 \Delta x_2 + D \Delta u \quad (32)$$

Using equation (30) to eliminate Δx_2 gives

$$\Delta y = C_1 \Delta x_1 + C_2 \hat{A}_{21} A_R \Delta x_1 + \left[C_2 \left(\hat{A}_{21} A_R \hat{A}_{12} - \hat{A}_{22} \right) B_2 + D \right] \Delta u \quad (33)$$

or

$$\Delta y = C_R \Delta x_1 + D_R \Delta u \quad (34)$$

where

$$C_R = C_1 + C_2 \hat{A}_{21} A_R \quad (35)$$

and

$$D_R = C_2 \left(\hat{A}_{21} A_R \hat{A}_{12} - \hat{A}_{22} \right) B_2 + D \quad (36)$$

USERS GUIDE

Changes to DYNGEN

The IBM 360/67 computer with TSS was chosen because of the storage size of the DYGABCD program. Certain changes have been made in the conversion of DYNGEN to DYGABCD for accuracy and speed of calculation. All real variables are now double precision. Each convergence loop now uses a convergence criterion of TOLALL multiplied by some constant, where TOLALL is input in the namelist data as before. Although the number of passes through some loops has been increased, the relationships among the loops have been kept constant, so that the accuracy of the convergence criteria can be increased. All BLOCK DATA subroutines are combined into one subroutine with the named common COMMON/COMDAT/COMD(5423). All program variables are com-

bined into one named common COMMON/COMALL/COM(1062). Within each subroutine, only those variables actually referenced are equivalenced to either COMD and/or COM, with one exception. In the main routine DYGABCD, each variable referenced anywhere in the program is equivalenced, so that all may be seen at a glance.

The DYGABCD program provides a maximum of 23 possible derivative variables for use in calculating the A and C matrices. The specific number of possible variables for any particular engine depends on the configuration of that engine. In calculating the B matrix, only two control variables are used. More parameters could be chosen. In calculating the C matrix, any variables calculated in the program, including the states and/or inputs, may be used. Variables that are both states and outputs are used in calculating the D matrix.

Minor changes have been made in the main routine DYGABCD and the subroutines ENGBAL and PUTIN (underlined in the listings) to accommodate the addition of the A, B, C, and D matrix calculations. An addition has been made to function DERIV to allow either the original calculations of DYNGEN or the calculations necessary for the A and/or C matrices to be performed. Since DISTRB was already a user-written subroutine in DYNGEN, the bulk of the A, B, C, and D matrix calculations are done in it.

Method

DYGABCD may be run exactly as DYNGEN if DYNGEN data are used. It may also be used to generate the A, B, C, and D matrices when it is used with a different set of data and a new subroutine DISTRB that is modified by the user. To use the A, B, C, and D matrix capability, the following tasks must be performed:

(1) A steady-state point is run and the resulting main fuel flow noted. This is the steady-state point about which the small perturbations (generating A, B, C, and D) will be made. When the A, B, C, and D matrices are generated, they will define a linear model that is applicable in the region of this steady-state point.

(2) A new run is made with the addition of one data card that includes the following parameters: MODE=2, WFB=(the steady-state value noted previously in task 1), ITRAN=1, and IAMTRX=1.

IAMTRX is a new variable that is input as 1 if the A, B, C, and D matrices are to be calculated. The default value is 0, which is the value when DYGABCD is used as DYNGEN. If IAMTRX is 1, the program runs a "pseudo-transient" to calculate the A and C matrices, a set of steady-state points to calculate the B matrix, and a set of steady-state points plus the C matrix to calculate the D matrix.

The term "pseudo-transient" is used to describe the following procedure: since ITRAN = 1 on the data card in task 2, the program runs in the transient mode. However, during every time step, when the time index, NSTEP, is increased by 1 in sub-

routine ENGINE, it is promptly decreased by 1 back to 0 by the next statement, if IAMTRX is 1. This "fool the program" pseudo-transient is necessary to calculate the A and C matrices in subroutine DISTRB. Just before calculating the B and D matrices, which depend on a set of steady-state points, DISTRB sets ITRAN to 0.

Changes to Subroutine DISTRB

DATA statements and program statements in subroutine DISTRB control the calculations of the A, B, C, and D matrices. DYGABCD provides a maximum of 23 possible time-varying state variables. These variables and their original order are as follows:

List number	Variable name
1	XNHP
2	XNIP
3	XNLP
4	P22
5	U22
6	P21
7	U21
8	P3
9	U3
10	P4
11	U4
12	P50
13	U50
14	P5
15	U5
16	P55
17	U55
18	P7
19	U7
20	P24
21	U24
22	P37
23	U37

The DATA statements and program statements include parameters that describe the particular case the user wishes to run.

INV	total number of states possible for particular engine being modeled, less than or equal to 23
INVRED	total number of states actually used in model (full or reduced), less than or equal to INV
IVARB	order in which states are to be done (If this is a reduced model, the states to be included are listed before those not included.)
INB	number of system control inputs desired, less than or equal to 5
BPER	percent (BPER=.02 means 2 percent) (The steady-state value of each input will be multiplied by this percent to form the Δu of each input in order to calculate the B and D matrices.)
INC	number of outputs desired, less than or equal to 50
NUCOM	list of equivalenced 'COM' numbers of outputs desired (All of the equivalences are in the main routine DYGABCD.)
PVRDOT	vector of percents (PVRDOT=.02 means 2 percent) in list number order (The steady-state value of each state will be multiplied by the percent associated with that state to form the $\Delta \dot{x}$ for that particular state in order to calculate the A and C matrices.)

There is one other necessary parameter that is set by a program statement - ICHOIC. If ICHOIC is 0, subroutine DISTRB calculates the A and C matrices by using the percentages of the states as set by the initial conditions of the PVRDOT's. If ICHOIC is set to 1, the percentages will be calculated and reset by the program to form an A^{-1} matrix with no zero columns or rows. A run with ICHOIC set to 1 should always be made first to find values for the PVRDOT's that do not result in an A^{-1} matrix containing any zero columns or rows. Obviously, an A^{-1} matrix that has zero columns or rows cannot be inverted.

Subroutine DISTRB is programmed to use inputs WFB (main fuel flow) and A8 (nozzle area). However, more and/or other inputs could be used. The number of inputs is limited to 5, but that limit could be changed by the user.

A line-by-line study of subroutine DISTRB should be made before attempting to make any runs other than the sample case. Subroutine DISTRB includes many comment cards that can be helpful. The listing starts on page 98.

Changes to Function DERIV

Function DERIV has been changed so that, if IAMTRX=1, a different set of statements is used. These statements set all derivatives to zero except for the particular

state being used. The derivative of that state is set to its steady-state value multiplied by the PVRDOT of that state. If IAMTRX=0, function DERIV behaves in the same manner as it did in DYNGEN.

Changes to Subroutine PUTIN

Subroutine PUTIN has been changed so that it will accept one more variable in the namelist DATAIN. This variable is IAMTRX, which is defaulted to zero if DYGABCD is to be used as DYNGEN and is set to 1 if DYGABCD is to be used to generate the A, B, C, and D matrices.

Changes to Subroutine ENGBAL

Two changes have been made to subroutine ENGBAL. One change resets the time index if IAMTRX=1. This has been explained in the section Method. The other change causes subroutines DISTRB and COINLT to be called during the steady-state calculations for the B and D matrices if IAMTRX=1. If IAMTRX=0, subroutine ENGBAL behaves in the same manner as it did in DYNGEN.

Changes to Main Routine DYGABCD

The routine DYGABCD sets the default value of IAMTRX to zero and initializes the parameter IDOT to zero. IDOT is used internally in subroutine DISTRB to keep a record on the states being used to generate the A and C matrices and later to keep a record on the inputs used in the calculations for the B and D matrices.

SAMPLE CASE

The sample case is a two-spool, two-stream engine simulation that has a maximum of 16 states. The system control inputs used were WFB (main fuel flow) and A8 (nozzle area). The outputs specified were SFC (specific fuel consumption), FG (gross thrust), and FN (net thrust).

A steady-state point was run and the main fuel flow was noted to be 2.75 lbm/sec. The data card for the A, B, C, and D matrix calculations was inserted. In subroutine DISTRB, the following parameters were set in DATA statements: the number of states possible for this engine (16), in INV; the number of states for a reduced model (9), in INVRED; the order of states, in IVARB; the number of system control inputs (2), in

INB; the percent delta of the inputs for the calculation of the B and D matrices (0.01), in BPER; the number of outputs (3), in INC; and the list of the equivalenced "COM" numbers of the outputs, in NUCOM. Subroutine statements were as follows: ICHOIC was set to 1 so that subroutine DISTRB would calculate the PVRDOT's. These PVRDOT's were all initialized to 0.02. The A, B, C, and D matrices generated were used to form a linear model.

Two transient runs were made using DYGABCD as DYNGEN. The first run had a 3-percent step change in main fuel flow, and the other had a 3-percent step change in nozzle area. The results from these two full-state, nonlinear transients were the time histories of the states, inputs, and outputs. These nonlinear results (squares on the graphs) were then used as the standard against which the results from the various runs using the linear model (circles on the graphs) were plotted.

Since one of the state eigenvalues was extremely large, 15th order (instead of 16th) was the largest order linear model that could be used to generate time responses. A run was made using the 15th-order (full) linear model with a 3-percent step change in main fuel flow. Another run was made using a second-order (reduced) linear model with the same step change. These two runs were then repeated with a 3-percent step change in nozzle area.

The responses of the states and outputs from these four linear cases are compared with the responses from the nonlinear cases in figures 1 to 19. The results of the full-order linear runs and the nonlinear runs for the two step inputs are shown in the upper quadrants of each figure. The agreement is very good. The reduced (low order) linear runs and the nonlinear runs for the two step inputs are shown in the lower quadrants of each figure. Here, there is disagreement, especially in the first 0.1 second of the transient, because those parameters that cause the high-frequency dynamics are missing.

The FORTRAN symbols used are defined in appendix A. The program is listed in appendix B. Sample case input data and output are listed in appendix C.

CONCLUSIONS

DYGABCD is a computer program that produces the A, B, C, and D matrices from a nonlinear, generalized, transient engine simulation. These matrices are used to generate a linear model. The results from the nonlinear simulations and the full-order linear simulations show good agreement. This method also permits reduced-order

models to be formed that produce varying degrees of agreement. The method of calculating these matrices could be applied to many other dynamic engine simulations.

Lewis Research Center,
National Aeronautics and Space Administration,
Cleveland, Ohio, April 21, 1978,
505-05.

APPENDIX A

FORTTRAN SYMBOLS

An asterisk denotes that the variable can be input.

A24	cross-sectional area at station 24, m^2 (ft^2)
A25	cross-sectional area at station 25, m^2 (ft^2)
* A28	area of fan duct nozzle throat, station 28, m^2 (ft^2)
A28SAV	saved area of fan duct nozzle throat, station 28, at design conditions, m^2 (ft^2)
A29	cross-sectional area at station 29, m^2 (ft^2)
A29SAV	saved cross-sectional area at station 29 at design conditions, m^2 (ft^2)
* A38	area of wing duct nozzle throat, station 38, m^2 (ft^2)
A39	cross-sectional area at station 39, m^2 (ft^2)
A55	cross-sectional area at station 55, m^2 (ft^2)
* A6	cross-sectional area of afterburner entrance, station 6, calculated from AM6, m^2 (ft^2)
A7	cross-sectional area at station 7, m^2 (ft^2)
* A8	area of main nozzle throat, station 8, (can be changed at off-design), m^2 (ft^2)
A8SAV	saved area of main nozzle throat, station 8, at design conditions, m^2 (ft^2)
A9	cross-sectional area at station 9, m^2 (ft^2)
A9SAV	saved cross-sectional area at station 9 at design conditions, m^2 (ft^2)
* AFTFAN	(logical) control for an aft-fan engine
* ALTP	altitude of aircraft, m (ft)

* AM Mach number of aircraft

* AM23 Input: design Mach number of ductburner
 entrance, station 23
 Output: Mach number at station 23

AM25 Mach number at station 25

AM28 Mach number at station 28

AM29 Mach number at station 29

AM38 Mach number at station 38

AM39 Mach number at station 39

* AM55 Input: design Mach number at low-pressure-
 turbine exit, station 55
 Output: Mach number at station 55

* AM6 Input: design Mach number at afterburner
 entrance, station 6
 Output: Mach number at station 6

AM6DSV saved Mach number at afterburner entrance at
 design conditions, station 6

AM7 Mach number at station 7

AM8 Mach number at station 8

AM9 Mach number at station 9

BLC bleed flow out of compressor, kg/sec (lbm/sec)

BLDU bleed flow into fan duct, kg/sec (lbm/sec)

BLF bleed flow out of fan (dumped overboard), kg/sec
 (lbm/sec)

BLHP bleed flow into high-pressure turbine, kg/sec
 (lbm/sec)

BLI airflow into third stream, kg/sec (lbm/sec)

BLIP bleed flow into intermediate-pressure turbine,
 kg/sec (lbm/sec)

BLLP bleed flow into low-pressure turbine, kg/sec
 (lbm/sec)

BLOB	bleed flow lost overboard (customer bleed), kg/sec (lbm/sec)
BPRINT	ratio of airflow into wing duct to airflow into core
BYPASS	ratio of airflow into fan duct to airflow into intermediate compressor
CNC	corrected shaft speed of core compressor
CNF	corrected shaft speed of fan compressor
CNHP	corrected shaft speed of high-pressure turbine
CNHPCF	correction factor of high-pressure-turbine corrected speed
* CNHPDS	design corrected speed of high-pressure turbine
CNI	corrected shaft speed of intermediate compressor
CNIP	corrected shaft speed of intermediate-pressure turbine
CNIPCF	correction factor of intermediate-pressure- turbine corrected speed
* CNIPDS	design corrected speed of intermediate-pressure turbine
CNLP	corrected shaft speed of low-pressure turbine
CNLPCF	correction factor of low-pressure turbine corrected speed
* CNLPDS	design corrected speed of low-pressure turbine
CS	ambient speed of sound, m/sec (ft/sec)
* CVDNOZ	velocity coefficient of duct nozzle thrust
* CVDWNG	velocity coefficient of wing nozzle thrust
* CVMNOZ	velocity coefficient of core nozzle thrust
* DELFG	gross-thrust delta degradation multiplier
* DELFN	net-thrust delta degradation multiplier

* DELSFC specific-fuel-consumption delta degradation multiplier

* DELT1 correction to standard-day temperature, K ($^{\circ}$ R)

DHHPCF Δ enthalpy correction factor of high-pressure turbine

DHIPCF Δ enthalpy correction factor of intermediate-pressure turbine

DHLPCF Δ enthalpy correction factor of low-pressure turbine

DHTC work done by high-pressure turbine, J/kg (Btu/lbm)

DHTCHP enthalpy change of high-pressure turbine, temperature corrected, J/kg-K (Btu/lbm- $^{\circ}$ R)

DHTCIP enthalpy change of intermediate-pressure turbine, temperature corrected, J/kg-K (Btu/lbm- $^{\circ}$ R)

DHTCLP enthalpy change of low-pressure turbine, temperature corrected, J/kg-K (Btu/lbm- $^{\circ}$ R)

DHTF work done by low-pressure turbine, J/kg (Btu/lbm)

DHTI work done by intermediate-pressure turbine, J/kg (Btu/lbm)

* DPAFDS design pressure drop ($\Delta P/P$) of afterburner

DPAFT pressure drop ($\Delta P/P$) of afterburner

* DPCODS design pressure drop ($\Delta P/P$) of combustor

DPCOM pressure drop ($\Delta P/P$) of combustor

DPDUC pressure drop ($\Delta P/P$) of fan duct

* DPDUDS design pressure drop ($\Delta P/P$) of fan duct

* DPWGDS design pressure drop ($\Delta P/P$) of wing duct

DPWING pressure drop ($\Delta P/P$) of wing duct

* DT solution time step for transient, sec

* DTPRNT time step for output listings, sec

DUMD1(15) dummy variables

* DUMSPL	(logical) control for spool that does not change temperature or pressure of air
ERRER	(logical) test of exceeding ITFYS
* ETAA	efficiency of afterburner
* ETAADS	design efficiency of afterburner
ETAASV	saved efficiency of afterburner at design conditions
ETAB	efficiency of combustor
ETABCF	correction factor of combustor efficiency
* ETABDS	design efficiency of combustor
ETAC	adiabatic efficiency of core compressor
ETACCF	correction factor of core-compressor efficiency
* ETACDS	design adiabatic efficiency of core compressor
* ETAD	efficiency of ductburner
ETAF	adiabatic efficiency of fan compressor
ETAFCF	correction factor of fan-compressor efficiency
* ETAFDS	design adiabatic efficiency of fan compressor
ETAI	adiabatic efficiency of intermediate compressor
ETAI CF	correction factor of intermediate-compressor efficiency
* ETAIDS	design adiabatic efficiency of intermediate compressor
* ETAR	pressure recovery of inlet (ram recovery), P_2/P_1
ETATHP	adiabatic efficiency of high-pressure turbine
ETATIP	adiabatic efficiency of intermediate-pressure turbine
ETATLP	adiabatic efficiency of low-pressure turbine

ETHPCF	correction factor of high-pressure-turbine efficiency
* ETHPDS	design adiabatic efficiency of high-pressure turbine
ETIPCF	correction factor of intermediate-pressure-turbine efficiency
* ETIPDS	design adiabatic efficiency of intermediate-pressure turbine
ETLPCF	correction factor of low-pressure-turbine efficiency
* ETLPDS	design adiabatic efficiency of low-pressure turbine
* FAN	(logical) control that indicates fan or turbojet
FAR24	fuel-to-air ratio at station 24
FAR4	fuel-to-air ratio at station 4
FAR5	fuel-to-air ratio at station 5
FAR50	fuel-to-air ratio at station 50
FAR55	fuel-to-air ratio at station 55
FAR7	fuel-to-air ratio at station 7
FAR7SV	saved fuel-to-air ratio at station 7 at design conditions
FCOVFN	ratio of core thrust to net thrust
FFOVFN	ratio of fan thrust to net thrust
FG	gross thrust, N (lbf)
FGM	momentum thrust of all but wing, N (lbf)
FGMD	fan duct momentum thrust of all but wing, N (lbf)
FGMM	core nozzle momentum thrust of all but wing, N (lbf)
FGMWNG	momentum thrust of wing, N (lbf)

FGP	pressure thrust of all but wing, N (lbf)
FGPD	fan duct pressure thrust of all but wing, N (lbf)
FGPM	core nozzle pressure thrust of all but wing, N (lbf)
FGPWNG	pressure thrust of wing, N (lbf)
FMNOFN	ratio of fan plus core thrust to net thrust
FN	net thrust, N (lbf)
FNMAIN	net thrust of all but wing, N (lbf)
FNOVFD	ratio of net thrust to design-point net thrust
FNWING	net thrust of wing, N (lbf)
FRD	ram drag, N (lbf)
FWOVFN	ratio of net wing thrust to net thrust
* FXFN2M	(logical) control for boosted fan
* FXM2CP	(logical) control for supercharged compressor
H1	enthalpy at station 1, J/kg (Btu/lbm)
H2	enthalpy at station 2, J/kg (Btu/lbm)
H21	enthalpy at station 21, J/kg (Btu/lbm)
H22	enthalpy at station 22, J/kg (Btu/lbm)
H23	enthalpy at station 23, J/kg (Btu/lbm)
H24	enthalpy at station 24, J/kg (Btu/lbm)
H25	enthalpy at station 25, J/kg (Btu/lbm)
H28	enthalpy at station 28, J/kg (Btu/lbm)
H29	enthalpy at station 29, J/kg (Btu/lbm)
H3	enthalpy at station 3, J/kg (Btu/lbm)
H38	enthalpy at station 38, J/kg (Btu/lbm)
H39	enthalpy at station 39, J/kg (Btu/lbm)

H4	enthalpy at station 4, J/kg (Btu/lbm)
H5	enthalpy at station 5, J/kg (Btu/lbm)
H50	enthalpy at station 50, J/kg (Btu/lbm)
H55	enthalpy at station 55, J/kg (Btu/lbm)
H6	enthalpy at station 6, J/kg (Btu/lbm)
H7	enthalpy at station 7, J/kg (Btu/lbm)
H8	enthalpy at station 8, J/kg (Btu/lbm)
H9	enthalpy at station 9, J/kg (Btu/lbm)
* HPEXT	power extracted, W (hp)
* IAFTBN	index for afterburning desired; zeroes automatically; values of 0, 1, or 2
* IAMTP	index for ram or inlet operation desired; values of 0 to 5
* IAMTRX	index that indicates if A,B,C, and D matrices are to be calculated
ICOAFB	index of error in subroutine COAFBN
ICODUC	index of error in subroutine CODUCT
ICOMIX	index of error in subroutine COMIX
* IDBURN	index for duct burning desired; zeroes automatically; values of 0, 1, or 2
* IDCD	duct nozzle convergent-divergent when value=1; convergent when value=0
* IDES	index for design point; zeroes automatically; must be set to 1 to design engine
* IDUMP	index for dumping of error matrix; values of 0, 1, or 2
* IGASMX	index for mixed or no-mixed flow turbofans; values of -1, 0, 1, or 2
* IMCD	main nozzle convergent-divergent when value=1; convergent when value=0

* INIT index for initializing guesses; zeroes
 automatically; 0 calls GUESS, 1 does not

* ISPOOL number of engine rotors

* ITRAN index for initiating transient

* ITRYS maximum number of iterations allowed through
 engine counter

 JTRAN index that indicates a transient is in progress

 LOOPER number of loops through engine counter

* MODE independent variable designator for engine
 operation

* NOZFLT index for floating main or duct nozzle; zeroes
 automatically; values of 0 to 3

 P1 standard pressure, N/m^2 (atm)

* P2 total pressure at station 2, N/m^2 (atm)

 P21 total pressure at station 21, N/m^2 (atm)

 P22 total pressure at station 22, N/m^2 (atm)

 P23 total pressure at station 23, N/m^2 (atm)

 P24 total pressure at station 24, N/m^2 (atm)

 P25 total pressure at station 25, N/m^2 (atm)

 P28 total pressure at station 28, N/m^2 (atm)

 P29 total pressure at station 29, N/m^2 (atm)

 P3 total pressure at station 3, N/m^2 (atm)

 P37 total pressure at station 37, N/m^2 (atm)

 P38 total pressure at station 38, N/m^2 (atm)

 P39 total pressure at station 39, N/m^2 (atm)

 P4 total pressure at station 4, N/m^2 (atm)

 P5 total pressure at station 5, N/m^2 (atm)

P50	total pressure at station 50, N/m^2 (atm)
P55	total pressure at station 55, N/m^2 (atm)
P6	total pressure at station 6, N/m^2 (atm)
P6DSAV	saved total pressure at station 6 at design conditions, N/m^2 (atm)
P7	total pressure at station 7, N/m^2 (atm)
P8	total pressure at station 8, N/m^2 (atm)
P9	total pressure at station 9, N/m^2 (atm)
* PCBLC	ratio of compressor bleed to cool turbines to total compressor airflow
* PCBLDU	ratio of compressor bleed leaked into fan duct to total compressor bleed flow
* PCBLF	ratio of bleed from fan compressor to fan airflow dumped overboard (i.e., leakage)
* PCBLHP	fraction of PCBLC used in high-pressure turbine for cooling
* PCBLI	fraction of intermediate compressor air that goes into third stream
* PCBLID	ratio of design value of air into wing to air into core; zero for two-stream engine
* PCBLIP	fraction of PCBLC used in intermediate-pressure turbine for cooling
* PCBLLP	fraction of PCBLC used in low-pressure turbine for cooling
* PCBLOB	fraction of bleed air out of compressor lost overboard (for customer use)
* PCNC	shaft speed of core compressor as a percent of design
* PCNCDS	design corrected speed of core compressor as a percent of design
PCNCGU	guessed shaft speed of core compressor as a percent of design

* PCNF shaft speed of fan compressor as a percent of design

* PCNFDS design corrected speed of fan compressor as a percent of design

PCNFGU guessed shaft speed of fan compressor as a percent of design

* PCNI shaft speed of intermediate compressor as a percent of design

* PCNIDS design corrected speed of intermediate compressor as a percent of design

PCNIGU guessed shaft speed of intermediate compressor as a percent of design

* PMIHP polar moment of inertia of high-pressure rotor, kg-m^2 (slug-ft²)

* PMIIP polar moment of inertia of intermediate-pressure rotor, kg-m^2 (slug-ft²)

* PMILP polar moment of inertia of low-pressure rotor, kg-m^2 (slug-ft²)

PRC pressure ratio of core compressor

PRCCF correction factor of core-compressor pressure ratio

* PRCDS design pressure ratio of core compressor

PRF pressure ratio of fan compressor

PRFCF correction factor of fan-compressor pressure ratio

* PRFDS design pressure ratio of fan compressor

PRI pressure ratio of intermediate compressor

PRICF correction factor of intermediate-compressor pressure ratio

* PRIDS design pressure ratio of intermediate compressor

PS28 static pressure at station 28, N/m^2 (atm)

PS29 static pressure at station 29, N/m^2 (atm)

PS38 static pressure at station 38, N/m^2 (atm)
 PS39 static pressure at station 39, N/m^2 (atm)
 * PS55 Input: static pressure at low-pressure-turbine
 exit, station 55, N/m^2 (atm)
 Output: static pressure at station 55, N/m^2 (atm)
 PS6 static pressure at station 6, N/m^2 (atm)
 PS7 static pressure at station 7, N/m^2 (atm)
 PS8 static pressure at station 8, N/m^2 (atm)
 PS9 static pressure at station 9, N/m^2 (atm)
 S1 entropy at station 1, J/kg-K ($\text{Btu/lbm-}^\circ\text{R}$)
 S2 entropy at station 2, J/kg-K ($\text{Btu/lbm-}^\circ\text{R}$)
 S21 entropy at station 21, J/kg-K ($\text{Btu/lbm-}^\circ\text{R}$)
 S22 entropy at station 22, J/kg-K ($\text{Btu/lbm-}^\circ\text{R}$)
 S23 entropy at station 23, J/kg-K ($\text{Btu/lbm-}^\circ\text{R}$)
 S24 entropy at station 24, J/kg-K ($\text{Btu/lbm-}^\circ\text{R}$)
 S25 entropy at station 25, J/kg-K ($\text{Btu/lbm-}^\circ\text{R}$)
 S28 entropy at station 28, J/kg-K ($\text{Btu/lbm-}^\circ\text{R}$)
 S29 entropy at station 29, J/kg-K ($\text{Btu/lbm-}^\circ\text{R}$)
 S3 entropy at station 3, J/kg-K ($\text{Btu/lbm-}^\circ\text{R}$)
 S4 entropy at station 4, J/kg-K ($\text{Btu/lbm-}^\circ\text{R}$)
 S5 entropy at station 5, J/kg-K ($\text{Btu/lbm-}^\circ\text{R}$)
 S50 entropy at station 50, J/kg-K ($\text{Btu/lbm-}^\circ\text{R}$)
 S55 entropy at station 55, J/kg-K ($\text{Btu/lbm-}^\circ\text{R}$)
 S6 entropy at station 6, J/kg-K ($\text{Btu/lbm-}^\circ\text{R}$)
 S7 entropy at station 7, J/kg-K ($\text{Btu/lbm-}^\circ\text{R}$)
 S8 entropy at station 8, J/kg-K ($\text{Btu/lbm-}^\circ\text{R}$)
 S9 entropy at station 9, J/kg-K ($\text{Btu/lbm-}^\circ\text{R}$)

SFC specific fuel consumption, kg/N-hr (lbm/lbf-hr)

* SI (logical) control for SI or U.S. customary
 (English) units

T1 standard temperature, station 1, K (°R)

* T2 Input: total temperature at fan inlet,
 station 2, K (°R)
 Output: total temperature at station 2, K (°R)

T21 total temperature at station 21, K (°R)

T21DS total temperature at intermediate-compressor
 exit at design conditions, station 21, K (°R)

T22 total temperature at station 22, K (°R)

T22DS design total temperature at fan exit, station 22,
 K (°R)

T23 total temperature at station 23, K (°R)

* T24 Input: total temperature at ductburner exit,
 station 24, K (°R)
 Output: total temperature at station 24, K (°R)

T25 total temperature at station 25, K (°R)

T28 total temperature at station 28, K (°R)

T29 total temperature at station 29, K (°R)

T2DS design total temperature at fan inlet, station 2,
 K (°R)

T3 total temperature at station 3, K (°R)

T38 total temperature at station 38, K (°R)

T39 total temperature at station 39, K (°R)

* T4 Input: total temperature at combustor exit,
 station 4, K (°R)
 Output: total temperature at station 4, K (°R)

* T4DS design total temperature at combustor exit,
 station 4, K (°R)

T4GU guessed total temperature at station 4, K (°R)

T5 total temperature at station 5, K ($^{\circ}$ R)
 T50 total temperature at station 50, K ($^{\circ}$ R)
 T55 total temperature at station 55, K ($^{\circ}$ R)
 T6 total temperature at station 6, K ($^{\circ}$ R)
 * T7 Input: total temperature at afterburner exit,
 station 7, K ($^{\circ}$ R)
 Output: total temperature at station 7, K ($^{\circ}$ R)
 * T7DS design total temperature at afterburner exit,
 station 7, K ($^{\circ}$ P)
 T8 total temperature at station 8, K ($^{\circ}$ R)
 T9 total temperature at station 9, K ($^{\circ}$ R)
 * TF final time for transient, sec
 TFAR total fuel-to-air ratio
 TFFHP flow function of high-pressure turbine,
 kg- \sqrt{K} -m²/N-sec (lbm- $\sqrt{^{\circ}F}$ -in²/lbf-sec)
 TFFIP flow function of intermediate-pressure turbine,
 kg- \sqrt{K} -m²/N-sec (lbm- $\sqrt{^{\circ}R}$ -in²/lbf-sec)
 TFFLP flow function of low-pressure turbine,
 kg- \sqrt{K} -m²/N-sec (lbm- $\sqrt{^{\circ}R}$ -in²/lbf-sec)
 TFHPCF correction factor of high-pressure turbine flow
 function
 * TFHPDS design flow function of high-pressure turbine,
 kg- \sqrt{K} -m²/N-sec (lbm- $\sqrt{^{\circ}R}$ -in²/lbf-sec)
 TFIPCF correction factor of intermediate-pressure
 turbine flow function
 * TFIPDS design flow function of intermediate-pressure
 turbine, kg- \sqrt{K} -m²/N-sec (lbm- $\sqrt{^{\circ}R}$ -in²/lbf-sec)
 TFLPCF correction factor of low-pressure turbine flow
 function
 * TFLPDS design flow function of low-pressure turbine,
 kg- \sqrt{K} -m²/N-sec (lbm- $\sqrt{^{\circ}R}$ -in²/lbf-sec)

TIME	time, sec
* TOLALL	tolerance on convergence
TS28	static temperature at station 28, K (°R)
TS29	static temperature at station 29, K (°R)
TS38	static temperature at station 38, K (°R)
TS39	static temperature at station 39, K (°R)
TS7	static temperature at station 7, K (°R)
TS8	static temperature at station 8, K (°R)
TS9	static temperature at station 9, K (°R)
U21	internal energy at station 21, J/kg (Btu/lbm)
U22	internal energy at station 22, J/kg (Btu/lbm)
U24	internal energy at station 24, J/kg (Btu/lbm)
U3	internal energy at station 3, J/kg (Btu/lbm)
U37	internal energy at station 37, J/kg (Btu/lbm)
U4	internal energy at station 4, J/kg (Btu/lbm)
U5	internal energy at station 5, J/kg (Btu/lbm)
U50	internal energy at station 50, J/kg (Btu/lbm)
U55	internal energy at station 55, J/kg (Btu/lbm)
U7	internal energy at station 7, J/kg (Btu/lbm)
V25	velocity at station 25, m/sec (ft/sec)
V28	velocity at station 28, m/sec (ft/sec)
V29	velocity at station 29, m/sec (ft/sec)
V38	velocity at station 38, m/sec (ft/sec)
V39	velocity at station 39, m/sec (ft/sec)
V55	velocity at station 55, m/sec (ft/sec)
V6	velocity at station 6, m/sec (ft/sec)

V7 velocity at station 7, m/sec (ft/sec)
 V8 velocity at station 8, m/sec (ft/sec)
 V9 velocity at station 9, m/sec (ft/sec)
 VA velocity of aircraft, m/sec (ft/sec)
 * VAFBN control volume associated with afterburner,
 m³ (ft³)
 * VCOMB control volume associated with combustor,
 m³ (ft³)
 * VCOMP control volume associated with core compressor,
 m³ (ft³)
 * VFAN control volume associated with fan compressor,
 m³ (ft³)
 * VFDUCT control volume associated with fan duct, m³ (ft³)
 * VHPTRB control volume associated with high-pressure
 turbine, m³ (ft³)
 * VINTC control volume associated with intermediate
 compressor, m³ (ft³)
 * VIPTRB control volume associated with
 intermediate-pressure turbine, m³ (ft³)
 VJD velocity of fan duct exhaust, m/sec (ft/sec)
 VJM velocity of core exhaust, m/sec (ft/sec)
 VJW velocity of wing duct exhaust, m/sec (ft/sec)
 * VLPTRB control volume associated with low-pressure
 turbine, m³ (ft³)
 * VWDUCT control volume associated with wing duct,
 m³ (ft³)
 WA21 airflow at station 21, kg/sec (lbm/sec)
 WA22 airflow at station 22, kg/sec (lbm/sec)
 WA23DS airflow at station 23 at design conditions,
 kg/sec (lbm/sec)
 WA3 airflow at station 3, kg/sec (lbm/sec)

WA32	airflow at station 32, kg/sec (lbm/sec)
WA32DS	airflow at station 32 at design conditions, kg/sec (lbm/sec)
WA3CDS	corrected airflow in combustor at design conditions, station 3, kg/sec (lbm/sec)
WAC	airflow of core compressor, kg/sec (lbm/sec)
WACC	corrected airflow of core compressor, kg/sec (lbm/sec)
* WACCDS	design corrected airflow of core compressor, kg/sec (lbm/sec)
WACCF	correction factor of core-compressor corrected airflow
WACDS	airflow of core compressor at design conditions, kg/sec (lbm/sec)
WACI	corrected airflow of intermediate compressor, kg/sec (lbm/sec)
WACP	saved airflow of core compressor, kg/sec (lbm/sec)
WAD	airflow of fan duct, kg/sec (lbm/sec)
WAF	airflow of fan compressor, kg/sec (lbm/sec)
W AFC	corrected airflow of fan compressor, kg/sec (lbm/sec)
* WAFCDs	design corrected airflow of fan compressor, kg/sec (lbm/sec)
WAFCF	correction factor of fan compressor corrected airflow
WAFDS	airflow of fan compressor at design conditions, kg/sec (lbm/sec)
WAFP	saved airflow of fan compressor, kg/sec (lbm/sec)
WAI	airflow of intermediate compressor, kg/sec (lbm/sec)

* WAICDS design corrected airflow of intermediate compressor, kg/sec (lbm/sec)

WAICF correction factor of intermediate-compressor corrected airflow

WAIDS airflow of intermediate compressor at design conditions, kg/sec (lbm/sec)

WAIP saved airflow of intermediate compressor, kg/sec (lbm/sec)

* WFA fuel flow rate to afterburner (IAFTBN=2 only for input), kg/sec (lbm/sec)

* WFB fuel flow rate to main combustor (MODE=2 only for input), kg/sec (lbm/sec)

* WFBDS design fuel flow rate to main combustor (MODE=2 only for input), kg/sec (lbm/sec)

WFD fuel flow rate to ductburner, kg/sec (lbm/sec)

WFT total fuel flow rate, kg/sec (lbm/sec)

WG24 gas flow at station 24, kg/sec (lbm/sec)

WG37 gas flow at station 37, kg/sec (lbm/sec)

WG4 gas flow at station 4, kg/sec (lbm/sec)

WG5 gas flow at station 5, kg/sec (lbm/sec)

WG50 gas flow at station 50, kg/sec (lbm/sec)

WG55 gas flow at station 55, kg/sec (lbm/sec)

WG6 gas flow at station 6, kg/sec (lbm/sec)

WG6CDS corrected gas flow at station 6 at design conditions, kg/sec (lbm/sec)

WG7 gas flow at station 7, kg/sec (lbm/sec)

WGT total gas flow rate, kg/sec (lbm/sec)

XBLDU saved BLDU

XBLF saved BLF

XFAR24	saved FAR24
XFAR55	saved FAR55
XH21	saved H21
XH25	saved H25
XH3	saved H3
XH55	saved H55
XNHP	speed of core compressor, rpm
* XNHPDS	design speed of high-pressure rotor, rpm
XNIP	speed of intermediate compressor, rpm
* XNIPDS	design speed of intermediate-pressure rotor, rpm
XNLDEM	commanded speed of fan compressor, rpm
XNLP	speed of fan compressor, rpm
* XNLPDS	design speed of low-pressure rotor, rpm
XP1	saved P1
XP21	saved P21
XP25	saved P25
XP55	saved P55
XS21	saved S21
XS25	saved S25
XS55	saved S55
XT21	saved T21
XT25	saved T25
XT55	saved T55
XWAC	saved WAC
XWAF	saved WAF
XWFB	saved WFB

XWFD	saved WFD
XWG24	saved WG24
XWG55	saved WG55
XXP1	saved P1
ZC	ratio of core-compressor pressure ratios
* ZCDS	design ratio of core compressor; equals pressure ratio at design point on design speed line minus value of pressure ratio at lowest point on speed line, divided by high (surge) value minus low value of pressure ratio on design speed line
ZF	ratio of fan-compressor pressure ratios
* ZFDS	design ratio of fan compressor (see ZCDS for explanation)
ZI	ratio of intermediate-compressor pressure ratios
* ZIDS	design ratio of intermediate compressor (see ZCDS for explanation)

APPENDIX B

FORTRAN LISTINGS

Main Program DYGABCD

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C      THIS IS THE MAIN PROGRAM
      IMPLICIT REAL*8 (A-H,O-Z)
      LOGICAL SI, ERRER, DUMSPL, FXFN2M, FXM2CP, AFTFAN, FAN
      COMMON /COMALL/ COM(1062)
      DIMENSION WORD(2), ERR(9), DUMD1(15), FO(50,4), SO(10,6),
1 PDATA(5,50), TIMEPT(50), XS(23), PVRDOT(23)
      EQUIVALENCE (WORD(1), COM(1)), (IDES, COM(3)), (JDES, COM(4)),
1 (KDES, COM(5)), (MODE, COM(6)), (INIT, COM(7)), (IDUMP, COM(8)),
2 (IAMTP, COM(9)), (IGASMX, COM(10)), (IDBURN, COM(11)),
3 (IAFTBN, COM(12)), (IDCD, COM(13)), (IMCD, COM(14)),
4 (IDSHOC, COM(15)), (IMSHOC, COM(16)), (MOZFLT, COM(17)),
5 (ITRYS, COM(18)), (LOOPER, COM(19)), (NOMAP, COM(20)),
6 (NUMMAP, COM(21)), (MAPEDG, COM(22)), (TOLALL, COM(23)),
7 (ERR(1), COM(24)), (P1, COM(33)), (H22, COM(34)),
8 (AM23, COM(35)), (WA23DS, COM(36)), (T23, COM(37)),
9 (P23, COM(38)), (H23, COM(39)), (S23, COM(40)), (A24, COM(41)),
1 (T24, COM(42)), (H24, COM(43)), (S24, COM(44)), (AM25, COM(45)),
2 (T25, COM(46)), (P25, COM(47)), (H25, COM(48)), (S25, COM(49)),
3 (A28, COM(50)), (A28SAV, COM(51)), (AM28, COM(52)),
4 (V28, COM(53)), (TS28, COM(54)), (PS28, COM(55)), (T28, COM(56)),
5 (P28, COM(57)), (H28, COM(58)), (S28, COM(59)), (A29, COM(60)),
6 (A29SAV, COM(61)), (AM29, COM(62)), (V29, COM(63)),
7 (TS29, COM(64)), (PS29, COM(65)), (T29, COM(66)), (P29, COM(67)),
8 (H29, COM(68)), (S29, COM(69)), (BYPASS, COM(70)),
9 (WAD, COM(71)), (WFD, COM(72)), (ETAD, COM(73)),
1 (DPDUC, COM(74)), (DPDUDS, COM(75)), (XFP1, COM(76))
      EQUIVALENCE (XWG24, COM(77)), (XFAR24, COM(78)), (XT25, COM(79)),
1 (XP25, COM(80)), (XH25, COM(81)), (XS25, COM(82)),
2 (XWG55, COM(83)), (XFAR55, COM(84)), (XT55, COM(85)),
3 (XP55, COM(86)), (XH55, COM(87)), (XS55, COM(88)),
4 (XWFB, COM(89)), (XWFD, COM(90)), (T2DS, COM(91)), (T2, COM(92)),
5 (P2, COM(93)), (H2, COM(94)), (S2, COM(95)), (S22, COM(96)),
6 (T22DS, COM(97)), (A25, COM(98)), (V25, COM(99)),
7 (T4GU, COM(100)), (T4DS, COM(101)), (T5, COM(102)),
8 (H5, COM(103)), (S5, COM(104)), (WGE, COM(105)),
9 (FAR5, COM(106)), (A455, COM(107)), (V55, COM(108)),
1 (A55, COM(109)), (PS55, COM(110)), (S6, COM(111)),
2 (PS6, COM(112)), (V6, COM(113)), (TFHPCF, COM(114)),
3 (CNHPCF, COM(115)), (ETHPCF, COM(116)), (DHHPCF, COM(117)),
4 (TFHPDS, COM(118)), (CNHPDS, COM(119)), (ETHPDS, COM(120)),
5 (PRFCF, COM(121)), (ETAFCF, COM(122)), (WAFCF, COM(123)),
6 (PCNFDS, COM(124)), (PRFDS, COM(125)), (ETAFDS, COM(126)),
7 (WAFDS, COM(127)), (PCNCGU, COM(128)), (HPEXT, COM(129)),
8 (WACCDs, COM(130)), (PPF, COM(131)), (ETAF, COM(132)),
9 (ZCDS, COM(133)), (CNF, COM(134)), (WAFc, COM(135)),
1 (ZF, COM(136)), (PCNP, COM(137)), (PCBLF, COM(138))
      EQUIVALENCE (ZI, COM(139)), (PCNI, COM(140)), (TFFIP, COM(141)),
1 (CNIP, COM(142)), (ETATIP, COM(143)), (DHTCIP, COM(144)),
2 (DHTI, COM(145)), (ZIDS, COM(146)), (PCNIDS, COM(147)),
3 (PCNIGU, COM(148)), (T1, COM(149)), (H1, COM(150)),
4 (S1, COM(151)), (T3, COM(152)), (H3, COM(153)), (WA3, COM(154)),
5 (WA3CDS, COM(155)), (T4, COM(156)), (H4, COM(157)),
6 (S4, COM(158)), (WG4, COM(159)), (FAR4, COM(160)),
7 (T50, COM(161)), (H50, COM(162)), (S50, COM(163)),

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8 (WG50, COM(164)), (PAR50, COM(165)), (PCBLHP, COM(166)),	ABCD0055
9 (PCBLIP, COM(167)), (PCBLLP, COM(168)), (PCBLDU, COM(169)),	ABCD0056
1 (PCBLOB, COM(170)), (CNHP, COM(171)), (ETATHP, COM(172)),	ABCD0057
2 (DHTCHP, COM(173)), (DHTC, COM(174)), (TFFHP, COM(175)),	ABCD0058
3 (PRICF, COM(176)), (ETAICF, COM(177)), (WAICF, COM(178)),	ABCD0059
4 (ETABCF, COM(179)), (PRIDS, COM(180)), (ETAIDS, COM(181)),	ABCD0060
5 (WAIDS, COM(182)), (WAICDS, COM(183)), (ETABDS, COM(184)),	ABCD0051
6 (WFBDS, COM(185)), (ZFDS, COM(186)), (ETAR, COM(187)),	ABCD0062
7 (ETAI, COM(188)), (PRI, COM(189)), (ETAB, COM(190)),	ABCD0063
8 (WAC, COM(191)), (WFB, COM(192)), (BLC, COM(193)),	ABCD0054
9 (CS, COM(194)), (AM, COM(195)), (ALTP, COM(196)),	ABCD0065
1 (DPCODS, COM(197)), (DPCOM, COM(198)), (PCNFGU, COM(199))	ABCD0066
EQUIVALENCE (XP1, COM(200)), (XI21, COM(201)), (XP21, COM(202)),	ABCD0067
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2 (XWAF, COM(206)), (XWAC, COM(207)), (XBLP, COM(208)),	ABCD0059
3 (XBLDU, COM(209)), (WG37, COM(210)), (A38, COM(211)),	ABCD0070
4 (AM38, COM(212)), (V38, COM(213)), (T38, COM(214)),	ABCD0071
5 (H38, COM(215)), (P38, COM(216)), (TS38, COM(217)),	ABCD0072
6 (PS38, COM(218)), (A39, COM(219)), (AM39, COM(220)),	ABCD0073
7 (V39, COM(221)), (T39, COM(222)), (H39, COM(223)),	ABCD0074
8 (P39, COM(224)), (TS39, COM(225)), (PS39, COM(226)),	ABCD0075
9 (WA32DS, COM(227)), (DPWING, COM(228)), (BPRINT, COM(229)),	ABCD0075
1 (FGMWNG, COM(230)), (FGPWNG, COM(231)), (FNWING, COM(232)),	ABCD0077
2 (FNMAIN, COM(233)), (FWOVFN, COM(234)), (DPWGDS, COM(235)),	ABCD0073
3 (DELFG, COM(236)), (DELFN, COM(237)), (DELSFC, COM(238)),	ABCD0079
4 (CVDWNG, COM(239)), (CVDNJZ, COM(240)), (CVMNOZ, COM(241)),	ABCD0080
5 (VA, COM(242)), (VJD, COM(243)), (VJW, COM(244)),	ABCD0081
6 (VJM, COM(245)), (WFT, COM(245)), (WGT, COM(247)),	ABCD0082
7 (SFC, COM(248)), (TFAR, COM(249)), (FRD, COM(250)),	ABCD0083
8 (FGMD, COM(251)), (FGMM, COM(252)), (FGPD, COM(253)),	ABCD0084
9 (FGPM, COM(254)), (FGM, COM(255)), (FGP, COM(256)),	ABCD0085
1 (FG, COM(257)), (FN, COM(258)), (FFOVFN, COM(259))	ABCD0085
EQUIVALENCE (FCOVFN, COM(260)), (FMNOFN, COM(261)),	ABCD0087
1 (FNOVFD, COM(262)), (T21, COM(263)), (H21, COM(264)),	ABCD0083
2 (S21, COM(265)), (WA21, COM(266)), (T21DS, COM(267)),	ABCD0089
3 (T22, COM(268)), (WA22, COM(269)), (S3, COM(270)),	ABCD0090
4 (WA32, COM(271)), (T55, COM(272)), (H55, COM(273)),	ABCD0091
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6 (ETLPDS, COM(277)), (TFIPDS, COM(278)), (CNIPDS, COM(279)),	ABCD0093
7 (ETIPDS, COM(280)), (TFLPCF, COM(281)), (CNLPFC, COM(282)),	ABCD0094
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1 (TFFLP, COM(289)), (CNLP, COM(290)), (ETATLP, COM(291)),	ABCD0097
2 (DHTCLP, COM(292)), (DHTF, COM(293)), (PRCCF, COM(294)),	ABCD0093
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5 (PCNC, COM(301)), (PCBLC, COM(302)), (PCNCDS, COM(303)),	ABCD0101
6 (PCBLI, COM(304)), (PCBLID, COM(305)), (CNC, COM(306)),	ABCD0102
7 (PRC, COM(307)), (ETAC, COM(308)), (CNI, COM(309)),	ABCD0103
8 (WACI, COM(310)), (WAI, COM(311)), (BLI, COM(312)),	ABCD0104
9 (BLHP, COM(313)), (BLIP, COM(314)), (BLLP, COM(315)),	ABCD0105
1 (BLP, COM(316)), (BLDU, COM(317)), (BLOB, COM(318))	ABCD0105
EQUIVALENCE (WAF, COM(319)), (WACC, COM(320)), (WG24, COM(321)),	ABCD0107
1 (PAR24, COM(322)), (WG55, COM(323)), (PAR55, COM(324)),	ABCD0108

2	(P6DSAV, COM(325)), (AM6DSV, COM(326)), (AM6, COM(327)),	ABCD0109
3	(A6, COM(328)), (WG6CDS, COM(329)), (WG6, COM(330)),	ABCD0110
4	(T6, COM(331)), (P6, COM(332)), (H6, COM(333)), (WG7, COM(334)),	ABCD0111
5	(FAR7, COM(335)), (FAR7SV, COM(336)), (TS7, COM(337)),	ABCD0112
6	(PS7, COM(338)), (V7, COM(339)), (AM7, COM(340)), (A7, COM(341)),	ABCD0113
7	(T7DS, COM(342)), (T7, COM(343)), (H7, COM(344)), (S7, COM(345)),	ABCD0114
8	(A8, COM(346)), (A8SAV, COM(347)), (TS8, COM(348)),	ABCD0115
9	(PS8, COM(349)), (V8, COM(350)), (AM8, COM(351)), (T8, COM(352)),	ABCD0115
1	(P8, COM(353)), (H8, COM(354)), (S8, COM(355)), (A9, COM(356)),	ABCD0117
2	(A9SAV, COM(357)), (TS9, COM(358)), (PS9, COM(359)),	ABCD0118
3	(V9, COM(360)), (AM9, COM(361)), (T9, COM(362)), (P9, COM(363)),	ABCD0119
4	(H9, COM(364)), (S9, COM(365)), (ETAADS, COM(366)),	ABCD0120
5	(DPAFDS, COM(367)), (WFA, COM(368)), (ETAA, COM(369)),	ABCD0121
6	(ETAASV, COM(370)), (DPAFT, COM(371)), (XNHP, COM(372)),	ABCD0122
7	(XNIP, COM(373)), (XNLP, COM(374)), (P22, COM(375)),	ABCD0123
8	(U22, COM(376)), (P21, COM(377)), (U21, COM(378)),	ABCD0124
9	(P3, COM(379)), (U3, COM(380)), (P4, COM(381)), (U4, COM(382)),	ABCD0125
1	(P50, COM(383)), (U50, COM(384)), (P5, COM(385)), (U5, COM(386))	ABCD0126
	EQUIVALENCE (P55, COM(387)), (U55, COM(388)), (P7, COM(389)),	ABCD0127
1	(U7, COM(390)), (P24, COM(391)), (U24, COM(392)),	ABCD0128
2	(P37, COM(393)), (U37, COM(394)), (VFAN, COM(395)),	ABCD0129
3	(VINTC, COM(396)), (VCOMP, COM(397)), (VCOMB, COM(398)),	ABCD0130
4	(VHPTRB, COM(399)), (VIPTRB, COM(400)), (VLPTRB, COM(401)),	ABCD0131
5	(VAFTBN, COM(402)), (VFDUCT, COM(403)), (VWDUCT, COM(404)),	ABCD0132
6	(DUMD1(1), COM(405)), (WAFP, COM(420)), (WAIP, COM(421)),	ABCD0133
7	(WACP, COM(422)), (XNHPDS, COM(423)), (XNIPDS, COM(424)),	ABCD0134
8	(XNLPDS, COM(425)), (PMIHP, COM(426)), (PMIIP, COM(427)),	ABCD0135
9	(PMILP, COM(428)), (DELT1, COM(429)), (FO(1,1), COM(430)),	ABCD0136
1	(XNLDEM, COM(630)), (SO(1,1), COM(631)), (PDATA(1,1), COM(691)),	ABCD0137
2	(TIMEPT(1), COM(941)), (PRFNEW, COM(991)), (PRCNEW, COM(992)),	ABCD0138
3	(TIME, COM(993)), (DT, COM(994)), (TF, COM(995)),	ABCD0139
4	(TPRINT, COM(996)), (DTPRNT, COM(997)), (PVRDOT(1), COM(998)),	ABCD0140
5	(XS(1), COM(1021)), (ISPOOL, COM(1044)), (ICOAFB, COM(1045)),	ABCD0141
6	(ICODUC, COM(1046)), (ICOMIX, COM(1047)), (KKG0, COM(1048)),	ABCD0142
7	(IATRN, COM(1049)), (JTRAN, COM(1050)), (NSTEP, COM(1051)),	ABCD0143
8	(IVRDOT, COM(1052)), (IDOT, COM(1053)), (IAMTRX, COM(1054)),	ABCD0144
9	(SI, COM(1055)), (ERRER, COM(1056)), (DUMSPL, COM(1057)),	ABCD0145
1	(FXFN2M, COM(1058)), (FXM2CP, COM(1059)), (AFTFAN, COM(1060))	ABCD0146
	EQUIVALENCE (FAN, COM(1061)), (WAFCDs, COM(1062))	ABCD0147
	ERRER = .FALSE.	ABCD0148
	ITRAN = 0	ABCD0149
	JTRAN = 0	ABCD0150
	NSTEP = 0	ABCD0151
	TIME = 0.0D0	ABCD0152
	TPRINT = 0.0D0	ABCD0153
	DTPRNT = 0.0D0	ABCD0154
	IDOT = 0	ABCD0155
	<u>IAMTRX = 0</u>	<u>ABCD0155</u>
	DO 1 J = 3,404	ABCD0157
1	WORD(J) = 0.0D0	ABCD0158
	DO 2 J = 1057,1062	ABCD0159
2	WORD(J) = 0.0D0	ABCD0160
	ISPOOL = 0	ABCD0161
C	SET ARBITRARY VALUES FOR INTERMEDIATE SPOOL DESIGN PARAMETERS TO	ABCD0162

```

C      AVOID ERROR WHEN RUNNING A DUMMYSPOOL ENGINE
      PRIDS = 1.5D0
      ETAIDS = 1.0D0
      PCNIDS = 100.0D0
      ZIDS = .75D0
      PCNCDS = 100.0D0
      KKGO = 0
      CALL CONOUT(1)
      P6DSAV = 1.0D0
      AM6DSV = 1.0D0
      ETAASV = 1.0D0
      FAR7SV = 1.0D0
      CALL ENGBAL
      STOP
      END

```

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ABCD0163
ABCD0164
ABCD0165
ABCD0166
ABCD0167
ABCD0168
ABCD0169
ABCD0170
ABCD0171
ABCD0172
ABCD0173
ABCD0174
ABCD0175
ABCD0176
ABCD0177

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Subroutine AFQUIR

```

      SUBROUTINE AFQUIR (X,AIND,DEPEND,ANS,AJ,TOL,DIR,ANEW,ICON)
      IMPLICIT REAL*8 (A-H,O-Z)
      DIMENSION X(9)
C X(1)=NAME OF ARRAY TO USE
C AIND=INDEPENDENT VARIABLE
C DEPEND= DEPENDENT VARIABLE
C ANS=ANSWER UPON WHICH TO CONVERGE
C AJ=MAX NUMBER OF TRIES
C TOL=PERCENT TOLERANCE FOR CONVERGENCE
C DIR=DIRECTION AND PERCENTAGE FOR FIRST GUESS
C ANEW=CALCULATED VALUE OF NEXT TRY AT INDEPENDENT VARIABLE
C ICON=CONTROL  =1 GO THRU LOOP AGAIN
C                =2 YOU HAVE REACHED THE ANSWER
C                =3 COUNTER HAS HIT LIMITS
C X(2)=COUNTER STORAGE
C X(3)=CHOOSES METHOD OF CONVERGENCE
C X(4)=THIRD DEPEND VAR
C X(5)=THIRD IND VAR
C X(6)=SECOND DEPEND VAR
C X(7)=SECOND IND VAR
C X(8)=FIRST DEPEND VAR
C X(9)=FIRST IND VAR
C X(3) MUST BE ZERO UPON FIRST ENTRY TO ROUTINE
      Y = 0.0D0
      IF (ANS .EQ. 0.0D0) GO TO 2
      DEF = DEPEND - ANS
      TOLANS = TOL * ANS
      GO TO 3
2     DEP = DEPEND
      TOLANS = TOL
3     IF (DABS(DEP) .LE. TOLANS) GO TO 5
      IF (X(2) - AJ) 8,8,7
5     ANEW = AIND
      X(2) = 0.0D0
      ICON = 2
      RETURN

```

```

ABCD0173
ABCD0179
ABCD0180
ABCD0181
ABCD0182
ABCD0183
ABCD0184
ABCD0185
ABCD0186
ABCD0187
ABCD0188
ABCD0189
ABCD0190
ABCD0191
ABCD0192
ABCD0193
ABCD0194
ABCD0195
ABCD0196
ABCD0197
ABCD0198
ABCD0199
ABCD0200
ABCD0201
ABCD0202
ABCD0203
ABCD0204
ABCD0205
ABCD0206
ABCD0207
ABCD0208
ABCD0209
ABCD0210
ABCD0211
ABCD0212
ABCD0213

```

6	ANEW = Y	ABCD0214
	X(2) = X(2) + 1.0D0	ABCD0215
	ICON = 1	ABCD0216
	RETURN	ABCD0217
7	ANEW = Y	ABCD0218
	X(2) = 0.0D0	ABCD0219
	ICON = 3	ABCD0220
	RETURN	ABCD0221
8	IF (X(3) .GT. 0.0D0) GO TO 12	ABCD0222
C ***	FIRST GUESS USING DIR	ABCD0223
9	X(3) = 1.0D0	ABCD0224
	X(8) = DEP	ABCD0225
	X(9) = AIND	ABCD0225
	IF (AIND .EQ. 0.0D0) GO TO 11	ABCD0227
10	Y = DIR * AIND	ABCD0223
	GO TO 6	ABCD0229
11	Y = DIR	ABCD0230
	GO TO 6	ABCD0231
12	IF (X(3) .GT. 1.0D0) GO TO 16	ABCD0232
C ***	LINEAR GUESS	ABCD0233
13	X(3) = 2.0D0	ABCD0234
	X(6) = DEP	ABCD0235
	X(7) = AIND	ABCD0235
	IF (X(8) .EQ. X(6) .OR. X(9) .EQ. X(7)) GO TO 9	ABCD0237
	A = (X(9) - X(7)) / (X(8) - X(6))	ABCD0238
	Y = X(9) - A * X(8)	ABCD0239
	IF (DABS(10.0D0 * X(9)) - DABS(Y)) 9,9,6	ABCD0240
C ***	QUADRATIC GUESS	ABCD0241
15	X(4) = DEP	ABCD0242
	X(5) = AIND	ABCD0243
	IF (X(7) .NE. X(5)) GO TO 18	ABCD0244
	IF (X(6) - X(4)) 13,9,13	ABCD0245
18	IF (X(6) .EQ. X(4)) GO TO 13	ABCD0246
	IF (X(9) .NE. X(5)) GO TO 23	ABCD0247
	IF (X(8) .EQ. X(4)) GO TO 22	ABCD0248
21	X(9) = X(7)	ABCD0249
	X(8) = X(6)	ABCD0250
	GO TO 13	ABCD0251
22	X(9) = X(7)	ABCD0252
	X(8) = X(6)	ABCD0253
	X(3) = 1.0D0	ABCD0254
	IF (X(9)) 10,11,10	ABCD0255
23	IF (X(8) .EQ. X(4)) GO TO 21	ABCD0256
	F = (X(6) - X(4)) / (X(7) - X(5))	ABCD0257
	A = (X(8) - X(4) - F * (X(9) - X(5))) / ((X(9) - X(7)) * 1 (X(9) - X(5)))	ABCD0258
	B = F - A * (X(5) + X(7))	ABCD0259
	C = X(4) + X(5) * (A * X(7) - F)	ABCD0260
	IF (A .NE. 0.0D0) GO TO 27	ABCD0261
	IF (B .EQ. 0.0D0) GO TO 7	ABCD0262
	Y = -C / B	ABCD0263
	GO TO 47	ABCD0264
27	IF (B .NE. 0.0D0) GO TO 32	ABCD0265
	IF (C .NE. 0.0D0) GO TO 30	ABCD0265
		ABCD0267

	Y = 0.0D0	ABCD0268
	GO TO 47	ABCD0269
30	G = -C / A	ABCD0270
	IF (G .LE. 0.0D0) GO TO 7	ABCD0271
	Y = DSQRT(G)	ABCD0272
	YY = -DSQRT(G)	ABCD0273
	GO TO 37	ABCD0274
32	IF (C .NE. 0.0D0) GO TO 34	ABCD0275
	Y = -B / A	ABCD0276
	YY = 0.0D0	ABCD0277
	GO TO 37	ABCD0278
34	D = 4.0D0 * A * C / B ** 2	ABCD0279
	IF (1.0D0 - D) 13,35,36	ABCD0280
35	Y = -B / (2.0D0 * A)	ABCD0281
	GO TO 47	ABCD0282
36	E = DSQRT(1.0D0 - D)	ABCD0283
	Y = (-B / (2.0D0 * A)) * (1.0D0 + E)	ABCD0284
	YY = (-B / (2.0D0 * A)) * (1.0D0 - E)	ABCD0285
37	J = 4	ABCD0286
	DEPMIN = DABS(X(4))	ABCD0287
	DO 39 I = 6,8,2	ABCD0288
	IF (DEPMIN .LE. DABS(X(I))) GO TO 39	ABCD0289
	J = I	ABCD0290
	DEPMIN = DABS(X(I))	ABCD0291
39	CONTINUE	ABCD0292
	K = J + 1	ABCD0293
	IF (((X(K) - Y) * (X(K) - YY)) .LE. 0.0D0) GO TO 42	ABCD0294
	IF ((DABS(X(K) - Y) - DABS(X(K) - YY)) .LE. 0.0D0) GO TO 47	ABCD0295
	Y = YY	ABCD0296
	GO TO 47	ABCD0297
42	IF (J .GE. 6) GO TO 44	ABCD0298
	JJ = J + 2	ABCD0299
	KK = K + 2	ABCD0300
	GO TO 45	ABCD0301
44	JJ = J - 2	ABCD0302
	KK = K - 2	ABCD0303
45	SLOPE = (X(KK) - X(K)) / (X(JJ) - X(J))	ABCD0304
	IF ((SLOPE * X(J) * (X(K) - Y)) .GT. 0.0D0) GO TO 47	ABCD0305
	Y = YY	ABCD0306
47	X(9) = X(7)	ABCD0307
	X(8) = X(6)	ABCD0308
	X(7) = X(5)	ABCD0309
	X(6) = X(4)	ABCD0310
	GO TO 6	ABCD0311
	END	ABCD0312

Subroutine ATMOS

	SUBROUTINE ATMOS (ZFT,TM,SIGMA,RHO,THETA,DELTA,CA,AMU,K)	ABCD0313
	IMPLICIT REAL*8 (A-H,O-Z)	ABCD0314
	LOGICAL SI	ABCD0315
C	THIS IS A SUBROUTINE TO COMPUTE CERTAIN ELEMENTS OF THE 1962	ABCD0316
C	U.S. STANDARD ATMOSPHERE UP TO 90 KILOMETERS.	ABCD0317
C	CALLING SEQUENCE...	ABCD0318



```
C
C CALL ATMOS (ZFT, TM, SIGMA, RHO, THETA, DELTA, CA, AMU, K)
C ZFT = GEOMETRIC ALTITUDE (FEET)
C TM = MOLECULAR SCALE TEMPERATURE (DEGREES RANKINE)
C SIGMA = RATIO OF DENSITY TO THAT AT SEA LEVEL
C RHO = DENSITY(LB-SEC**2-FT**(-4) OR SLUG-FT**(-3))
C THETA = RATIO OF TEMPERATURE TO THAT AT SEA LEVEL
C DELTA = RATIO OF PRESSURE TO THAT AT SEA LEVEL
C CA = SPEED OF SOUND (FT/SEC)
C AMU = VISCOSITY COEFFICIENT (LB-SEC/FT**2)
C
C K = 1 NORMAL
C      = 2 ALTITUDE LESS THAN -5000 METERS OR GREATER THAN 90 KM
C      = 3 FLOATING POINT OVEFLOW
C
C ALL DATA AND FUNDAMENTAL CONSTANTS ARE IN THE METRIC SYSTEM AS
C THESE QUANTITIES ARE DEFINED AS EXACT IN THIS SYSTEM.
C
C THE RADIUS OF THE EARTH (REFT59) IS THE VALUE ASSOCIATED WITH THE
C 1959 ARDC ATMOSPHERE SO THAT PROGRAMS CURRENTLY USING THE LIBRARY
C ROUTINE WILL NOT REQUIRE ALTERATION TO USE THIS ROUTINE.
C   COMMON /COMALL/ COM(1062)
C   DIMENSION HB(10), TMB(10), DELTAB(10), ALM(10)
C   EQUIVALENCE (SI, COM(1055))
C   DATA HB / -5.0D0, 0.0D0, 11.0D0, 20.0D0, 32.0D0, 47.0D0, 52.0D0,
1 61.0D0, 79.0D0, 88.743D0 /
C   DATA TMB / 320.65D0, 288.15D0, 2 * 216.65D0, 228.65D0,
1 2 * 270.65D0, 252.65D0, 2 * 180.65D0 /
C   DATA DELTAB / 1.75363D+00, 1.00000D+00, 2.23361D-01, 5.40328D-02,
1 8.56663D-03, 1.09455D-03, 5.82289D-04, 1.79718D-04, 1.0241D-05,
2 1.6223D-06 /
C   DATA ALM / 2 * -6.5D0, 0.0D0, 1.0D0, 2.8D0, 0.0D0, -2.0D0,
1 -4.0D0, 2 * 0.0D0 /
C   DATA REFT59/2.0855531D+07/, GZ /9.80665D+00/,
1 AMZ /2.89644D+01 /, RSTAR /8.31432D+00/,
2 FTTOKM/3.048D-04 /, S /1.104D+02 /,
3 AMUZ /1.2024D-05 /, CAZ /1.11645D+03/,
4 RHOZ /7.6474D-02 /, GZENG /3.21741D+01/
C CONVERT GEOMETRIC ALTITUDE TO GEOPOTENTIAL ALTITUDE
C IF IN SI UNITS, CHANGE ZFT TO FEET
C IF (SI) ZFT = ZFT * 3.280833D0
C HFT = (REFT59 / (REFT59 + ZFT)) * ZFT
C CONVERT HFT AND ZFT TO KILOMETERS
C Z = FTTOKM * ZFT
C H = FTTOKM * HFT
C K = 1
C TMZ = TMB(2)
C IF (H.LT. -5.0D0 .OR. Z.GT. 90.0D0) GO TO 7
C DO 1 M = 1,10
C IF (H - HB(M)) 2,3,1
1 CONTINUE
C GO TO 7
2 M = M - 1
3 DELH = H - HB(M)
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ABCD0319
ABCD0320
ABCD0321
ABCD0322
ABCD0323
ABCD0324
ABCD0325
ABCD0326
ABCD0327
ABCD0328
ABCD0329
ABCD0330
ABCD0331
ABCD0332
ABCD0333
ABCD0334
ABCD0335
ABCD0336
ABCD0337
ABCD0338
ABCD0339
ABCD0340
ABCD0341
ABCD0342
ABCD0343
ABCD0344
ABCD0345
ABCD0346
ABCD0347
ABCD0348
ABCD0349
ABCD0350
ABCD0351
ABCD0352
ABCD0353
ABCD0354
ABCD0355
ABCD0356
ABCD0357
ABCD0358
ABCD0359
ABCD0360
ABCD0361
ABCD0362
ABCD0363
ABCD0364
ABCD0365
ABCD0366
ABCD0367
ABCD0368
ABCD0369
ABCD0370
ABCD0371
ABCD0372

	IF (ALM(M) .EQ. 0.0D0) GO TO 4	ABCD0373
	TMK = TMB(M) + ALM(M) * DELH	ABCD0374
C	GRADIENT IS NON ZERO, PAGE 10, EQUATION I.2.10-(3)	ABCD0375
	DELTA = DELTAB(M) * ((TMB(M) / TMK) ** (GZ * AMZ /	ABCD0376
	1 (RSTAR * ALM(M))))	ABCD0377
	GO TO 5	ABCD0378
4	TMK = TMB(M)	ABCD0379
C	GRADIENT IS ZERO, PAGE 10, EQUATION I.2.10-(4)	ABCD0380
	DELTA = DELTAB(M) * DEXP(-GZ * AMZ * DELH / (RSTAR * TMB(M)))	ABCD0381
5	THETA = TMK / TMZ	ABCD0382
	SIGMA = DELTA / THETA	ABCD0383
	ALPHA = DSQRT(THETA ** 3) * ((TMZ + S) / (TMK + S))	ABCD0384
C	CONVERSION TO ENGLISH UNITS	ABCD0385
	TM = 1.8D0 * TMK	ABCD0386
	RHO = RHOZ * SIGMA / GZENG	ABCD0387
	CA = CAZ * DSQRT(THETA)	ABCD0388
	AMU = AMUZ * ALPHA / GZENG	ABCD0389
	IF (SI) GO TO 100	ABCD0390
	GO TO 101	ABCD0391
100	TM = TM / 1.8D0	ABCD0392
	RHO = RHO * 515.379D0	ABCD0393
	CA = CA * .3048D0	ABCD0394
	AMU = AMU * 47.880258D0	ABCD0395
	ZFT = ZFT / 3.280833D0	ABCD0396
	IF IN SI UNITS:	ABCD0397
C	TM DEGREES KELVIN	ABCD0398
C	RHO KG/M**2	ABCD0399
C	CA M/SEC	ABCD0400
C	AMU (N-SEC)/M**2	ABCD0401
C	ZFT M	ABCD0402
101	CALL OVERFL (J)	ABCD0403
	IF (J .EQ. 2) RETURN	ABCD0404
	K = K + 2	ABCD0405
	RETURN	ABCD0406
7	K = 2	ABCD0407
	RETURN	ABCD0408
	END	ABCD0409

Block Data

	BLOCK DATA	ABCD0410
	IMPLICIT REAL*8 (A-H,O-Z)	ABCD0411
C	THESE ARE THE GENERALIZED MAPS FOR AN UNREALISTIC SUPERSONIC	ABCD0412
C	ENGINE. THEY INCLUDE: FAN, INTERMEDIATE FAN, COMPRESSOR,	ABCD0413
C	COMBUSTOR, AND HIGH, INTERMEDIATE AND LOW TURBINES.	ABCD0414
	COMMON /COMDAT/ COMD(5423)	ABCD0415
	DIMENSION CNXF(15), PRXF(15,15), WACXF(15,15), ETAXF(15,15),	ABCD0416
1	NPTF(15)	ABCD0417
	DIMENSION CNXIN(15), PRXIN(15,15), WACXIN(15,15), ETAXIN(15,15),	ABCD0418
1	NPTI(15)	ABCD0419
	DIMENSION CNXP(15), PRXP(15,15), WACXP(15,15), ETAXP(15,15),	ABCD0420
1	NPTP(15)	ABCD0421
	DIMENSION PSIXB(15), DELXB(15,15), ETAXB(15,15), NPTB(15)	ABCD0422
	DIMENSION TFFXH(15), CNXH(15,15), DHTCXH(15,15), ETATXH(15,15),	ABCD0423

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1 NPTTFH(15)                                ABCD0424
  DIMENSION TFFXI(15), CNXI(15,15), DHTCXI(15,15), ETATXI(15,15), ABCD0425
1 NPTTFI(15)                                ABCD0426
  DIMENSION CNXI1(15,14), CNXI2(15,1)        ABCD0427
  DIMENSION TFFXL(15), CNXL(15,15), DHTCXL(15,15), ETATXL(15,15), ABCD0429
1 NPTTFL(15)                                ABCD0429
  DIMENSION CNXL1(15,14), CNXL2(15,1)        ABCD0430
  EQUIVALENCE (CNXF(1), COMD(1)), (PRXF(1,1), COMD(16)), ABCD0431
1 (WACXF(1,1), COMD(241)), (ETAXF(1,1), COMD(466)), ABCD0432
2 (NCNF, COMD(5296)), (NPTF(1), COMD(5297))   ABCD0433
  EQUIVALENCE (CNXIN(1), COMD(691)), (PRXIN(1,1), COMD(706)), ABCD0434
1 (WACXIN(1,1), COMD(931)), (ETAXIN(1,1), COMD(1156)), ABCD0435
2 (NCNI, COMD(5312)), (NPTI(1), COMD(5313))   ABCD0436
  EQUIVALENCE (CNXP(1), COMD(2071)), (PRXP(1,1), COMD(2086)), ABCD0437
1 (WACXP(1,1), COMD(2311)), (ETAXP(1,1), COMD(2536)), ABCD0438
2 (NCNP, COMD(5344)), (NFTP(1), COMD(5345))   ABCD0439
  EQUIVALENCE (PSIXB(1), COMD(2761)), (DELXB(1,1), COMD(2776)), ABCD0440
1 (ETAXB(1,1), COMD(3001)), (NPSB, COMD(5360)), ABCD0441
2 (NPTB(1), COMD(5361))                      ABCD0442
  EQUIVALENCE (TFFXH(1), COMD(3226)), (CNXH(1,1), COMD(3241)), ABCD0443
1 (DHTCXH(1,1), COMD(3466)), (ETATXH(1,1), COMD(3691)), ABCD0444
2 (NTFFSH, COMD(5376)), (NPITFH(1), COMD(5377)) ABCD0445
  EQUIVALENCE (TFFXI(1), COMD(3916)), (CNXI(1,1), COMD(3931)), ABCD0446
1 (DHTCXI(1,1), COMD(4156)), (ETATXI(1,1), COMD(4381)), ABCD0447
2 (NTFFSI, COMD(5392)), (NPTTFI(1), COMD(5393)) ABCD0448
  EQUIVALENCE (CNXI(1,1), CNXI1(1,1)), (CNXI(1,15), CNXI2(1,1)) ABCD0449
  EQUIVALENCE (TFFXL(1), COMD(4606)), (CNXL(1,1), COMD(4621)), ABCD0450
1 (DHTCXL(1,1), COMD(4846)), (ETATXL(1,1), COMD(5071)), ABCD0451
2 (NTFFSL, COMD(5408)), (NPTTFL(1), COMD(5409)) ABCD0452
  EQUIVALENCE (CNXL(1,1), CNXL1(1,1)), (CNXL(1,15), CNXL2(1,1)) ABCD0453
  DATA NCNF, NPTF / 10, 6, 3 * 7, 5 * 10, 8, 5 * 0 / ABCD0454
  DATA CNXF / .3, .4, .5, .6, .7, .3, .9, 1.0, 1.1, 1.2, 5 * 0.0 / ABCD0455
  DATA PRXF / ABCD0456
1 10 * 1.0, 5 * 0.0, 1.012, 1.02, 1.0256, 1.0368, 1.064, 1.1, ABCD0457
2 1.076, 1.044, 1.104, 1.1632, 5 * 0.0, 1.028, 1.04, 1.0512, 1.068, ABCD0458
3 1.1184, 1.16, 1.152, 1.1352, 1.22, 1.312, 5 * 0.0, 1.0384, ABCD0459
4 1.0584, 1.08, 1.124, 1.148, 1.2, 1.2192, 1.2208, 1.324, 1.4, ABCD0460
5 5 * 0.0, 1.0448, 1.0752, 1.116, 1.16, 1.184, 1.228, 1.26, 1.2944, ABCD0461
6 1.4, 1.48, 5 * 0.0, 1.048, 1.092, 1.132, 1.1896, 1.2096, 1.2552, ABCD0462
7 1.2896, 1.34, 1.448, 1.54, 6 * 0.0, 1.1, 1.148, 1.1952, 1.2176, ABCD0463
8 1.272, 1.3312, 1.4, 1.5, 1.56, 9 * 0.0, 1.224, 1.2864, 1.3616, ABCD0464
9 1.428, 1.5336, 1.66, 9 * 0.0, 1.244, 1.3024, 1.3912, 1.448, ABCD0465
1 1.568, 10 * 0.0, 1.2672, 1.332, 1.4, 1.48, 1.584, 81 * 0.0 / ABCD0466
  DATA WACXF / ABCD0467
1 243.6, 286.8, 332.6, 383.4, 439.8, 499.8, 566.4, 633.6, 700.2, ABCD0468
2 750.0, 5 * 0.0, 229.8, 270.0, 322.8, 376.2, 436.8, 499.8, 566.4, ABCD0469
3 633.6, 700.2, 750.0, 5 * 0.0, 199.8, 253.2, 310.2, 358.2, 428.4, ABCD0470
4 493.2, 566.4, 633.6, 700.2, 750.0, 5 * 0.0, 166.8, 233.4, 291.6, ABCD0471
5 340.2, 420.6, 495.4, 559.8, 633.0, 700.2, 750.0, 5 * 0.0, 133.2, ABCD0472
6 209.4, 259.8, 313.2, 406.8, 476.4, 553.2, 625.8, 700.2, 750.0, ABCD0473
7 5 * 0.0, 86.4, 183.6, 240.0, 276.6, 393.6, 466.8, 544.8, 616.8, ABCD0474
8 693.4, 750.0, 6 * 0.0, 156.6, 213.6, 266.4, 388.2, 456.6, 528.6, ABCD0475
9 600.0, 693.6, 749.4, 9 * 0.0, 383.4, 448.2, 509.4, 586.8, 683.4, ABCD0476
1 736.8, 9 * 0.0, 368.4, 433.2, 483.6, 576.6, 666.6, 10 * 0.0, ABCD0477

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2 342.6, 406.8, 474.0, 553.2, 656.4, 81 * 0.0 / ABCD0473
 DATA ETAXF / ABCD0479
 1 2 * .75592, .75064, .74536, .72512, .68816, .64152, .60016, ABCD0480
 2 .56936, .51744, 5 * 0.0, .7612, 5 * .77616, .72512, 3 * .64152, ABCD0481
 3 5 * 0.0, .76648, .792, .80256, 3 * .82808, .77616, 3 * .72512, ABCD0482
 4 5 * 0.0, .75592, .79728, .82808, 3 * .85448, .82808, 2 * .77616, ABCD0483
 5 .75592, 5 * 0.0, .72512, .80256, .84392, 3 * .88, .85888, .82808, ABCD0484
 6 .80256, .7612, 5 * 0.0, .64152, .77616, 2 * .82808, 2 * .90112, ABCD0485
 7 .88, .85888, .80784, .75064, 5 * 0.0, .74008, .77616, .80784, ABCD0486
 8 .90376, .9108, .90112, .88, .80256, .72512, 9 * 0.0, 2 * .90112, ABCD0487
 9 .88, .85888, .77616, .64152, 9 * 0.0, 2 * .88, 2 * .82808, ABCD0488
 1 .74536, 10 * 0.0, .82808, .8272, .81752, .78672, .72512, ABCD0489
 2 81 * 0.0 / ABCD0490
 DATA NCNI, NPTI / 10, 6, 3 * 7, 5 * 10, 8, 5 * 0 / ABCD0491
 DATA CNXIN / .3, .4, .5, .6, .7, .8, .9, 1.0, 1.1, 1.2, 5 * 0.0 / ABCD0492
 DATA PRXIN / ABCD0493
 1 10 * 1.0, 5 * 0.0, 1.018, 1.03, 1.0384, 1.0552, 1.096, 1.15, ABCD0494
 2 1.114, 1.066, 1.156, 1.2448, 5 * 0.0, 1.042, 1.06, 1.0768, ABCD0495
 3 1.132, 1.1776, 1.24, 1.228, 1.2028, 1.33, 1.468, 5 * 0.0, 1.0576, ABCD0496
 4 1.0876, 1.12, 1.186, 1.222, 1.3, 1.3288, 1.3312, 1.486, 1.6, ABCD0497
 5 5 * 0.0, 1.0672, 1.1128, 1.174, 1.24, 1.276, 1.342, 1.39, 1.4416, ABCD0498
 6 1.6, 1.72, 5 * 0.0, 1.072, 1.138, 1.198, 1.2844, 1.3144, 1.3828, ABCD0499
 7 1.4344, 1.51, 1.672, 1.81, 6 * 0.0, 1.15, 1.222, 1.2928, 1.3264, ABCD0500
 8 1.408, 1.4968, 1.6, 1.75, 1.87, 9 * 0.0, 1.336, 1.4296, 1.542, ABCD0501
 9 1.642, 1.8004, 1.99, 9 * 0.0, 1.366, 1.4536, 1.5868, 1.672, ABCD0502
 1 1.852, 10 * 0.0, 1.4008, 1.493, 1.6, 1.72, 1.876, 81 * 0.0 / ABCD0503
 DATA WAXIN / ABCD0504
 1 121.8, 143.4, 166.8, 191.7, 219.9, 249.9, 283.2, 316.8, 350.1, ABCD0505
 2 375.0, 5 * 0.0, 114.9, 135.0, 161.4, 188.1, 218.4, 249.9, 283.2, ABCD0506
 3 316.8, 350.1, 375.0, 5 * 0.0, 99.9, 126.6, 155.1, 179.1, 214.2, ABCD0507
 4 246.6, 283.2, 316.8, 350.1, 375.0, 5 * 0.0, 83.4, 116.7, 145.8, ABCD0508
 5 170.1, 210.3, 242.7, 279.9, 316.5, 350.1, 375.0, 5 * 0.0, 66.6, ABCD0509
 6 104.7, 129.9, 156.6, 203.4, 238.2, 276.6, 312.9, 350.1, 375.0, ABCD0510
 7 5 * 0.0, 43.2, 91.8, 120.0, 133.3, 196.8, 233.4, 272.4, 308.4, ABCD0511
 8 349.2, 375.0, 6 * 0.0, 78.3, 106.8, 133.2, 194.1, 228.3, 264.3, ABCD0512
 9 300.0, 346.8, 374.7, 9 * 0.0, 191.7, 224.1, 254.7, 293.4, 341.7, ABCD0513
 1 368.4, 9 * 0.0, 184.2, 216.6, 241.8, 288.3, 333.3, 10 * 0.0, ABCD0514
 2 171.3, 203.4, 237.0, 276.6, 328.2, 81 * 0.0 / ABCD0515
 DATA ETAXIN / ABCD0516
 1 2 * .75592, .75064, .74536, .72512, .68816, .64152, .60016, ABCD0517
 2 .56936, .51744, 5 * 0.0, .7612, 5 * .77616, .72512, 3 * .64152, ABCD0518
 3 5 * 0.0, .76648, .792, .80256, 3 * .82808, .76616, 3 * .72512, ABCD0519
 4 5 * 0.0, .75592, .79728, .82808, 3 * .85448, .82808, 2 * .77616, ABCD0520
 5 .75592, 5 * 0.0, .72512, .80256, .84392, 3 * .88, .85888, .82808, ABCD0521
 6 .80256, .7612, 5 * 0.0, .64152, .77616, 2 * .82808, 2 * .90112, ABCD0522
 7 .88, .85888, .80784, .75064, 5 * 0.0, .74008, .77616, .80784, ABCD0523
 8 .90376, .9108, .90112, .88, .80256, .72512, 9 * 0.0, 2 * .90112, ABCD0524
 9 .88, .85888, .77616, .64152, 9 * 0.0, 2 * .88, 2 * .82808, ABCD0525
 1 .74536, 10 * 0.0, .82808, .8272, .81752, .78672, .72512, ABCD0526
 2 81 * 0.0 / ABCD0527
 DATA NCNP, NPTP / 10, 2 * 6, 2 * 8, 4 * 10, 2 * 8, 5 * 0 / ABCD0528
 DATA CNXP / .562, .674, .787, .899, 1.0, 1.034, 1.067, 1.124, ABCD0529
 1 1.236, 1.292, 5 * 0.0 / ABCD0530
 DATA PRXP / ABCD0531

1 10 * 1.0, 5 * 0.0, 1.84, 1.966, 1.84, 2.008, 2.519, 2.855, 3.261, ABCD0532
2 1.686, 4.353, 3.765, 5 * 0.0, 2.428, 3.093, 2.68, 3.429, 3.982, ABCD0533
3 4.297, 4.759, 3.849, 7.622, 6.481, 5 * 0.0, 2.869, 3.933, 3.408, ABCD0534
4 4.605, 5.277, 5.613, 6.117, 5.466, 10.219, 9.176, 5 * 0.0, 3.835, ABCD0535
5 4.689, 4.521, 5.697, 6.488, 6.936, 7.454, 6.866, 11.059, 10.219, ABCD0536
6 5 * 0.0, 4.549, 5.529, 5.445, 6.614, 7.202, 7.622, 8.308, 8.371, ABCD0537
7 11.899, 11.479, 7 * 0.0, 6.313, 7.538, 8.0, 8.546, 9.218, 8.966, ABCD0538
8 13.159, 12.711, 7 * 0.0, 6.523, 7.958, 8.567, 9.134, 9.638, ABCD0539
9 9.883, 13.656, 14.412, 9 * 0.0, 9.386, 9.925, 10.513, 10.912, ABCD0540
1 11 * 0.0, 9.596, 10.219, 10.936, 11.815, 82 * 0.0 / ABCD0541
DATA WACXP / ABCD0542
1 51.0, 59.3, 70.0, 84.8, 101.7, 103.1, 114.5, 122.9, 139.8, 146.2, ABCD0543
2 5 * 0.0, 50.2, 59.3, 70.0, 84.8, 101.7, 108.1, 114.5, 122.9, ABCD0544
3 139.8, 146.2, 5 * 0.0, 49.5, 58.8, 70.0, 84.8, 101.7, 108.1, ABCD0545
4 114.5, 122.9, 139.8, 146.2, 5 * 0.0, 48.8, 57.9, 69.5, 84.8, ABCD0546
5 101.7, 108.1, 114.5, 122.9, 139.8, 146.2, 5 * 0.0, 46.7, 56.7, ABCD0547
6 68.8, 84.0, 101.2, 107.6, 114.5, 122.9, 139.8, 146.2, 5 * 0.0, ABCD0548
7 44.5, 55.0, 67.9, 83.3, 101.0, 107.1, 114.3, 122.9, 139.5, 146.2, ABCD0549
8 7 * 0.0, 66.4, 81.7, 100.0, 106.7, 113.6, 122.6, 139.3, 146.2, ABCD0550
9 7 * 0.0, 65.7, 80.5, 99.5, 105.0, 113.3, 122.1, 139.0, 146.2, ABCD0551
1 9 * 0.0, 98.1, 104.5, 112.6, 121.7, 11 * 0.0, 97.4, 104.0, 112.4, ABCD0552
2 120.7, 82 * 0.0 / ABCD0553
DATA ETAXP / ABCD0554
1 2 * .59082, .58566, .5805, .5719, .57018, .55986, .53922, .47644, ABCD0555
2 .46612, 5 * 0.0, .62178, 6 * .64242, .57018, .60114, .57018, ABCD0556
3 5 * 0.0, .64242, .69402, .6837, 4 * .72498, .64242, .72498, ABCD0557
4 .64242, 5 * 0.0, .65274, 2 * .72498, 4 * .77744, .72498, .77744, ABCD0558
5 .72498, 5 * 0.0, .67338, .74552, .77744, 4 * .8084, .77744, ABCD0559
6 .7826, .75078, 5 * 0.0, .64242, .72498, .79292, .82904, ABCD0560
7 3 * .83936, .8084, .77744, .75078, 7 * 0.0, .77744, .9084, ABCD0561
8 2 * .86, .84968, .82388, 2 * .72498, 7 * 0.0, .7697, .79292, ABCD0562
9 4 * .83936, .69918, .64242, 9 * 0.0, 4 * .8084, 11 * 0.0, .80582, ABCD0563
1 .8041, .79808, .77744, 82 * 0.0 / ABCD0564
DATA NPSB, NPTB / 15, 15 * 15 / ABCD0565
DATA PSIXB / 4.9116, 9.8232, 14.735, 19.646, 24.558, 29.47, ABCD0566
1 34.381, 39.293, 44.207, 73.674, 100.0, 200.0, 300.0, 400.0, ABCD0567
2 500.0 / ABCD0568
DATA DELXB / 15 * 200.0, 15 * 300.0, 15 * 400.0, 15 * 500.0, ABCD0569
1 15 * 600.0, 15 * 700.0, 15 * 800.0, 15 * 900.0, 15 * 1000.0, ABCD0570
2 15 * 1100.0, 15 * 1200.0, 15 * 1300.0, 15 * 1400.0, 15 * 1500.0, ABCD0571
3 15 * 1600.0 / ABCD0572
DATA ETAXB / ABCD0573
1 .6, .758, .868, .925, .95, .933, 9 * 1.0, .726, .825, .893, .936, ABCD0574
2 .966, .991, 9 * 1.0, .777, .858, .911, .946, .972, .992, 9 * 1.0, ABCD0575
3 .806, .875, .925, .955, .977, .994, 9 * 1.0, .826, .888, .935, ABCD0576
4 .933, .982, .995, 9 * 1.0, .843, .898, .942, .969, .985, .997, ABCD0577
5 9 * 1.0, .855, .906, .947, .974, .99, .998, 9 * 1.0, .865, .912, ABCD0578
6 .951, .977, .992, .999, 9 * 1.0, .87, .914, .953, .978, .993, ABCD0579
7 2 * .999, 8 * 1.0, .87, .915, .953, .979, .995, 2 * .999, ABCD0580
8 8 * 1.0, .87, .915, .953, .979, .995, 2 * .999, 8 * 1.0, .87, ABCD0581
9 .915, .953, .979, .995, 2 * .999, 8 * 1.0, .87, .915, .953, .979, ABCD0582
1 .995, 2 * .999, 8 * 1.0, .87, .915, .953, .979, .995, 2 * .999, ABCD0583
2 8 * 1.0, .87, .915, .953, .979, .995, 2 * .999, 8 * 1.0 / ABCD0584
DATA NTFFSH, NPTTFH / 10, 9 * 15, 12, 5 * 0 / ABCD0585

DATA TFFXH / 39.67, 42.99, 47.46, 48.61, 49.175, 49.6, 50.0,	ABCD0586
1 50.425, 50.92, 51.575, 5 * 0.0 /	ABCD0587
DATA CNXH /	ABCD0588
1 10 * .1872, 5 * 0.0, .3372, .3942, .4362, .255, .3, .3568, .4314,	ABCD0589
2 .4834, .3372, .2814, 5 * 0.0, .5156, .5814, .6568, .4784, .5254,	ABCD0590
3 .6196, .6844, .7314, .5344, .3304, 5 * 0.0, 2 * .7128, .8726,	ABCD0591
4 .6942, .75, .8628, .9568, .8814, .6754, .4686, 5 * 0.0, .9382,	ABCD0592
5 .8442, 1.0696, .9148, .9754, 1.0932, 1.2010, 1.0226, .8069,	ABCD0593
6 .5628, 5 * 0.0, 1.1442, .9804, 1.2382, 1.1442, 1.2754, 1.2852,	ABCD0594
7 1.3834, 1.1442, .9196, .6382, 5 * 0.0, 1.3138, 1.1068, 1.4638,	ABCD0595
8 1.3882, 1.4824, 1.501, 1.5108, 1.2804, 1.0128, .6892, 5 * 0.0,	ABCD0596
9 1.5382, 1.2754, 1.6882, 1.5618, 1.7638, 1.6882, 1.6186, 1.3696,	ABCD0597
1 1.1254, .7362, 5 * 0.0, 1.7264, 1.445, 1.9696, 1.801, 2.045,	ABCD0598
2 1.9138, 1.745, 1.4638, 1.2196, .7696, 5 * 0.0, 1.9324, 1.7068,	ABCD0599
3 2.2138, 1.9794, 2.3362, 2.1245, 1.8618, 1.595, 1.3138, .8068,	ABCD0600
4 5 * 0.0, 2.15, 1.9696, 2.552, 2.2794, 2.645, 2.2706, 1.9558,	ABCD0601
5 1.6746, 1.3696, .8254, 5 * 0.0, 2.4058, 2.2706, 2.805, 2.5138,	ABCD0602
6 2.8706, 2.4226, 2.0, 1.745, 1.4068, .8304, 5 * 0.0, 2.5892,	ABCD0603
7 2.697, 3.0392, 2.8334, 3.0764, 2.495, 2.045, 1.801, 1.445,	ABCD0604
8 6 * 0.0, 2.7862, 3.096, 3.2648, 3.1422, 3.152, 2.5372, 2.0824,	ABCD0605
9 1.8156, 1.4638, 6 * 0.0, 2.945, 3 * 3.3774, 3.1618, 2.5558,	ABCD0606
1 2.101, 1.8196, 1.4676, 6 * 0.0 /	ABCD0607
DATA DHTCXH /	ABCD0608
1 .0032, .0038, .0046, .0052, .0056, .0068, .008, .0088, .0093,	ABCD0609
2 .0132, 5 * 0.0, .0057, .008, .01, .0068, .0088, .012, .0164,	ABCD0610
3 .0196, .0159, .018, 5 * 0.0, .0084, .0113, .0144, .012, .0144,	ABCD0611
4 .0192, .0236, .0272, .0232, .0223, 5 * 0.0, .0108, .0136, .0184,	ABCD0612
5 .0164, .0192, .0252, .0308, .0316, .0284, .0268, 5 * 0.0, .0133,	ABCD0613
6 .0156, .0216, .0204, .0236, .03, .0372, .0356, .033, .0314,	ABCD0614
7 5 * 0.0, .0152, .0176, .024, .0244, .0288, .034, .0416, .0392,	ABCD0615
8 .0368, .0352, 5 * 0.0, .0164, .0192, .0268, .028, .0321, .0384,	ABCD0616
9 .0448, .0432, .04, .038, 5 * 0.0, .0174, .0212, .0292, .0304,	ABCD0617
1 .036, .0421, .0476, .046, .0442, .0412, 5 * 0.0, .0179, .0228,	ABCD0618
2 .0316, .0336, .04, .0472, .051, .0488, .048, .044, 5 * 0.0,	ABCD0619
3 .0176, .0248, .0331, .0356, .0444, .0524, .0544, .0528, .0524,	ABCD0620
4 .0476, 5 * 0.0, .0167, .026, .0344, .0388, .0496, .0564, .0576,	ABCD0621
5 .056, .0556, .0504, 5 * 0.0, .0144, .0261, .0346, .0412, .054,	ABCD0622
6 .0612, .06, .0596, .058, .053, 5 * 0.0, .012, .0241, .034, .0441,	ABCD0623
7 .0596, .064, .0624, .064, .0612, 6 * 0.0, .0082, .0188, .0324,	ABCD0624
8 .0472, .064, .0668, .066, .0654, .064, 6 * 0.0, .0034, .0128,	ABCD0625
9 .0312, .0494, .0661, .0698, .07, .0693, .0668, 5 * 0.0 /	ABCD0626
DATA ETATXH /	ABCD0627
1 .6219, .6068, .5764, .5643, .5562, .5309, .5062, .5051, .4909,	ABCD0628
2 .4257, 5 * 0.0, 3 * .7078, 5 * .6068, .538, .4747, 5 * 0.0,	ABCD0629
3 .7868, 2 * .809, 5 * .7073, .5053, .5056, 5 * 0.0, .809, .8292,	ABCD0630
4 .8494, 4 * .809, .7665, .6573, .5359, 5 * 0.0, .809, .8363,	ABCD0631
5 .8543, 4 * .8494, .809, .7073, .5683, 5 * 0.0, .7963, .8393,	ABCD0632
6 .8515, .8596, 3 * .8697, .8292, .7463, .5941, 5 * 0.0, .7779,	ABCD0633
7 .8368, .8494, .8596, .8695, .8319, .8797, .8494, .7776, .6068,	ABCD0634
8 5 * 0.0, .7422, .8302, .8409, .8575, .8662, 2 * .8899, .9596,	ABCD0635
9 .809, .6178, 5 * 0.0, .7078, .8254, .8262, .8535, .8615, .894,	ABCD0636
1 .8954, .8697, .8191, .624, 5 * 0.0, .7635, 2 * .809, .8494,	ABCD0637
2 .8555, .8969, .9, .8808, .8302, .531, 5 * 0.0, .6068, .7696,	ABCD0638
3 .7579, .8363, .852, .8975, .901, .8848, .8347, .6265, 5 * 0.0,	ABCD0639

4 .5309, 2 * .7078, .8262, .8494, .8976, .9, .8848, .9363, .6118, ABCD0640
 5 5 * 0.0, .4773, .6068, .5652, .909, .8494, .8968, .998, .8789, ABCD0641
 6 .8322, 6 * 0.0, .4045, .5056, .6068, .7797, .8532, .8937, .8925, ABCD0642
 7 .8697, .8241, 6 * 0.0, .3034, .4197, .5865, .7584, .857, .8896, ABCD0643
 8 .8793, .859, .809, 6 * 0.0 / ABCD0644
 DATA NTFFSI, NPTTFI / 11, 9 * 15, 12, 9, 4 * 0 / ABCD0645
 DATA TFFXI / 70.776, 82.236, 93.468, 103.464, 112.836, 116.58, ABCD0646
 1 120.0, 122.676, 125.124, 127.324, 130.536, 4 * 0.0 / ABCD0647
 DATA CNXI1 / ABCD0648
 1 11 * .3522, 4 * 0.0, .5104, .5278, .5654, .4052, .4844, .5896, ABCD0649
 2 .7392, .5808, .5278, .4574, .4226, 4 * 0.0, .7044, .7575, .8279, ABCD0650
 3 .6514, .7044, .8008, .9689, .7575, .634, .6167, .5278, 4 * 0.0, ABCD0651
 4 .933, 1.0208, 1.0296, .8452, .933, 1.0567, 1.2109, .933, .7922, ABCD0652
 5 .7218, .6167, 4 * 0.0, 1.1618, 1.2322, 1.1975, 1.0567, 2 * 1.2322, ABCD0653
 6 1.4089, 1.1801, .9689, .3279, .7044, 4 * 0.0, 1.3556, 1.3818, ABCD0654
 7 1.373, 1.2322, 1.4967, 1.4619, 1.6056, 1.3915, 1.1183, .933, ABCD0655
 8 .7922, 4 * 0.0, 1.5497, 1.6201, 1.5497, 1.4434, 1.6548, 1.6722, ABCD0656
 9 1.7609, 1.5671, 1.1801, 1.0567, .8452, 4 * 0.0, 1.6905, 1.813, ABCD0657
 1 1.7609, 1.6722, 1.8834, 1.866, 1.9367, 1.7609, 1.3209, 1.1493, ABCD0658
 2 .8983, 4 * 0.0, 1.9367, 1.9723, 1.9367, 1.954, 2.0071, 2.1171, ABCD0659
 3 2.0948, 1.866, 1.4619, 1.2148, .9293, 4 * 0.0, 2.1835, 2.1305, ABCD0660
 4 2.1479, 2.1131, 2.1652, 2.3245, 2.2, 1.9897, 1.5497, 1.2505, ABCD0661
 5 5 * 0.0, 2.3593, 2.2715, 2.3245, 2.2715, 2.3274, 2.5357, 2.2889, ABCD0662
 6 2.0601, 1.6722, 1.2784, 5 * 0.0, 2.5001, 2.5089, 2.4827, 2.4915, ABCD0663
 7 2.5531, 2.7375, 2.3949, 2.1131, 1.7609, 1.2824, 5 * 0.0, 2.6941, ABCD0664
 8 2.7471, 2.6583, 2.7471, 2.8175, 3.0019, 2.4471, 2.1652, 1.813, ABCD0665
 9 6 * 0.0, 2.8175, 2 * 2.9227, 2.9931, 3.0461, 3.1167, 2.5001, ABCD0666
 1 2.2009, 1.8315, 6 * 0.0 / ABCD0667
 DATA CNXI2 / ABCD0668
 1 6 * 3.1698, 2.5175, 2.2048, 1.8401, 6 * 0.0 / ABCD0669
 DATA DHTCXI / ABCD0670
 1 .0016, .0023, .0027, .0029, .0031, .0034, .0038, .0042, .0047, ABCD0671
 2 .0054, .0061, 4 * 0.0, .0023, .0035, .0045, .0034, .0043, .0057, ABCD0672
 3 .0078, .0069, .007, .0069, .0075, 4 * 0.0, .0031, .0047, .0063, ABCD0673
 4 .0054, .0062, .0076, .0101, .009, .0084, .0092, .0093, 4 * 0.0, ABCD0674
 5 .0038, .0061, .0076, .0069, .0081, .01, .0124, .0109, .0104, ABCD0675
 6 .0107, .0108, 4 * 0.0, .0045, .007, .0087, .0084, .0105, .0114, ABCD0676
 7 .0142, .0135, .0124, .0123, .0124, 4 * 0.0, .0049, .0076, .0098, ABCD0677
 8 .0097, .0124, .0134, .0159, .0156, .0141, .0138, .014, 4 * 0.0, ABCD0678
 9 .0052, .0084, .0107, .0111, .0136, .015, .0173, .0177, .0148, ABCD0679
 1 .0159, .0151, 4 * 0.0, .0054, .0089, .0118, .0124, .0152, .0165, ABCD0680
 2 .019, .0199, .0166, .0177, .0164, 4 * 0.0, .0055, .0092, .0126, ABCD0681
 3 .014, .0159, .0184, .0207, .0213, .0184, .0191, .0177, 4 * 0.0, ABCD0682
 4 .0054, .0094, .0134, .0146, .0169, .0199, .022, .023, .0196, ABCD0683
 5 .0202, 5 * 0.0, .0051, .0095, .0139, .0153, .0178, .0214, .0233, ABCD0684
 6 .0241, 2 * .0214, 5 * 0.0, .0047, .0093, .0142, .0161, .0189, ABCD0685
 7 .0228, .025, .0251, .0232, .0221, 5 * 0.0, .0038, .0089, .0146, ABCD0686
 8 .0168, .0199, .0251, .0261, .0263, .0245, 6 * 0.0, .0031, .0083, ABCD0687
 9 .0147, .0172, .0207, .0267, 2 * .0276, .0255, 6 * 0.0, .0001, ABCD0688
 1 .0068, .0145, .0173, .021, .028, .029, .0283, .0267, 6 * 0.0 / ABCD0689
 DATA ETATXI / ABCD0690
 1 .712, 2 * .8, .7995, .775, .76, .731, .71, .678, .638, .6, ABCD0691
 2 4 * 0.0, .73, .81, .83, 4 * .3, .745, .7, .655, .6, 4 * 0.0, ABCD0692
 3 .7472, .82, .86, .84, .848, .345, .83, .768, .7125, .67, .612, ABCD0693


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4 4 * 0.0, .73, .83, .863, 4 * .86, .8, .735, .685, .617, 4 * 0.0, ABCD0694
5 .714, .83, .867, .868, .875, .873, .875, .838, .769, .7, .621, ABCD0695
6 4 * 0.0, .7, .829, .87, .873, 3 * .89, .86, .8, .711, .6258, ABCD0695
7 4 * 0.0, .685, .81, .872, .88, .8912, .895, .893, .8712, .806, ABCD0697
8 .718, .625, 4 * 0.0, .673, .8, .872, .883, .894, .9, .8975, .878, ABCD0698
9 .8225, .718, .623, 4 * 0.0, .6452, .785, .87, .8835, .8955, ABCD0699
1 .9005, .8999, .88, .8395, .717, .6009, 4 * 0.0, .62, .76, .867, ABCD0700
2 .883, .897, .901, .9, .8775, .845, .714, 5 * 0.0, .6, .745, .86, ABCD0701
3 .88, .8961, .9004, .898, .876, .847, .7, 5 * 0.0, .575, .7, .85, ABCD0702
4 .874, .89, .9, .8937, .8722, .8445, .689, 5 * 0.0, .531, .68, ABCD0703
5 .83, .86, .879, 2 * .89, .866, .833, 6 * 0.0, .5, .645, .8, .835, ABCD0704
6 .8671, .88, .8799, .86, .8235, 6 * 0.0, .385, .59, .76, .82, .86, ABCD0705
7 .8735, .871, .848, .808, 6 * 0.0 / ABCD0705
DATA NTFFSL, NPTTFL / 11, 9 * 15, 12, 9, 4 * 0 / ABCD0707
DATA TFFXL / 88.47, 102.795, 116.835, 129.33, 141.045, 145.725, ABCD0708
1 150.0, 153.345, 156.405, 159.78, 163.17, 4 * 0.0 / ABCD0709
DATA CNXL1 / ABCD0710
1 11 * .3682, 4 * 0.0, .5335, .5518, .5911, .4237, .5065, .6164, ABCD0711
2 .7728, .6072, .5518, .4782, .4419, 4 * 0.0, .7365, .7919, .8655, ABCD0712
3 .681, .7365, .8372, 1.0129, .7919, .6629, .6447, .5518, 4 * 0.0, ABCD0713
4 .9754, 1.0672, 1.0764, .3837, .9754, 1.1047, 1.2659, .9754, ABCD0714
5 .8282, .7546, .6447, 4 * 0.0, 1.2146, 1.2882, 1.2519, 1.1047, ABCD0715
6 2 * 1.2882, 1.4729, 1.2337, 1.0129, .8655, .7365, 4 * 0.0, ABCD0716
7 1.4173, 1.4446, 1.4354, 1.2882, 1.5647, 1.5283, 1.6785, 1.4548, ABCD0717
8 1.1691, .9754, .8282, 4 * 0.0, 1.6201, 1.6937, 1.6201, 1.509, ABCD0718
9 1.7301, 1.7482, 1.8409, 1.6383, 1.2337, 1.1047, .8837, 4 * 0.0, ABCD0719
1 1.7673, 1.8954, 1.8409, 1.7482, 1.969, 1.9509, 2.0247, 1.8409, ABCD0720
2 1.3809, 1.2015, .9391, 4 * 0.0, 2.0247, 2.0619, 2.0247, 2.0429, ABCD0721
3 2.0983, 2.2133, 2.1901, 1.9509, 1.5283, 1.2701, .9715, 4 * 0.0, ABCD0722
4 2.2827, 2.2273, 2.2455, 2.2091, 2.2637, 2.4302, 2.3, 2.0801, ABCD0723
5 1.6201, 1.3073, 5 * 0.0, 2.4655, 2.3747, 2.4302, 2.3747, 2.4332, ABCD0724
6 2.651, 2.3929, 2.1537, 1.7482, 1.3365, 5 * 0.0, 2.6137, 2.6229, ABCD0725
7 2.5956, 2.6047, 2.6691, 2.8619, 2.5038, 2.2091, 1.8409, 1.3407, ABCD0726
8 5 * 0.0, 2.8166, 2.872, 2.7791, 2.872, 2.9456, 3.1384, 2.5583, ABCD0727
9 2.2637, 1.8954, 6 * 0.0, 2.9456, 2 * 3.0555, 3.1291, 3.1846, ABCD0728
1 3.2584, 2.6137, 2.3009, 1.9147, 6 * 0.0 / ABCD0729
DATA CNXL2 / ABCD0730
1 6 * 3.3138, 2.6319, 2.3051, 1.9237, 6 * 0.0 / ABCD0731
DATA DHTCXL / ABCD0732
1 .0018, .0026, .0031, .0033, .0036, .0038, .0044, .0048, .0054, ABCD0733
2 .0061, .0069, 4 * 0.0, .0026, .0039, .0051, .0038, .0049, .0064, ABCD0734
3 .0089, .0078, .008, .0073, .0036, 4 * 0.0, .0035, .0054, .0071, ABCD0735
4 .0061, .0071, .0087, .0115, .0102, .0096, .0104, .0106, 4 * 0.0, ABCD0736
5 .0044, .0069, .0087, .0078, .0092, .0113, .0141, .0124, .0119, ABCD0737
6 .0122, .0123, 4 * 0.0, .0051, .008, .0099, .0096, .0119, .013, ABCD0738
7 .0162, .0153, .0141, .0139, .0141, 4 * 0.0, .0056, .0087, .0111, ABCD0739
8 .011, .0141, .0152, .0181, .0177, .016, .0157, .0159, 4 * 0.0, ABCD0740
9 .0059, .0096, .0122, .0125, .0155, .0171, .0197, .0201, .0169, ABCD0741
1 .0181, .0172, 4 * 0.0, .0061, .0101, .0134, .0141, .0172, .0187, ABCD0742
2 .0216, .0226, .0188, .0201, .0186, 4 * 0.0, .0062, .0104, .0143, ABCD0743
3 .0159, .0181, .0209, .0235, .0242, .0209, .0217, .0201, 4 * 0.0, ABCD0744
4 .0061, .0107, .0152, .0165, .0192, .0226, .025, .0261, .0223, ABCD0745
5 .023, 5 * 0.0, .0057, .0108, .0157, .0174, .0202, .0244, .0265, ABCD0746
6 .0274, 2 * .0244, 5 * 0.0, .0053, .0106, .0162, .0183, .0214, ABCD0747

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7	.0259, .0284, .0285, .0263, .0251, 5 * 0.0, .0044, .0101, .0166,	ABCD0743
8	.0191, .0266, .0286, .0296, .0299, .0279, 6 * 0.0, .0035, .0094,	ABCD0749
9	.0167, .0195, .0235, .0303, 2 * .0314, .0289, 6 * 0.0, .0001,	ABCD0750
1	.0077, .0164, .0197, .0239, .0319, .0329, .0321, .0303, 6 * 0.0 /	ABCD0751
	DATA ETATXL /	ABCD0752
1	.712, 2 * .8, .7995, .775, .76, .731, .71, .678, .639, .6,	ABCD0753
2	4 * 0.0, .73, .81, .83, 4 * .8, .745, .7, .655, .6, 4 * 0.0,	ABCD0754
3	.7472, .82, .86, .84, .848, .845, .83, .768, .7125, .67, .512,	ABCD0755
4	4 * 0.0, .73, .83, .863, 4 * .86, .8, .735, .685, .617, 4 * 0.0,	ABCD0756
5	.714, .83, .867, .868, .875, .873, .875, .838, .769, .7, .621,	ABCD0757
6	4 * 0.0, .7, .829, .87, .873, 3 * .89, .86, .8, .711, .6258,	ABCD0758
7	4 * 0.0, .685, .81, .872, .88, .8912, .895, .893, .8712, .906,	ABCD0759
8	.718, .625, 4 * 0.0, .673, .8, .872, .883, .894, .9, .8975, .878,	ABCD0760
9	.8225, .718, .623, 4 * 0.0, .6452, .785, .87, .8835, .8955,	ABCD0761
1	.9005, .8999, .88, .8395, .717, .6009, 4 * 0.0, .62, .76, .867,	ABCD0762
2	.883, .897, .901, .9, .8775, .845, .714, 5 * 0.0, .6, .745, .86,	ABCD0763
3	.88, .8961, .9004, .898, .875, .847, .7, 5 * 0.0, .575, .7, .85,	ABCD0764
4	.874, .89, .9, .8937, .8722, .8445, .689, 5 * 0.0, .531, .58,	ABCD0765
5	.83, .86, .879, 2 * .89, .866, .833, 6 * 0.0, .5, .645, .8, .835,	ABCD0766
6	.8671, .88, .8799, .86, .8235, 6 * 0.0, .385, .53, .76, .82, .86,	ABCD0767
7	.8735, .871, .848, .808, 6 * 0.0 /	ABCD0768
	END	ABCD0769

Subroutine COAFBN

SUBROUTINE COAFBN	ABCD0770
IMPLICIT REAL*8 (A-H,O-Z)	ABCD0771
LOGICAL SI	ABCD0772
COMMON /COMALL/ COM(1062)	ABCD0773
DIMENSION WORD(2)	ABCD0774
DIMENSION Q(9), AWORD(2)	ABCD0775
EQUIVALENCE (WORD(1), COM(1)), (IDES, COM(3)), (IGASMX, COM(10)),	ABCD0776
1 (IAFTBN, COM(12)), (TOLALL, COM(23)), (WG24, COM(321)), (FAP24,	ABCD0777
2 COM(322)), (WG55, COM(323)), (FAR35, COM(324)), (P6DSAV,	ABCD0778
3 COM(325)), (AM6DSV, COM(326)), (AM6, COM(327)), (A6, COM(328)),	ABCD0779
4 (WG6CDS, COM(329)), (WG6, COM(330)), (T6, COM(331)),	ABCD0780
5 (P6, COM(332)), (H6, COM(333)), (WG7, COM(334)),	ABCD0781
6 (FAR7, COM(335)), (FAR7SV, COM(336)), (TS7, COM(337)),	ABCD0782
7 (PS7, COM(338)), (V7, COM(339)), (AM7, COM(340)), (A7, COM(341)),	ABCD0783
8 (T7DS, COM(342)), (T7, COM(343)), (H7, COM(344)), (S7, COM(345)),	ABCD0784
9 (ETAADS, COM(366)), (DPAFDS, COM(367)), (WFA, COM(368)),	ABCD0785
1 (ETAASV, COM(370)), (DPAFT, COM(371)),	ABCD0786
2 (P7, COM(389)), (U7, COM(390)), (VAFTBN, COM(402)),	ABCD0787
3 (ICOAFB, COM(1045)), (SI, COM(1055))	ABCD0788
DATA AWORD /4HCOAF, 4HEN /	ABCD0789
WORD(1) = AWORD(1)	ABCD0790
WORD(2) = AWORD(2)	ABCD0791
Q(2) = 0.0DC	ABCD0792
Q(3) = 0.0DC	ABCD0793
IF (SI) GO TO 100	ABCD0794
AJ = 778.26D0	ABCD0795
AJX = 2.719D0	ABCD0796
CAPSF = 2116.2170D0	ABCD0797
G = 32.174049D0	ABCD0798

	PRATH = 14.696D0	ABCD0799
	TDEL = 2000.0D0	ABCD0800
	T7MAX = 4000.0D0	ABCD0801
	RA = .0252D0	ABCD0802
	GO TO 101	ABCD0803
100	AJ = 1.0D0	ABCD0804
	AJX = 1.0D0	ABCD0805
	CAPSF = 101325.0D0	ABCD0806
	G = 1.0D0	ABCD0807
	PRATH = 14.696D0 / 101324.6D0	ABCD0808
	TDEL = 1111.0D0	ABCD0809
	T7MAX = 2222.0D0	ABCD0810
	RA = 286.9D0	ABCD0811
101	GAJ2 = 2.0D0 * G * AJ	ABCD0812
	ICOAFB = 0	ABCD0813
C***	P6DS AND AM6DS ARE SET FOR GENERALIZATION OF AFTERBURNER	ABCD0814
C***	EFFICIENCY MAP GENERALIZATION	ABCD0815
	IF (IDES .NE. 1) GO TO 102	ABCD0816
	P6DS = P6 * PRATH	ABCD0817
	AM6DS = AM6	ABCD0818
102	WF6 = FAR55 * WG55 / (FAR55 + 1.0D0)	ABCD0819
	IF (IGASMX .GT. 0) WF6 = WF6 + FAR24 * WG24 / (FAR24 + 1.0D0)	ABCD0820
	WA6 = WG6 - WF6	ABCD0821
C ***	DRY LOSS	ABCD0822
	WG6C = WG6 * DSQRT(T6) / P6	ABCD0823
	IF (IDES .EQ. 1) WG6CDS = WG6C	ABCD0824
	DPAFT = DPAFDS * (WG6C / WG6CDS)	ABCD0825
	IF (DPAFT .GT. 1.0D0) DPAFT = 1.0D0	ABCD0826
	P7 = P6 * (1.0D0 - DPAFT)	ABCD0827
	A7 = A6	ABCD0828
	FAR6 = WF6 / WA6	ABCD0829
	CALL PROCOM (FAR6,T6,XX1,XX2,XX3,XX4,PHI6,XX6)	ABCD0830
	WQA = WG6 / A7	ABCD0831
	C1 = P7 * DSQRT(G / (T6 * AJ)) * CAPSF	ABCD0832
	AM7 = AM6	ABCD0833
	TS7 = 0.875D0 * T6	ABCD0834
1	DO 2 I = 1,50	ABCD0835
	CALL PROCOM (FAR6,TS7,CS7,AK7,CP7,REX7,PHIS7,HS7)	ABCD0836
	V7 = AM7 * CS7	ABCD0837
	HSCAL = H6 - V7 ** 2 / GAJ2	ABCD0838
	DELHS = HSCAL - HS7	ABCD0839
	IF (DABS(DELHS) .LE. .5D0 * TOLALL * HSCAL) GO TO 3	ABCD0840
2	TS7 = TS7 + DELHS / CP7	ABCD0841
	ICOAFB = 1	ABCD0842
	GO TO 14	ABCD0843
3	WQAT = C1 * DSQRT(AK7 / REX7) * AM7 / (1.0D0 + (AK7 - 1.0D0) * 1 AM7 ** 2 / 2.0D0) ** ((AK7 + 1.0D0) / (2.0D0 * (AK7 - 1.0D0)))	ABCD0844
	DIR = WQA / WQAT	ABCD0845
	EW = (WQA - WQAT) / WQA	ABCD0846
	CALL AFQUIR (Q(1),AM7,EW,0.0D0,40.0D0,1.0D0*TOLALL,DIR,AM7T,IGO)	ABCD0847
	ICOAFB = 2	ABCD0848
	GO TO (4,5,14), IGO	ABCD0849
4	AM7 = AM7T	ABCD0850
	IF (AM7 .LE. 0.0D0) AM7 = 1.0D-10	ABCD0851
		ABCD0852

	IF (AM7 .GE. 1.0D0) AM7 = 0.9D0	ABCD0853
	GO TO 1	ABCD0854
5	PS7 = P7 / DEXP((PHI6 - PHIS7) / PEX7)	ABCD0855
	IF (IAFTBN .GT. 0) GO TO 7	ABCD0856
C ***	NON-AFTERBURNING	ABCD0857
6	T7 = T6	ABCD0858
	WFA = 0.0D0	ABCD0859
	FAR7 = FAR6	ABCD0860
	WG7 = WG6	ABCD0861
	IF (IDES .NE. 1 .OR. T7DS .EQ. 0.0D0) GO TO 20	ABCD0862
C ***	AFTERBURNING	ABCD0863
7	IF (IAFTBN .EQ. 2) T7 = T6 + FDEL	ABCD0864
	IF (IDES .EQ. 1) T7 = T7DS	ABCD0865
	IF (T7 .LE. T6) GO TO 6	ABCD0866
	RHO65 = CAPSF * PS7 / (AJ * REX7 * TS7)	ABCD0867
	PS65 = PS7	ABCD0868
	V65 = V7	ABCD0869
	Q(2) = 0.0D0	ABCD0870
	Q(3) = 0.0D0	ABCD0871
8	IF (T7 .GT. T7MAX) T7 = T7MAX	ABCD0872
	IF (T7 .LT. T6) T7 = T6 * 1.001D0	ABCD0873
	IF (SI) T7 = T7 * 9.0D0 / 5.0D0	ABCD0874
	HV = ((((((- .4594317D-19 * T7) - .2034116D-15) * T7 +	ABCD0875
	1 .2783643D-11) * T7 + .2051501D-07) * T7 - .2453116D-03) * T7 -	ABCD0876
	2 .9433296D-01) * T7 + .1845537D+05	ABCD0877
	IF (.NOT. SI) GO TO 103	ABCD0878
	T7 = T7 * 5.0D0 / 9.0D0	ABCD0879
	HV = HV * 2325.4295D0	ABCD0880
103	CALL THERMO (P7, HA, T7, XX1, XX2, 1, FAR6, 0)	ABCD0881
C ***	TO ALTER DESIGN ABETAA MAP FROM GENERAL TO SPECIFIC MAP	ABCD0882
	IF (IDES .NE. 1) GO TO 9	ABCD0883
	FAR7DS = (HA - H6) / (HV * ETAADS)	ABCD0884
	CALL ETAAB (0.0D0, 0.0D0, 0.0D0, 0.0D0, ETAADS, ETAASV, P6DS, P6DSAV,	ABCD0885
	1 AM6DS, AM6DSV, IDES, FAR7DS, FAR7SV)	ABCD0886
	T7 = T6	ABCD0887
	GO TO 20	ABCD0888
9	P6GS = P6 * PRATH	ABCD0889
	FAR7GS = (HA - H6) / (HV * ETAADS)	ABCD0890
	DO 10 II = 1, 50	ABCD0891
	CALL ETAAB (FAR7GS, AM6, P6GS, ETAA, ETAADS, ETAASV, P6DS, P6DSAV, AM6DS,	ABCD0892
	1 AM6DSV, IDES, FAR7DS, FAR7SV)	ABCD0893
	FAR7 = (HA - H6) / (HV * ETAA)	ABCD0894
	DELFA7 = DABS (FAR7 - FAR7GS)	ABCD0895
	IF (DELFA7 .LE. 1.0D0 * TOLALL * FAR7) GO TO 11	ABCD0896
10	FAR7GS = FAR7	ABCD0897
11	IF (FAR7 .GT. 0.0D0) GO TO 12	ABCD0898
	ICOAFB = 3	ABCD0899
	CALL ERROR	ABCD0900
12	WFAX = FAR7 * WG6	ABCD0901
	IF (IAFTBN .EQ. 1) GO TO 15	ABCD0902
	ERRW = (WFA - WFAX) / WFA	ABCD0903
	DIR = DSQRT(WFA / WFAX)	ABCD0904
	CALL AFQUIR (Q(1), T7, ERRW, 0.0D0, 30.0D0, .5D0 * TOLALL, DIR, T7T, IGO)	ABCD0905
	ICOAFB = 4	ABCD0906

	GO TO (13,16,14), IGO	ABCD0907
13	T7 = T7T	ABCD0908
	GO TO 8	ABCD0909
14	CALL ERROR	ABCD0910
15	WFA = WFAX	ABCD0911
16	FAR7 = (WF6 + WFA) / WA6	ABCD0912
	WG7 = WG6 + WFA	ABCD0913
C ***	MOMENTUM LOSS	ABCD0914
	CALL PROCOM (FAR7,T7,XX1,XX2,XX3,REX7,PHI7,H7)	ABCD0915
	RHO7 = CAPSF * P7 / (AJ * REX7 * T7)	ABCD0916
	V7 = WG7 / (RHO7 * A7)	ABCD0917
	Q(2) = 0.0D0	ABCD0918
	Q(3) = 0.0D0	ABCD0919
	PS7 = PS65 - 0.01D0	ABCD0920
17	RHO7 = WG7 / (V7 * A7)	ABCD0921
	HS7 = H7 - V7 ** 2 / GAJ2	ABCD0922
	CALL THERMO (1.0D0,HS7,TS7,PHI7,XX2,1,FAR7,1)	ABCD0923
	IF (TS7 .GE. 301.0D0) GO TO 13	ABCD0924
	CALL THERMO (1.0D0,HS7,400.0D0,PHI7,XX2,1,FAR7,0)	ABCD0925
	V7 = DSQRT(GAJ2 * (H7 - HS7))	ABCD0926
	GO TO 17	ABCD0927
18	PS7 = RHO7 * AJ * REX7 * TS7 / CAPSF	ABCD0928
	PS7A = PS65 + (RHO65 * V65 ** 2 - RHO7 * V7 ** 2) / (G * CAPSF)	ABCD0929
	DIR = DSQRT(DABS(PS7 / PS7A))	ABCD0930
	EP = (PS7 - PS7A) / PS7	ABCD0931
	CALL AFQUIR (Q(1),V7,EP,0.0D0,50.0D0,1.0D0*TOLALL,DIR,V7T,IGO)	ABCD0932
	V7 = V7T	ABCD0933
	IF (V7 .LT. 100.0D0) V7 = 100.0D0	ABCD0934
	ICOAFB = 5	ABCD0935
	GO TO (17,19,14), IGO	ABCD0936
19	P7 = PS7 * DEXP((PHI7 - PHI7) / REX7)	ABCD0937
	CALL PROCOM (FAR7,TS7,CS7,XX2,XX3,XX4,XX5,XX6)	ABCD0938
	AM7 = V7 / CS7	ABCD0939
20	CALL THERMO (P7,H7,T7,S7,XX2,1,FAR7,0)	ABCD0940
	IF (VAFTBN .EQ. 0.0D0) GO TO 31	ABCD0941
	Q(2) = 0.0D0	ABCD0942
	Q(3) = 0.0D0	ABCD0943
	WG7P = WG7	ABCD0944
	H7P = H7	ABCD0945
	P7DOT = DERIV(18,P7)	ABCD0946
28	CALL THERMO (P7,H7,T7,S7,XX2,1,FAR7,0)	ABCD0947
	WG7 = WG7P - P7DOT * VAFTBN / T7 / (1.4D0 * PA)	ABCD0948
	U7 = H7 - AJX * RA * T7	ABCD0949
	U7DOT = DERIV(19,U7)	ABCD0950
	H7X = (WG7P * H7P - (WG7P - WG7) * U7 - U7DOT * P7 * VAFTBN /	ABCD0951
1	T7 / RA) / WG7	ABCD0952
	ERRW = (H7 - H7X) / H7	ABCD0953
	DIR = DSQRT(DABS(H7 / H7X))	ABCD0954
	CALL AFQUIR (Q(1),T7,ERRW,0.0D0,20.0D0,.1D0*TOLALL,DIR,T7T,IGO)	ABCD0955
	ICOAFB = 6	ABCD0956
	GO TO (29,31,30), IGO	ABCD0957
29	T7 = T7T	ABCD0958
	GO TO 28	ABCD0959
30	CALL ERROR	ABCD0960

31	ICOFB = 0	ABCD0961
	CALL COMNOZ	ABCD0962
	RETURN	ABCD0963
C		ABCD0964
C		ABCD0965
	END	ABCD0966

Subroutine COCOMB

	SUBROUTINE COCOMB	ABCD0967
	IMPLICIT REAL*8 (A-H,O-Z)	ABCD0968
	LOGICAL SI, FXM2CP	ABCD0969
	COMMON /COMALL/ COM(1062)	ABCD0970
	COMMON /COMDAT/ COMD(5423)	ABCD0971
	DIMENSION WORD(2), PSIXB(15), DELXB(15,15), ETAXB(15,15),	ABCD0972
	1 NPTB(15)	ABCD0973
	DIMENSION Q(9), DUMBO(15,15), AWORD(2)	ABCD0974
	EQUIVALENCE (WORD(1), COM(1)), (IDES, COM(3)), (MODE, COM(6)),	ABCD0975
	1 (MAPEDG, COM(22)), (TOLALL, COM(23)), (T3, COM(152)), (H3,	ABCD0976
	2 COM(153)), (WA3, COM(154)), (WA3CDS, COM(155)), (T4, COM(156)),	ABCD0977
	3 (H4, COM(157)), (S4, COM(158)), (WG4, COM(159)),	ABCD0978
	4 (FAR4, COM(160)), (T50, COM(161)), (H50, COM(162)),	ABCD0979
	5 (S50, COM(163)), (WG50, COM(164)), (FAR50, COM(165)),	ABCD0980
	6 (PCBLHP, COM(166)), (PCBLIP, COM(167)), (PCBLP, COM(168)),	ABCD0981
	7 (PCBLDU, COM(169)), (PCBLOB, COM(170)), (CNHP, COM(171)),	ABCD0982
	8 (ETATHP, COM(172)), (DHTCHP, COM(173)), (DHTC, COM(174)),	ABCD0983
	9 (TFFHP, COM(175)), (ETABCF, COM(179)), (ETABDS, COM(184)),	ABCD0984
	1 (WFBDS, COM(185)), (ETAB, COM(190)), (WAC, COM(191)),	ABCD0985
	2 (WFB, COM(192)), (BLC, COM(193)), (DPCODS, COM(197)),	ABCD0986
	3 (DPCOM, COM(198)), (P3, COM(379)), (P4, COM(381)),	ABCD0987
	4 (U4, COM(382)), (P50, COM(383)), (VCOMB, COM(398)),	ABCD0988
	5 (ISPOOL, COM(1044)), (ITRAN, COM(1049)), (SI, COM(1055)),	ABCD0989
	6 (FXM2CP, COM(1059))	ABCD0990
	EQUIVALENCE (PSIXB(1), COMD(2761)), (DELXB(1,1), COMD(2776)),	ABCD0991
	1 (ETAXB(1,1), COMD(3001)), (NPSB, COMD(5360)),	ABCD0992
	2 (NPTB(1), COMD(5361))	ABCD0993
	DATA AWORD /4HCOCO, 4HMB /	ABCD0994
	WORD(1) = AWORD(1)	ABCD0995
	WORD(2) = AWORD(2)	ABCD0996
	IF(SI) GO TO 100	ABCD0997
	RA = .0252D0	ABCD0998
	AJ = 2.719D0	ABCD0999
	TMAX = 4000.0D0	ABCD1000
	TMIN = 1000.0D0	ABCD1001
	GO TO 101	ABCD1002
100	RA = 286.9D0	ABCD1003
	AJ = 1.0D0	ABCD1004
	TMAX = 2222.0D0	ABCD1005
	TMIN = 555.5D0	ABCD1006
101	Q(2) = 0.0D0	ABCD1007
	Q(3) = 0.0D0	ABCD1008
	P3PSI = 14.696D0 * P3	ABCD1009
	IF (SI) P3PSI = .14504D-3 * P3	ABCD1010
	WA3C = WA3 * DSQRT(T3) / P3PSI	ABCD1011

	IF (SI) WA3C = WA3 * DSQRT(T3) / P3	ABCD1012
	IF (IDES .EQ. 1) WA3CDS = WA3C	ABCD1013
	DPCOM = DPCODS * (WA3C / WA3CDS)	ABCD1014
	IF (DPCOM .GT. 1.0D0) DPCOM = 1.0D0	ABCD1015
	P4 = P3 * (1.0D0 - DPCOM)	ABCD1016
	IF (IDES .EQ. 1 .AND. MODE .EQ. 2) T4 = (TMAX + TMIN) / 2.0	ABCD1017
	IF (ITRAN .EQ. 1 .AND. MODE .EQ. 2) CALL FCNTRL	ABCD1018
1	IF (T4 .GT. TMAX) T4 = TMAX	ABCD1019
	IF (T4 .GE. TMIN) GO TO 2	ABCD1020
	T4 = TMIN	ABCD1021
	IF (MODE .EQ. 1) MAPEDG = 1	ABCD1022
2	DTCO = T4 - T3	ABCD1023
	IF (SI) DTCO = DTCO * 9.0D0 / 5.0D0	ABCD1024
	P3PSIN = P3PSI	ABCD1025
	CALL SEARCH (-1.0D0, P3PSIN, DTCO, ETAB, DUMMY, PSIXB(1), NPSB,	ABCD1026
1	DELXB(1,1), ETAXB(1,1), DUMBO(1,1), NPTB(1), 15, 15, IGO)	ABCD1027
	IF (IGO .EQ. 7) CALL ERROR	ABCD1028
	IF (IDES .NE. 1) GO TO 4	ABCD1029
	ETABCF = ETABDS / ETAB	ABCD1030
4	ETAB = ETABCF * ETAB	ABCD1031
	IF (SI) T4 = T4 * 9.0D0 / 5.0D0	ABCD1032
	HV = ((((((- .4594317D-19 * T4) - .2034116D-15) * T4 +	ABCD1033
1	.2783643D-11) * T4 + .2051501D-07) * T4 - .2453116D-03) * T4 -	ABCD1034
2	.9433296D-01) * T4 + .1845537D+05	ABCD1035
	IF (.NOT. SI) GO TO 3	ABCD1036
	T4 = T4 * 5.0D0 / 9.0D0	ABCD1037
	HV = HV * 2325.4295D0	ABCD1038
3	CALL THERMO (P4, HA, T4, XX1, XX2, 0, 0.0D0, 0)	ABCD1039
	FAR4 = (HA - H3) / (HV * ETAB)	ABCD1040
	IF (FAR4 .LT. 0.0D0) FAR4 = 0.0D0	ABCD1041
	WFBX = FAR4 * WA3	ABCD1042
	IF (MODE .NE. 2) GO TO 7	ABCD1043
	ERRW = (WFB - WFBX) / WFB	ABCD1044
	DIR = DSQRT(WFB / WFBX)	ABCD1045
	CALL AFQUIR (Q(1), T4, ERRW, 0.0D0, 20.0D0, .1D0*TOLALL, DIR, T4T, IGO)	ABCD1046
	GO TO (5, 8, 6), IGO	ABCD1047
5	T4 = T4T	ABCD1048
	GO TO 1	ABCD1049
6	CALL ERROR	ABCD1050
7	WFB = WFBX	ABCD1051
	IF (IDES .EQ. 1) WFBDS = WFB	ABCD1052
8	CALL THERMO (P4, H4, T4, S4, XX2, 1, FAR4, 0)	ABCD1053
	WG4 = WFB + WA3	ABCD1054
	IF (VCOMB .EQ. 0.0D0) GO TO 21	ABCD1055
	Q(2) = 0.0D0	ABCD1056
	Q(3) = 0.0D0	ABCD1057
	WG4P = WG4	ABCD1058
	H4P = H4	ABCD1059
	P4DOT = DERIV(10, P4)	ABCD1060
13	CALL THERMO (P4, H4, T4, S4, XX2, 1, FAR4, 0)	ABCD1061
	WG4 = WG4P - P4DOT * VCOMB / T4 / 1.4D0 / RA	ABCD1062
	U4 = H4 - AJ * RA * T4	ABCD1063
	U4DOT = DERIV(11, U4)	ABCD1064
	H4X = (WG4P * H4P - (WG4P - WG4) * U4 - U4DOT * P4 * VCOMB / T4 /	ABCD1065

	1 RA) / WG4	ABCD1066
	ERRW = (H4 - H4X) / H4	ABCD1067
	DIR = DSQRT(DABS(H4 / H4X))	ABCD1068
	CALL AFQUIR (Q(1), T4, ERFW, 0.0D0, 20.0D0, .1D0*TOLALL, DIR, T4T, IGO)	ABCD1069
	GO TO (19, 21, 20), IGO	ABCD1070
19	T4 = T4T	ABCD1071
	GO TO 18	ABCD1072
20	CALL ERROR	ABCD1073
21	PCBLUS = 1.0 - PCBLHP - PCBLIP - PCBLLP - PCBLOB - PCBLDU	ABCD1074
	IF (PCBLUS .LT. .00001D0) GO TO 22	ABCD1075
	BLUS = BLC * PCBLUS	ABCD1076
	IF (BLUS .LT. (.0000001D0 * WAC)) GO TO 22	ABCD1077
	FAR4 = FAR4 * WG4 / (WG4 + BLUS * (1.0D0 + FAR4))	ABCD1078
	H4 = (H4 * WG4 + H3 * BLUS) / (WG4 + BLUS)	ABCD1079
	WG4 = WG4 + BLUS	ABCD1080
	CALL THERMO (P4, H4, T4, S4, XX2, 1, FAR4, 1)	ABCD1081
22	IF (IDES .EQ. 1) WRITE (6, 10) WA3CDS, ETABCF	ABCD1082
	IF (FXM2CP .OR. ISPOOL .EQ. 1) GO TO 9	ABCD1083
	CALL COHPTE	ABCD1084
	RETURN	ABCD1085
9	P50 = P4	ABCD1086
	H50 = H4	ABCD1087
	T50 = T4	ABCD1088
	S50 = S4	ABCD1089
	FAR50 = FAR4	ABCD1090
	WG50 = WG4	ABCD1091
C	SET HIGH PRESSURE TURBINE PARAMETERS TO ZERO, NOT USED	ABCD1092
	TFFHP = 0.0D0	ABCD1093
	CNHP = 0.0D0	ABCD1094
	DHTC = 0.0D0	ABCD1095
	DHTCHP = 0.0D0	ABCD1096
	ETATHP = 0.0D0	ABCD1097
	IF (FXM2CP) CALL COIPTB	ABCD1098
C	IF RUNNING 1 SPOOL TJ GO TO COHPTE TO ZERO OUT COIPTB	ABCD1099
	IF (.NOT. FXM2CP) CALL COHPTE	ABCD1100
	RETURN	ABCD1101
C		ABCD1102
C		ABCD1103
C		ABCD1104
10	FORMAT (17H0COMBUSTOR DESIGN, 7X, 8H WA3CDS=, F15.8, 8H ETABCF=,	ABCD1105
	1 E15.3)	ABCD1106
	END	ABCD1107

Subroutine COCOMP

	SUBROUTINE COCOMP	ABCD1108
	IMPLICIT REAL*8 (A-H, O-Z)	ABCD1109
	LOGICAL SI, DUMSPL, FXM2CP, AFFFAN, FAN	ABCD1110
	COMMON /COMALL/ COM(1062)	ABCD1111
	COMMON /COMDAT/ COMD(5423)	ABCD1112
	DIMENSION WORD(2), ERR(9), CNXP(15), PRXP(15,15), WACXP(15,15),	ABCD1113
1	ETAXP(15,15), NPTP(15)	ABCD1114
	DIMENSION Q(9), WLH(2,2), AWORD(2)	ABCD1115
	EQUIVALENCE (WORD(1), COM(1)), (IDES, COM(3)), (MODE, COM(6)),	ABCD1116

1	(MAPEDG, COM(22)), (TOLALL, COM(23)), (ERR(1), COM(24)), (T2,	ABCD1117
2	COM(92)), (T3, COM(152)), (H3, COM(153)), (WA3, COM(154)),	ABCD1118
3	(PCBLHP, COM(166)), (PCBLIP, COM(167)), (PCBLLP, COM(168)),	ABCD1119
4	(PCBLDU, COM(169)), (PCBLOB, COM(170)), (WAC, COM(191)),	ABCD1120
5	(BLC, COM(193)), (T21, COM(263)), (H21, COM(264)),	ABCD1121
6	(S21, COM(265)), (WA21, COM(266)), (T21DS, COM(267)),	ABCD1122
7	(T22, COM(268)), (WA22, COM(269)), (S3, COM(270)),	ABCD1123
8	(WA32, COM(271)), (PRCCF, COM(294)), (ETACCF, COM(295)),	ABCD1124
9	(WACCF, COM(296)), (PRCDS, COM(297)), (ETACDS, COM(298)),	ABCD1125
1	(WACDS, COM(299)), (ZC, COM(300)), (PCNC, COM(301)),	ABCD1126
2	(PCBLC, COM(302)), (PCNCDS, COM(303)), (PCBLI, COM(304)),	ABCD1127
3	(PCBLID, COM(305)), (CNC, COM(306)), (PRC, COM(307)),	ABCD1128
4	(ETAC, COM(308)), (CNI, COM(309)), (WACI, COM(310)),	ABCD1129
5	(WAI, COM(311)), (BLI, COM(312)), (BLHP, COM(313)),	ABCD1130
6	(BLIP, COM(314)), (BLLP, COM(315)), (BLF, COM(316)),	ABCD1131
7	(BLDU, COM(317)), (BLOB, COM(318)), (WAF, COM(319)),	ABCD1132
8	(WACC, COM(320)), (P21, COM(377)), (P3, COM(379)),	ABCD1133
9	(U3, COM(380)), (VCOMP, COM(397)), (WACP, COM(422)),	ABCD1134
1	(ISPOOL, COM(1044)), (SI, COM(1055)), (DUMSPL, COM(1057))	ABCD1135
	EQUIVALENCE (FXM2CP, COM(1059)), (AFTFAN, COM(1060)),	ABCD1136
1	(FAN, COM(1061))	ABCD1137
	EQUIVALENCE (CNXP(1), COMD(2071)), (PRXP(1,1), COMD(2086)),	ABCD1138
1	(WACXP(1,1), COMD(2311)), (ETAXP(1,1), COMD(2536)),	ABCD1139
2	(NCNP, COMD(5344)), (NPTP(1), COMD(5345))	ABCD1140
	DATA AWORD, WLH / 4HCOCO, 4HMP , 4H (LO, 4H) , 4H (HI, 4H) /	ABCD1141
	WORD(1) = AWORD(1)	ABCD1142
	WORD(2) = AWORD(2)	ABCD1143
	IF (SI) GO TO 100	ABCD1144
	TSTD = 518.668D0	ABCD1145
	PSTD = 1.0D0	ABCD1146
	RA = .0252D0	ABCD1147
	AJ = 2.719D0	ABCD1148
	GO TO 101	ABCD1149
100	TSTD = 288.149D0	ABCD1150
	PSTD = 101325.0D0	ABCD1151
	RA = 286.9D0	ABCD1152
	AJ = 1.0D0	ABCD1153
101	THETA = DSQRT(T21 / TSTD)	ABCD1154
	DELTA = P21 / PSTD	ABCD1155
	IF (IDES .NE. 1 .AND. .NOT. FXM2CP) GO TO 2	ABCD1156
	IF (IDES .NE. 1) GO TO 1	ABCD1157
	WACDS = WAC	ABCD1158
	WACC = WAC * THETA / DELTA	ABCD1159
	IF (FXM2CP) GO TO 1	ABCD1160
	PCNC = PCNCDS * THETA	ABCD1161
	GO TO 2	ABCD1162
C	SPEEDS OF MIDDLE AND INNER SPOOL ARE THE SAME	ABCD1163
1	SPDMID = CNI * DSQRT(T22 / TSTD)	ABCD1164
	IF (AFTFAN) SPDMID = CNI * DSQRT(T2 / TSTD)	ABCD1165
	CNC = SPDMID / THETA	ABCD1166
	PCNC = 100.0D0 * THETA * CNC	ABCD1167
	IF (IDES .EQ. 1) PCNCDS = PCNC / THETA	ABCD1168
2	CNC = PCNC / (100.0D0 * THETA)	ABCD1169
	IF (ZC .LT. 0.0D0) ZC = 0.0D0	ABCD1170

	IF (ZC .GT. 1.0D0) ZC = 1.0D0	ABCD1171
	CNCS = CNC	ABCD1172
	IF (ISPOOL .EQ. 1) GO TO 12	ABCD1173
	CALL SEARCH (ZC,CNC,PRC,WACC,ETAC,CNXP(1),NCNP,PRXP(1,1),	ABCD1174
	1 WACXP(1,1),ETAXP(1,1),NPIP(1),15,15,IGO)	ABCD1175
	GO TO 13	ABCD1176
12	PRC = 1.0D0	ABCD1177
	ETAC = 1.0D0	ABCD1178
	WAC = WA21	ABCD1179
	WACC = WAC * THETA / DELTA	ABCD1180
	CNC = 1.0D0	ABCD1181
	PRCCF = 1.0D0	ABCD1182
13	IF (MODE .EQ. 1) GO TO 4	ABCD1183
	IF ((CNC - CNCS) .GT. .5D0 * TOLALL * CNC) MAPEDG = 1	ABCD1184
4	IF (IGO .EQ. 1 .OR. IGO .EQ. 2) WRITE (8,9) CNCS,WLH(1,IGO),	ABCD1185
	1 WLH(2,IGO)	ABCD1186
	WAC = WACC * DELTA / THETA	ABCD1187
	IF (IDES .NE. 1) GO TO 5	ABCD1188
	T21DS = T21	ABCD1189
	IF (ISPOOL .GE. 2) PRCCF = (PRCDS - 1.0D0) / (PRC - 1.0D0)	ABCD1190
	ETACCF = ETACDS / ETAC	ABCD1191
	IF (ISPOOL .EQ. 1) ETACCF = 1.0D0	ABCD1192
	WACCF = WACDS / WAC	ABCD1193
	WRITE (6,10) PRCCF,ETACCF,WACCF,T21DS	ABCD1194
5	PRC = PRCCF * (PRC - 1.0D0) + 1.0D0	ABCD1195
	ETAC = ETACCF * ETAC	ABCD1196
	WAC = WACCF * WAC	ABCD1197
	WACP = WAC	ABCD1198
	IF (.NOT. DUMSPL .OR. PCBLID .NE. 0.0D0 .OR. .NOT. FAN) GO TO 6	ABCD1199
	WA22 = WAC	ABCD1200
	WAI = WA22	ABCD1201
	WACI = WACC * WACCF	ABCD1202
6	WA32 = WAI - WAC	ABCD1203
	BLI = WA32	ABCD1204
	WA21 = WAC	ABCD1205
	WACC = WACC * WACCF	ABCD1206
	PCBLI = BLI / WAI	ABCD1207
	CALL WDUCT1	ABCD1208
	IF (PCBLID .EQ. 0.0D0) ERF(7) = (WAC - WAI) / WAC	ABCD1209
	IF (.NOT. FAN) ERF(5) = (WAF - WAC - BLF) / WAC	ABCD1210
	IF (IDES .EQ. 1 .AND. PCBLID .EQ. 0.0D0) ERF(7) = 1.0D-4	ABCD1211
	CALL THCOMP (PRC,ETAC,T21,H21,S21,P21,T3,H3,S3,P3)	ABCD1212
	IF (VCOMP .EQ. 0.0D0) GO TO 21	ABCD1213
	Q(2) = 0.0D0	ABCD1214
	Q(3) = 0.0D0	ABCD1215
	H3F = H3	ABCD1216
	P3DOT = DERIV(8,P3)	ABCD1217
13	CALL THEPMO (P3,H3,T3,S3,XX2,0,0.0D0,0)	ABCD1218
	WAC = WACP - P3DOT * VCOMP / T3 / 1.4D0 / RA	ABCD1219
	U3 = H3 - AJ * RA * T3	ABCD1220
	U3DOT = DERIV(9,U3)	ABCD1221
	H3X = (WACP * H3F - (WACP - WAC) * U3 - U3DOT * P3 * VCOMP / T3 /	ABCD1222
	1 RA) / WAC	ABCD1223
	ERRW = (H3 - H3X) / H3	ABCD1224

	DIR = DSQRT(DABS(H3 / H3X))	ABCD1225
	CALL AFQUIR(Q(1),T3,ERRW,0.0D0,20.0D0,.1D0*TOLALL,DIR,T3T,IGO)	ABCD1226
	GO TO (19,21,20), IGO	ABCD1227
19	T3 = T3T	ABCD1228
	GO TO 18	ABCD1229
20	CALL ERROR	ABCD1230
21	IF (PCBLC .GT. 0.0D0) BLC = PCBLC * WAC	ABCD1231
	WA3 = WAC - BLC	ABCD1232
	BLDU = PCBLDU * BLC	ABCD1233
	BLDB = PCBLOB * BLC	ABCD1234
	BLHP = PCBLHP * BLC	ABCD1235
	BLIP = PCBLIP * BLC	ABCD1236
	BLLP = PCBLLP * BLC	ABCD1237
	IF (MODE .NE. 1) GO TO 7	ABCD1238
	IF (DABS(CNC - CNCS) .LE. 1.0D0 * TOLALL * CNCS) GO TO 8	ABCD1239
	WRITE(8,11) CNCS,CNC	ABCD1240
	CALL ERROR	ABCD1241
7	PCNC = 100.0D0 * THETA * CNC	ABCD1242
8	CALL COCOMB	ABCD1243
	RETURN	ABCD1244
C		ABCD1245
C		ABCD1246
C		ABCD1247
9	FORMAT(19H0* * * CNC OFF MAP,F10.4,2X,A4,A2,11H* * *\$\$\$\$\$)	ABCD1248
10	FORMAT(18H0COMPRESSOR DESIGN,6X,8H PRCCF=,E15.8,8H ETACCF=,	ABCD1249
	1 E15.8,8H WACCF=,E15.8,8H T2IDS=,E15.8)	ABCD1250
11	FORMAT(10H0CNC WAS=,E15.8,11H AND NOW=,E15.8,12H CHECK PCNC,	ABCD1251
	1 12H INPUT\$\$\$\$\$)	ABCD1252
	END	ABCD1253

Subroutine CODUCT

	SUBROUTINE CODUCT	ABCD1254
	IMPLICIT REAL*8 (A-H,O-Z)	ABCD1255
	LOGICAL SI, APTFAN	ABCD1256
	COMMON /COMALL/ COM(1062)	ABCD1257
	DIMENSION WORD(2), ERR(9)	ABCD1258
	DIMENSION Q(9), AWORD1(2), AWORD2(2)	ABCD1259
	EQUIVALENCE (WORD(1), COM(1)), (IDES, COM(3)), (IGASMX, COM(10)),	ABCD1260
1	(IDBURN, COM(11)), (IDCD, COM(13)), (IDSHOC, COM(15)),	ABCD1261
2	(NOZFLT, COM(17)), (TOLALL, COM(23)), (ERR(1), COM(24)), (P1,	ABCD1262
3	COM(33)), (H22, COM(34)), (AM23, COM(35)), (WA23DS, COM(36)),	ABCD1263
4	(T23, COM(37)), (P23, COM(38)), (H23, COM(39)), (S23, COM(40)),	ABCD1264
5	(A24, COM(41)), (T24, COM(42)), (H24, COM(43)), (S24, COM(44)),	ABCD1265
6	(AM25, COM(45)), (T25, COM(46)), (P25, COM(47)), (H25, COM(48)),	ABCD1266
7	(S25, COM(49)), (A28, COM(50)), (A28SAV, COM(51)),	ABCD1267
8	(AM28, COM(52)), (V28, COM(53)), (TS28, COM(54)),	ABCD1268
9	(PS28, COM(55)), (T28, COM(56)), (P28, COM(57)), (H28, COM(58)),	ABCD1269
1	(S28, COM(59)), (A29, COM(60)), (A29SAV, COM(61)),	ABCD1270
2	(AM29, COM(62)), (V29, COM(63)), (TS29, COM(64)),	ABCD1271
3	(PS29, COM(65)), (T29, COM(66)), (P29, COM(67)), (H29, COM(68)),	ABCD1272
4	(S29, COM(69)), (BYPASS, COM(70)), (WAD, COM(71)),	ABCD1273
5	(WFD, COM(72)), (ETAD, COM(73)), (DPDNC, COM(74)),	ABCD1274
6	(DPDUDS, COM(75)), (H3, COM(153)), (WAC, COM(191)),	ABCD1275

7	(PCBLID, COM(305)), (WAI, COM(311)), (BLF, COM(316)),	ABCD1276
8	(BLDU, COM(317)), (WAF, COM(319)), (WG24, COM(321)),	ABCD1277
9	(FAR24, COM(322)), (P22, COM(375)), (P24, COM(391)),	ABCD1278
1	(U24, COM(392)), (VFDUCT, COM(403)), (ICODUC, COM(1046))	ABCD1279
	EQUIVALENCE (ITRAN, COM(1049)), (SI, COM(1055)),	ABCD1280
1	(AFTFAN, COM(1060))	ABCD1281
	DATA AWORD1, AWORD2 /4HCODU, 4HCT , 4HDNO7, 4HZL /	ABCD1282
	WORD(1) = AWORD1(1)	ABCD1283
	WORD(2) = AWORD1(2)	ABCD1284
	Q(2) = 0.0D0	ABCD1285
	Q(3) = 0.0D0	ABCD1286
	GOGC = 0.0D0	ABCD1287
	IF (SI) GO TO 100	ABCD1288
	AJ = 778.26D0	ABCD1289
	AJX = 2.719D0	ABCD1290
	CAPSF = 2116.217D0	ABCD1291
	G = 32.174049D0	ABCD1292
	TSID = 518.67D0	ABCD1293
	TDEL = 2000.0D0	ABCD1294
	TMAX = 4000.0D0	ABCD1295
	RA = .0252D0	ABCD1296
	GO TO 101	ABCD1297
100	AJ = 1.0D0	ABCD1298
	AJX = 1.0D0	ABCD1299
	CAPSF = 101323.0D0	ABCD1300
	G = 1.0D0	ABCD1301
	TSTD = 234.15D0	ABCD1302
	TDEL = 1111.0D0	ABCD1303
	TMAX = 2222.0D0	ABCD1304
	RA = 286.9D0	ABCD1305
101	GAJ2 = 2.0D0 * G * AJ	ABCD1306
	ICODUC = 0	ABCD1307
	WAX = WAF - WAI - BLF	ABCD1308
	IF (PCBLID .EQ. 0.0D0) WAX = WAF - WAC - BLF	ABCD1309
	IF (AFTFAN) WAX = WAF - BLF	ABCD1310
	WAD = WAX + BLDU	ABCD1311
	P23 = P22	ABCD1312
C***	DRY LOSS	ABCD1313
	H23 = (BLDU * H3 + WAX * H22) / WAD	ABCD1314
	CALL THERMO (P23, H23, T23, S23, XX2, 1, 0.0D0, 1)	ABCD1315
	WA23C = WAD * DSQRT(T23) / P23	ABCD1316
	IF (IDES .EQ. 1) WA23DS = WA23C	ABCD1317
	BYPASS = (WAF - WAI) / WAI	ABCD1318
	IF (AFTFAN) BYPASS = WAF / WAI	ABCD1319
	DPDUC = DPDUCS * (WA23C / WA23DS)	ABCD1320
	IF (DPDUC .GT. 1.0D0) DPDUC = 1.0D0	ABCD1321
	P24 = P23 * (1.0D0 - DPDUC)	ABCD1322
	CALL PROCOM (0.0D0, T23, XX1, XX2, XX3, XX4, PHI23, XX6)	ABCD1323
	IF (IGASM .GT. 0) IDBURN = 0	ABCD1324
	AM24 = AM23	ABCD1325
	TS24 = T23 * 0.875D0	ABCD1326
1	DO 2 I = 1, 50	ABCD1327
	CALL PROCOM (0.0D0, TS24, CS24, AK24, CP24, REX24, PHIS24, HS24)	ABCD1328
	V24 = AM24 * CS24	ABCD1329

	HSCAL = H23 - V24 ** 2 / GAJ2	ABCD1330
	DELHS = HSCAL - HS24	ABCD1331
	IF (DABS(DELHS) .LE. 1.0D0 * TOLALL * HSCAL) GO TO 3	ABCD1332
2	TS24 = TS24 + DELHS / CF24	ABCD1333
	ICODUC = 1	ABCD1334
	GO TO 11	ABCD1335
3	C1 = P24 * DSQRT(G / (T23 * AJ)) * CAPSF	ABCD1336
	AK24M1 = AK24 - 1.0D0	ABCD1337
	AK24P1 = AK24 + 1.0D0	ABCD1338
	AKM1 = AK24M1 / 2.0D0	ABCD1339
	AKP1 = AK24P1 / 2.0D0	ABCD1340
	IF (IDES .NE. 1) GO TO 4	ABCD1341
	IF (GOGO .GT. 0.0D0) GO TO 4	ABCD1342
	ASTOA = AKP1 ** (AKP1 / AK24M1) * AM24 * (1.0D0 + AKM1 *	ABCD1343
1	AM24 ** 2) ** (- AKP1 / AK24M1)	ABCD1344
	EQWCR = DSQRT(G * AK24 / REX24 / AJ) / (DSQRT(TSTD) / CAPSF) *	ABCD1345
1	(2.0D0 / AK24P1) ** (AKP1 / AK24M1)	ABCD1346
	WA23CC = WA23C / DSQRT(TSTD)	ABCD1347
	A24 = 1.0D0 / ASTOA * WA23CC / EQWCR	ABCD1348
	GOGO = 1.0D0	ABCD1349
4	WQA = WAD / A24	ABCD1350
	WQAT = C1 * DSQRT(AK24 / REX24) * AM24 / (1.0D0 + AKM1 * AM24 **	ABCD1351
1	2) ** (AKP1 / AK24M1)	ABCD1352
	DIR = WQA / WQAT	ABCD1353
	EW = (WQA - WQAT) / WQA	ABCD1354
	CALL AFQUIR (Q(1), AM24, EW, 0.0D0, 30.0D0, 1.0D0 * TOLALL, DIR, AM24T, IGO)	ABCD1355
	ICODUC = 2	ABCD1356
	GO TO (5, 6, 11), IGO	ABCD1357
5	AM24 = AM24T	ABCD1358
	IF (AM24 .GT. 1.0D0) AM24 = 0.5D0	ABCD1359
	GO TO 1	ABCD1360
6	PS24 = P24 / DEXP((PHI23 - PHIS24) / PEX24)	ABCD1361
7	IF (IDBURN .GT. 0) GO TO 8	ABCD1362
C***	NON-DUCT BURNING	ABCD1363
	T24 = T23	ABCD1364
	WFD = 0.0D0	ABCD1365
	FAR24 = 0.0D0	ABCD1366
	GO TO 17	ABCD1367
8	IF (IDBUFN .EQ. 2) T24 = T23 + TDEL	ABCD1368
9	IF (T24 .GT. TMAX) T24 = TMAX	ABCD1369
	IF (T24 .LT. T23) T24 = T23	ABCD1370
C***	DUCT BURNING	ABCD1371
	RHO42 = CAPSF * PS24 / (AJ * REX24 * TS24)	ABCD1372
	PS42 = PS24	ABCD1373
	V42 = V24	ABCD1374
	Q(2) = 0.0D0	ABCD1375
	Q(3) = 0.0D0	ABCD1376
	IF (T24 .LT. T23) T24 = T23 * 1.001D0	ABCD1377
C ***	IF DESIRED, ENTER CALCULATIONS FOR ETAD HERE	ABCD1378
	IF (SI) T24 = T24 * 9.0D0 / 5.0D0	ABCD1379
	HV = ((((((- .4594317D-19 * T24) - .2034116D-15) * T24 +	ABCD1380
1	.2783643D-11) * T24 + .2051501D-07) * T24 - .2453116D-03) * T24	ABCD1381
2	- .9433296D-01) * T24 + .1845537D+05	ABCD1382
	IF (.NOT. SI) GO TO 102	ABCD1383

	T24 = T24 * 5.0D0 / 9.0D0	ABCD1384
	HV = HV * 2325.4295D0	ABCD1385
102	CALL THERMO (P24,HA,T24,XX1,XX2,0,0.0D0,0)	ABCD1386
	FAR24 = (HA - H23) / (HV * ETAD)	ABCD1387
	IF (FAR24 .LT. 0.0D0) FAR24 = 0.0D0	ABCD1388
	WFDX = FAR24 * WAD	ABCD1389
	IF (IDBURN .NE. 2) GO TO 12	ABCD1390
	ERRW = (WFD - WFDX) / WFD	ABCD1391
	DIR = DSQRT(WFD / WFDX)	ABCD1392
	CALL AFQUIR (Q(1),T24,ERRW,0.0D0,20.0D0,.1D0*TOLALL,DIR,T24T,IGO)	ABCD1393
	ICODUC = 3	ABCD1394
	GO TO (10,13,11), IGO	ABCD1395
10	T24 = T24T	ABCD1396
	GO TO 9	ABCD1397
11	CALL ERROR	ABCD1398
12	WFD = WFDX	ABCD1399
C***	MOMENTUM LOSS	ABCD1400
13	WG24 = WFD + WAD	ABCD1401
	CALL PROCOM (FAR24,T24,XX1,XX2,XX3,REX24,PHI24,H24)	ABCD1402
	RHO24 = CAPSF * P24 / (AJ * REX24 * T24)	ABCD1403
	V24 = WG24 / (RHO24 * A24)	ABCD1404
	Q(2) = 0.0D0	ABCD1405
	Q(3) = 0.0D0	ABCD1406
	PS24 = PS42 - 0.01D0	ABCD1407
14	RHO24 = WG24 / (V24 * A24)	ABCD1408
	HS24 = H24 - V24 ** 2 / GAJ2	ABCD1409
	CALL THERMO (1.0D0,HS24,TS24,PHI524,XX2,1,FAR24,1)	ABCD1410
	IF (TS24 .GE. 301.0D0) GO TO 15	ABCD1411
	CALL THERMO (1.0D0,HS24,400.0D0,PHI524,XX2,1,FAR24,1)	ABCD1412
	V24 = DSQRT(GAJ2 * (H24 - HS24))	ABCD1413
	GO TO 14	ABCD1414
15	PS24 = RHO24 * AJ * REX24 * TS24 / CAPSF	ABCD1415
	PS24A = PS42 + (RHO24 * V24 ** 2 - RHO24 * V24 ** 2) / (G * CAPSF)	ABCD1416
	DIR = DSQRT(DABS(PS24 / PS24A))	ABCD1417
	EP = (PS24 - PS24A) / PS24	ABCD1418
	CALL AFQUIR (Q(1),V24,EP,0.0D0,50.0D0,1.0D0*TOLALL,DIR,V24T,IGO)	ABCD1419
	V24 = V24T	ABCD1420
	IF (V24 .LT. 25.0D0) V24 = 25.0D0	ABCD1421
	ICODUC = 4	ABCD1422
	GO TO (14,16,11), IGO	ABCD1423
16	P24 = PS24 * DEXP((PHI24 - PHI524) / REX24)	ABCD1424
	CALL PROCOM (FAR24,TS24,CS24,XX2,XX3,XX4,XX5,XX6)	ABCD1425
	AM24 = V24 / CS24	ABCD1426
17	CALL THERMO (P24,H24,T24,S24,XXT,1,FAR24,0)	ABCD1427
	WG24 = WFD + WAD	ABCD1428
	IF (VFDUCT .EQ. 0.0D0) GO TO 31	ABCD1429
	Q(2) = 0.0D0	ABCD1430
	Q(3) = 0.0D0	ABCD1431
	WG24P = WG24	ABCD1432
	H24P = H24	ABCD1433
	P24DOT = DERIV(20,P24)	ABCD1434
28	CALL THERMO (P24,H24,T24,S24,XX2,1,FAR24,0)	ABCD1435
	WG24 = WG24P - P24DOT * VFDUCT / T24 / (1.4D0 * RA)	ABCD1436
	U24 = H24 - AJX * RA * T24	ABCD1437

	U24DOT = DERIV(21,U24)	ABCD1438
	H24X = (WG24P * H24P - (WG24P - WG24) * U24 - U24DOT * P24 *	ABCD1439
	1 VFDUCT / T24 / RA) / WG24	ABCD1440
	ERRW = (H24 - H24X) / H24	ABCD1441
	DIR = DSQRT(DABS(H24 / H24X))	ABCD1442
	CALL AFQUIR (Q(1),T24,ERRW,0.0D0,20.0D0,.1D0*TOLALL,DIR,T24T,IGO)	ABCD1443
	ICODUC = 5	ABCD1444
	GO TO (29,31,30), IGO	ABCD1445
29	T24 = T24T	ABCD1446
	GO TO 28	ABCD1447
30	CALL ERROR	ABCD1448
31	T25 = T24	ABCD1449
	P25 = P24	ABCD1450
	H25 = H24	ABCD1451
	S25 = S24	ABCD1452
	AM25 = AM24	ABCD1453
	IF (IGASMX.GT. 0) GO TO 21	ABCD1454
	WORD(1) = AWORD2(1)	ABCD1455
	WORD(2) = AWORD2(2)	ABCD1456
	A28SAV = A28	ABCD1457
	A29SAV = A29	ABCD1458
	NOZD = 0	ABCD1459
	IDNOZ = 0	ABCD1460
	IF (NOZFLT.EQ. 2 .OR. NOZFLT.EQ. 3) NOZD = 1	ABCD1461
	IF (IDES.EQ. 1 .OR. IDBURN.GT. 0 .OR. NOZF.EQ. 1) IDNOZ = 1	ABCD1462
	IF (ITRAN.EQ. 1) IDNOZ = 0	ABCD1463
	IF (IDCD.EQ. 1) GO TO 18	ABCD1464
	CALL CONVRG (T25,H25,P25,S25,FAF24,WG24,P1,IDNOZ,A28,A29,P25R,T24T,120,ABCD1465	ABCD1465
	1 P28,S28,TS28,PS28,V28,AM28,ICON)	ABCD1466
	GO TO (19,19,19,11), ICON	ABCD1467
18	CALL CONDIV (T25,H25,P25,S25,FAF24,WG24,P1,IDNOZ,P28,A28,P25R,T24T,ABCD1468	ABCD1468
	1 H28,P28,S28,T28,H29,P29,S29,TS28,PS28,TS29,V28,V29,AM28,	ABCD1469
	2 AM29,ICON)	ABCD1470
	IDSHOC = ICON	ABCD1471
	ICODUC = 6	ABCD1472
	GO TO (20,20,20,11), ICON	ABCD1473
19	T29 = T28	ABCD1474
	H29 = H28	ABCD1475
	P29 = P28	ABCD1476
	S29 = S28	ABCD1477
	TS29 = TS28	ABCD1478
	PS29 = PS28	ABCD1479
	V29 = V28	ABCD1480
	AM29 = AM28	ABCD1481
	A29 = A29	ABCD1482
	IDSHOC = ICON + 3	ABCD1483
20	ERR(5) = (P25R - P25) / P25R	ABCD1484
	IF (IDNOZ.EQ. 1) WRITE (6,22) A28,AM28,A29,AM29	ABCD1485
21	ICODUC = 0	ABCD1486
	CALL FASTBK	ABCD1487
	RETURN	ABCD1488
C		ABCD1489
C		ABCD1490
22	FORMAT (19HODUCT NOZZLE DESIGN, 5X, 8H A28=, E15.8,	ABCD1491

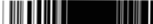
1 8H AM28=, E15.8, 8H A29=, E15.8, 8H AM29=, E15.8)
END

ABCD1492
ABCD1493

Subroutine COFAN

SUBROUTINE COFAN	ABCD1494
IMPLICIT REAL*8 (A-H,O-Z)	ABCD1495
LOGICAL SI, FXM2CP	ABCD1496
COMMON /COMALL/ COM(1062)	ABCD1497
COMMON /COMDAT/ COMD(5423)	ABCD1498
DIMENSION WORD(2), CNXF(15), PRXF(15,15), WACXF(15,15),	ABCD1499
1 ETAXF(15,15), NPTF(15), DUMD1(15)	ABCD1500
DIMENSION Q(9), WLH(2,2), AWORD(2)	ABCD1501
EQUIVALENCE (WORD(1), COM(1)), (IDES, COM(3)), (JDES, COM(4)),	ABCD1502
1 (MODE, COM(6)), (INIT, COM(7)), (MAPEDG, COM(22)), (TOLALL,	ABCD1503
2 COM(23)), (H22, COM(34)), (T2DS, COM(91)), (T2, COM(92)), (P2,	ABCD1504
3 COM(93)), (H2, COM(94)), (S2, COM(95)), (S22, COM(96)), (T22DS,	ABCD1505
4 COM(97)), (T4GU, COM(100)), (T4DS, COM(101)), (PRFCF, COM(121)),	ABCD1506
5 (ETAFCF, COM(122)), (WAFCF, COM(123)), (PCNFDS, COM(124)),	ABCD1507
6 (PRFDS, COM(125)), (ETAFDS, COM(126)), (WAFDS, COM(127)),	ABCD1508
7 (PCMCGU, COM(128)), (PFF, COM(131)), (ETAF, COM(132)),	ABCD1509
8 (ZCDS, COM(133)), (CNF, COM(134)), (WAF, COM(135)),	ABCD1510
9 (ZF, COM(136)), (PCNF, COM(137)), (PCBLF, COM(138)),	ABCD1511
1 (ZI, COM(139)), (PCNI, COM(140)), (ZIDS, COM(146)),	ABCD1512
2 (PCNIDS, COM(147)), (PCNIGU, COM(148)), (T4, COM(156)),	ABCD1513
3 (WFBDS, COM(185)), (WFB, COM(192)), (T21, COM(263)),	ABCD1514
4 (T21DS, COM(267)), (T22, COM(268)), (ZC, COM(300)),	ABCD1515
5 (PCNC, COM(301)), (PCNCDS, COM(303)), (BLF, COM(316)),	ABCD1516
6 (WAF, COM(319)), (P22, COM(375)), (U22, COM(376)),	ABCD1517
7 (VFAN, COM(395)), (DUMD1(1), COM(405)), (WAFP, COM(420)),	ABCD1518
8 (JTRAN, COM(1050)), (SI, COM(1055)), (FXM2CP, COM(1059))	ABCD1519
EQUIVALENCE (CNXF(1), COMD(1)), (PRXF(1,1), COMD(16)),	ABCD1520
1 (WACXF(1,1), COMD(241)), (ETAXF(1,1), COMD(466)),	ABCD1521
2 (NCNF, COMD(5296)), (NPTF(1), COMD(5297))	ABCD1522
DATA AWORD, WLH /4H COP, 4HAN , 4H (LO, 4H) , 4H (HI, 4H) /	ABCD1523
WORD(1) = AWORD(1)	ABCD1524
WORD(2) = AWORD(2)	ABCD1525
IF (SI) GO TO 100	ABCD1526
TSTD = 518.668D0	ABCD1527
PSTD = 1.0D0	ABCD1528
RA = .0252D0	ABCD1529
AJ = 2.719D0	ABCD1530
GO TO 101	ABCD1531
100 TSTD = 288.149D0	ABCD1532
PSTD = 101325.0D0	ABCD1533
RA = 286.9D0	ABCD1534
AJ = 1.0D0	ABCD1535
101 THETA = DSQRT(T2 / TSTD)	ABCD1536
DELTA = P2 / PSTD	ABCD1537
IF (IDES .NE. 1) GO TO 1	ABCD1538
WAFDS = WAF * DELTA / THETA	ABCD1539
1 CNF = PCNF / (100.0D0 * THETA)	ABCD1540
IF (ZF .LT. 0.0D0) ZF = 0.0D0	ABCD1541
IF (ZF .GT. 1.0D0) ZF = 1.0D0	ABCD1542

	CNFS = CNF	ABCD1543
	CALL SEARCH (ZF,CNF,PRF,WAF,ETAF,CNFXF(1),NCNF,PRXF(1,1),	ABCD1544
	1 WACXF(1,1),ETAXF(1,1),NPTF(1),15,15,IGO)	ABCD1545
	IF ((CNF - CNFS) .GT. .5D0 * TOLALL * CNF) MAPEDG = 1	ABCD1546
	IF (IGO .EQ. 1 .OR. IGO .EQ. 2) WRITE (8,12) CNFS, WLH(1,IGO),	ABCD1547
	1 WLH(2,IGO)	ABCD1548
	WAF = WAF * DELTA / THETA	ABCD1549
	IF (IDES .NE. 1) GO TO 2	ABCD1550
	PRFCF = (PRFDS - 1.0D0) / (PRF - 1.0D0)	ABCD1551
	ETAFCF = ETAFDS / ETAF	ABCD1552
	WAFCF = WAFDS / WAF	ABCD1553
	WRITE (6,13) PRFCF,ETAFCF,WAFCF,T2DS	ABCD1554
2	PRF = PRFCF * (PRF - 1.0D0) + 1.0D0	ABCD1555
	ETAF = ETAFCF * ETAF	ABCD1556
	WAF = WAFCF * WAF	ABCD1557
	WAFP = WAF	ABCD1558
	WAPC = WAF * WAFCF	ABCD1559
	PCNF = 100.0D0 * THETA * CNF	ABCD1560
	DUMD1(1) = PCNF	ABCD1561
	CALL THCOMP (PRF,ETAF,T2,H2,S2,P2,T22,H22,S22,P22)	ABCD1562
	IF (VFAN .EQ. 0.0D0) GO TO 21	ABCD1563
	Q(2) = 0.0D0	ABCD1564
	Q(3) = 0.0D0	ABCD1565
	H22P = H22	ABCD1566
	P22DOT = DERIV(4,P22)	ABCD1567
18	CALL THERMO (P22,H22,T22,S22,XX2,0,0.0D0,0)	ABCD1568
	WAF = WAFP - P22DOT * VFAN / T22 / 1.4D0 / RA	ABCD1569
	U22 = H22 - AJ * RA * T22	ABCD1570
	U22DOT = DERIV(5,U22)	ABCD1571
	H22X = (WAFP * H22P - (WAFP - WAF) * U22 - U22DOT * P22 * VFAN /	ABCD1572
	1 T22 / RA) / WAF	ABCD1573
	ERRW = (H22 - H22X) / H22	ABCD1574
	DIR = DSQRT(DABS(H22 / H22X))	ABCD1575
	CALL AFQUIR (Q(1),T22,ERRW,0.0D0,20.0D0,.1D0*TOLALL,DIR,T22T,IGO)	ABCD1576
	GO TO (19,21,20), IGO	ABCD1577
19	T22 = T22T	ABCD1578
	GO TO 18	ABCD1579
20	CALL ERROR	ABCD1580
21	IF (PCBLF .GT. 0.0D0) BLF = PCBLF * WAF	ABCD1581
	IF (JDES .EQ. 1) GO TO 9	ABCD1582
	JDES = 1	ABCD1583
	IF (INIT .EQ. 1) GO TO 8	ABCD1584
	IF (IDES .EQ. 1) GO TO 6	ABCD1585
	IF (JTRAN .EQ. 1) GO TO 9	ABCD1586
	IF (MODE .NE. 2) GO TO 3	ABCD1587
	T4 = GUESS(3,Y1,Y2,PCNF,PCNFDS,WFB,WFBDS,Y7,Y8,T4DS)	ABCD1588
	PCNI = GUESS(8,T4,T4DS,Y3,Y4,Y5,Y6,T22,T22DS,PCNIDS)	ABCD1589
	PCNC = GUESS(4,Y1,Y2,PCNI,PCNIDS,WFB,WFBDS,Y7,Y8,PCNCDS)	ABCD1590
	GO TO 7	ABCD1591
3	IF (MODE .EQ. 1) GO TO 5	ABCD1592
	IF (MODE .EQ. 0) GO TO 4	ABCD1593
	T4 = GUESS(7,Y1,Y2,PCNF,PCNFDS,Y5,Y6,T2,T2DS,T4DS)	ABCD1594
4	PCNC = GUESS(5,T4,T4DS,Y3,Y4,Y5,Y6,T22,T22DS,PCNCDS)	ABCD1595
	IF (FXM2CP) PCNC = PCNCDS * .99D0 * THETA	ABCD1596



	PCNCG1 = PCNC	ABCD1597
	PCNCG2 = PCNCDS	ABCD1598
	PCNI = GUESS(9,Y1,Y2,PCNCG1,PCNCG2,Y5,Y6,T22,T22DS,PCNIDS)	ABCD1599
	GO TO 7	ABCD1600
5	T4 = GUESS(6,Y1,Y2,PCNC,PCNCDS,Y5,Y6,T22,T22DS,T4DS)	ABCD1601
	PCNI = GUESS(8,T4,T4DS,Y3,Y4,Y5,Y6,T22,T22DS,PCNIDS)	ABCD1602
	GO TO 7	ABCD1603
6	T4 = T4DS	ABCD1604
	WFB = WFBDS	ABCD1605
	T21DS = T21	ABCD1606
7	ZC = ZCDS	ABCD1607
	ZI = ZIDS	ABCD1608
	PCNIGU = PCNI	ABCD1609
	PCNCGU = PCNC	ABCD1610
	T4GU = T4	ABCD1611
8	INIT = 0	ABCD1612
9	IF (MODE .NE. 3) GO TO 10	ABCD1613
	IF (DABS(CNF - CNFS) .LE. 1.0D0 * TOLALL * CNFS) GO TO 11	ABCD1614
	WRITE (8,14) CNFS,CNF	ABCD1615
	CALL ERROR	ABCD1615
10	PCNF = 100.0D0 * THETA * CNF	ABCD1617
11	CALL COINTC	ABCD1618
	RETURN	ABCD1619
C		ABCD1620
C		ABCD1621
12	FORMAT (19H0* * * CNF OFF MAP,P10.4,2X,A4,A2,11H* * *\$\$\$\$\$)	ABCD1622
13	FORMAT (11H0FAN DESIGN,13X,8H PRFCF=,E15.8,PH ETAFCF=,E15.8,	ABCD1623
	1 8H WAFCF=,E15.8,8H T2DS=,E15.8)	ABCD1624
14	FORMAT (10H0CNF WAS= ,E15.3,11H AND NOW= ,E15.8,12H CHECK PCNF,	ABCD1625
	1 12H INPUT\$\$\$\$\$)	ABCD1625
	END	ABCD1627

Subroutine COHPTB

	SUBROUTINE COHPTB	ABCD1623
	IMPLICIT REAL*8 (A-H,O-Z)	ABCD1629
	LOGICAL SI, DUMSPL, FXFN2M	ABCD1630
	COMMON /COMALL/ COM(1062)	ABCD1631
	COMMON /COMDAT/ COMD(5423)	ABCD1632
	DIMENSION WORD(2), ERR(9), TFFXH(15), CNXH(15,15), DHTCXH(15,15),	ABCD1633
1	ETATXH(15,15), NPTTFH(15)	ABCD1634
	DIMENSION Q(9), AWORD(2), WLO(2), WHI(2)	ABCD1635
	EQUIVALENCE (WORD(1), COM(1)), (IDES, COM(3)), (NOMAP, COM(2)),	ABCD1636
1	(TOLALL, COM(23)), (EFF(1), COM(24)), (T5, COM(102)), (H5,	ABCD1637
2	COM(103)), (S5, COM(104)), (W35, COM(105)), (FAR5, COM(106)),	ABCD1638
3	(TFHPCF, COM(114)), (CNHPCF, COM(115)), (ETHPCF, COM(116)),	ABCD1639
4	(DHHPCF, COM(117)), (TFHPDS, COM(118)), (CNHPDS, COM(119)),	ABCD1640
5	(ETHPDS, COM(120)), (HPEXT, COM(129)), (TFFIP, COM(141)),	ABCD1641
6	(CNIP, COM(142)), (ETATIP, COM(143)), (DHTCIP, COM(144)),	ABCD1642
7	(DHTI, COM(145)), (H3, COM(153)), (T4, COM(156)), (H4, COM(157)),	ABCD1643
8	(S4, COM(158)), (WG4, COM(159)), (FAR4, COM(160)),	ABCD1644
9	(T50, COM(161)), (H50, COM(162)), (S50, COM(163)),	ABCD1645
1	(WG50, COM(164)), (FAR50, COM(165)), (CNHP, COM(171)),	ABCD1646
2	(ETATHP, COM(172)), (DHTCHP, COM(173)), (DHTC, COM(174)),	ABCD1647

3	(TFFHP, COM(175)), (H21, COM(264)), (PCNC, COM(301)),	ABCD1648
4	(BLHP, COM(313)), (XNHP, COM(372)), (P4, COM(381)),	ABCD1649
5	(P50, COM(383)), (U50, COM(384)), (P5, COM(385)),	ABCD1650
6	(VHPTRB, COM(399)), (WACP, COM(422)), (XNHPDS, COM(423)),	ABCD1651
7	(PMIHP, COM(426)), (ISPOOL, COM(1044)), (SI, COM(1055)),	ABCD1652
8	(DUMSPL, COM(1057)), (FXFN2M, COM(1058))	ABCD1653
	EQUIVALENCE (TFFXH(1), COMD(3226)), (CNXH(1,1), COMD(3241)),	ABCD1654
1	(DHTCXH(1,1), COMD(3466)), (ETATXH(1,1), COMD(3691)),	ABCD1655
2	(NTFFSH, COMD(5376)), (NPITFH(1), COMD(5377))	ABCD1656
	DATA AWORD, WLO, WHI /4HCJHP, 4HTB , 4H (LO, 4H) , 4H (HI,	ABCD1657
1	4H) /	ABCD1658
	WORD(1) = AWORD(1)	ABCD1659
	WORD(2) = AWORD(2)	ABCD1660
	IF (SI) GO TO 100	ABCD1661
	RA = .0252D0	ABCD1662
	AJ = 2.719D0	ABCD1663
	CONFAC = 1.4091D-5	ABCD1664
	GO TO 101	ABCD1665
100	RA = 286.9D0	ABCD1666
	AJ = 1.0D0	ABCD1667
	CONFAC = 1.0966D-2	ABCD1668
101	IF (ISPOOL .EQ. 1) GO TO 8	ABCD1669
	THDE = DSQRT(T4) / PCNC	ABCD1670
	IF (IDES .EQ. 0) GO TO 1	ABCD1671
	CNHPCF = CNHPDS * THDE	ABCD1672
1	CNHP = CNHPCF / THDE	ABCD1673
	CNHPS = CNHP	ABCD1674
	TFFHPS = TFFHP	ABCD1675
	CALL SEARCH (-1.D0, TFFHP, CNHP, DHTCHP, ETATHP, TFFXH(1), NTFFSH,	ABCD1676
1	CNXH(1,1), DHTCXH(1,1), ETATXH(1,1), NPITFH(1), 15, 15, IGO)	ABCD1677
	IF (IGO .EQ. 1 .OR. IGO .EQ. 11 .OR. IGO .EQ. 21)	ABCD1678
1	WRITE (8,9) TFFHPS, WLO	ABCD1679
	IF (IGO .EQ. 2 .OR. IGO .EQ. 12 .OR. IGO .EQ. 22)	ABCD1680
1	WRITE (8,9) TFFHPS, WHI	ABCD1681
	IF (IGO .EQ. 10 .OR. IGO .EQ. 11 .OR. IGO .EQ. 12)	ABCD1682
1	WRITE (8,10) CNHPS, WLO	ABCD1683
	IF (IGO .EQ. 20 .OR. IGO .EQ. 21 .OR. IGO .EQ. 22)	ABCD1684
1	WRITE (8,10) CNHPS, WHI	ABCD1685
	IF (IGO .NE. 7) GO TO 2	ABCD1686
	CALL ERROR	ABCD1687
	RETURN	ABCD1688
2	NOMAP = 0	ABCD1689
	TFHCAL = WG4 * DSQRT(T4) / (14.596D0 * P4)	ABCD1690
	BTUEXT = 0.706705D0 * HPEXT	ABCD1691
	IF (.NOT. SI) GO TO 102	ABCD1692
	TFHCAL = WG4 * DSQRT(T4) / P4	ABCD1693
	BTUEXT = HPEXT	ABCD1694
102	XNHP = XNHPDS * PCNC / 100.0D0	ABCD1695
	XNHDOT = DERIV(1, XNHP)	ABCD1696
	DHTCC = (BTUEXT + WACP * (H3 - H21) + CONFAC * PMIHP * XNHP *	ABCD1697
1	XNHDOT) / (WG4 * T4)	ABCD1698
	IF (IDES .EQ. 0) GO TO 5	ABCD1699
	TFHPCF = TFHPDS / TFHCAL	ABCD1700
	DHHPCF = DHTCC / DHTCHP	ABCD1701

	ETHPCF = ETHPDS / ETATHP	ABCD1702
	WRITE (6,11) CNHPCF,TFHPCF,ETHPCF,DHHPCF	ABCD1703
5	TFHCAL = TFHPCF * TFHCAL	ABCD1704
	DHTCHP = DHHPCF * DHTCHP	ABCD1705
	ETATHP = ETHPCF * ETATHP	ABCD1706
	DHTC = DHTCC * T4	ABCD1707
	ERR(1) = (TFHCAL - TFFHP) / TFHCAL	ABCD1708
	ERR(2) = (DHTCC - DHTCHP) / DHTCC	ABCD1709
	CALL THTURB (DHTC,ETATHP,FAR4,H4,S4,P4,T50,H50,S50,P50)	ABCD1710
	IF (BLHP .LE. 0.0D0) GO TO 6	ABCD1711
	FAR50 = FAR4 * WG4 / (WG4 + BLHP * (FAR4 + 1.0D0))	ABCD1712
	WG50 = WG4 + BLHP	ABCD1713
	H50 = (BLHP * H3 + WG4 * H50) / WG50	ABCD1714
	CALL THERMO (P50,H50,T50,S50,XX2,1,FAR50,1)	ABCD1715
	GO TO 7	ABCD1716
6	FAR50 = FAR4	ABCD1717
	WG50 = WG4	ABCD1718
7	IF (VHPTRB .EQ. 0.0D0) GO TO 21	ABCD1719
	Q(2) = 0.0D0	ABCD1720
	Q(3) = 0.0D0	ABCD1721
	WG50P = WG50	ABCD1722
	H50P = H50	ABCD1723
	P50DOT = DERIV(12,P50)	ABCD1724
18	CALL THERMO (P50,H50,T50,S50,XX2,1,FAR50,0)	ABCD1725
	WG50 = WG50P - P50DOT * VHPTRB / T50 / 1.4D0 / RA	ABCD1726
	U50 = H50 - RA * AJ * T50	ABCD1727
	U50DOT = DERIV(13,U50)	ABCD1728
	H50X = (WG50P * H50P - (WG50P - WG50) * U50 - U50DOT * P50 * 1 VHPTRB / T50 / RA) / WG50	ABCD1729 ABCD1730
	ERRW = (H50 - H50X) / H50	ABCD1731
	DIR = DSQRT(DABS(H50 / H50X))	ABCD1732
	CALL AFQUIR (Q(1),T50,ERFW,0.0D0,20.0D0,.1D0*TOLALL,DIR,T50T,IGO)	ABCD1733
	GO TO (19,21,20), IGO	ABCD1734
19	T50 = T50T	ABCD1735
	GO TO 18	ABCD1736
20	CALL ERROR	ABCD1737
21	IF (FXFN2M .OR. DUMSPL) GO TO 8	ABCD1738
	CALL COIPTB	ABCD1739
	RETURN	ABCD1740
8	P5 = P50	ABCD1741
	H5 = H50	ABCD1742
	T5 = T50	ABCD1743
	S5 = S50	ABCD1744
	FAR5 = FAR50	ABCD1745
	WG5 = WG50	ABCD1746
C	SET MIDDLE TURBINE PARAMETERS TO ZERO, NOT USED	ABCD1747
	TFFIP = 0.0D0	ABCD1748
	CNIP = 0.0D0	ABCD1749
	DHTI = 0.0D0	ABCD1750
	DHTCIP = 0.0D0	ABCD1751
	ETATIP = 0.0D0	ABCD1752
	CALL COLPTB	ABCD1753
	RETURN	ABCD1754
C		ABCD1755

C		ABCD1756
C		ABCD1757
9	FORMAT (19H0*****TFFHP OFF MAP,F10.4,2X,A4,A2,11H*****\$\$\$\$F\$)	ABCD1758
10	FORMAT (19H0*****CNHP OFF MAP,F10.4,2X,A4,A2,11H*****\$\$\$\$F\$)	ABCD1759
11	FORMAT(20H0H.P. TURBINE DESIGN,5X,7HCNHPCF=,E15.8,8H TFFHPCF=,	ABCD1760
	1 E15.8,8H ETHPCF=,E15.8,8H DHHPCF=,E15.8)	ABCD1761
	END	ABCD1762

Subroutine COINLT

	SUBROUTINE COINLT	ABCD1753
	IMPLICIT REAL*8 (A-H,O-Z)	ABCD1764
	LOGICAL SI	ABCD1765
	COMMON /COMALL/ COM(1062)	ABCD1766
	DIMENSION WORD(2)	ABCD1767
	DIMENSION AWORD(2)	ABCD1768
	EQUIVALENCE (WORD(1), COM(1)), (IDES, COM(3)), (MODE, COM(6)),	ABCD1769
	1 (INIT, COM(7)), (IAMTP, COM(9)), (TOLALL, COM(23)), (P1,	ABCD1770
	2 COM(33)), (T2DS, COM(91)), (T2, COM(92)), (P2, COM(93)), (H2,	ABCD1771
	3 COM(94)), (S2, COM(95)), (T4DS, COM(101)), (PCNFDS, COM(124)),	ABCD1772
	4 (ZF, COM(136)), (PCNF, COM(137)), (T1, COM(149)), (H1, COM(150)),	ABCD1773
	5 (S1, COM(151)), (T4, COM(156)), (WFBDS, COM(185)), (ZFDS,	ABCD1774
	6 COM(186)), (ETAR, COM(187)), (WFB, COM(192)), (CS, COM(194)),	ABCD1775
	7 (AM, COM(195)), (ALTP, COM(196)), (PCNFGU, COM(199)),	ABCD1776
	8 (PCNC, COM(301)), (PCNCDS, COM(303)), (DELT1, COM(429)),	ABCD1777
	9 (SI, COM(1055))	ABCD1778
	DATA AWORD /4HCOIN, 4HLT /	ABCD1779
	WORD(1) = AWORD(1)	ABCD1780
	WORD(2) = AWORD(2)	ABCD1781
	IF (SI) GO TO 10	ABCD1782
	AJ = 778.26D0	ABCD1783
	G = 32.174049D0	ABCD1784
	REF59 = 2.0855531D07	ABCD1785
	R = 1.986375D0	ABCD1786
	TSTD = 518.668D0	ABCD1787
	GO TO 11	ABCD1788
10	AJ = 1.0D0	ABCD1789
	G = 1.0D0	ABCD1790
	REF59 = 6.3567658D06	ABCD1791
	R = 8314.34D0	ABCD1792
	TSTD = 288.149D0	ABCD1793
11	ALT = ALTP * REF59 / (REF59 - ALTP)	ABCD1794
	GAJ2 = 2.0D0 * G * AJ	ABCD1795
	CALL ATMOS (ALT,T1STD,XX1,XX2,XX3,DELTA,CS,XX4,IIER)	ABCD1796
	P1 = DELTA	ABCD1797
	IF (SI) P1 = 101325.0D0 * DELTA	ABCD1798
	T1 = T1STD	ABCD1799
	IF (IAMTP.EQ. 2) T1 = T1STD + DELT1	ABCD1800
	IF (IAMTP.EQ. 5) CALL RAM2 (AM,ETAR)	ABCD1801
	IF (IAMTP.NE. 1.AND. IAMTP.NE. 5) CALL RAM (AM,ETAR)	ABCD1802
	FAR = 0.0D0	ABCD1803
	CALL PROCOM (FAR,T1,CS,XX2,XX3,R1,PHI1,H1)	ABCD1804
	S1 = PHI1 - R1 * DLOG(DELTA)	ABCD1805
	H2 = H1 + (AM * CS) ** 2 / GAJ2	ABCD1806

	P2T = 1.0D0	ABCD1807
	IF (SI) P2T = 101325.0D0	ABCD1808
	DO 1 I = 1,50	ABCD1809
	CALL THERMO (P2T,H2,T2T,S2T,AW,0,0.0D0,1)	ABCD1810
	IF (DABS(S2T - S1) .LE. .1D0 * TOLALL * S1) GO TO 2	ABCD1811
1	P2T = P1 * DEXP((AW / R) * ((S2T - S1) + (R / AW) * 1 DLOG(P2T / P1)))	ABCD1812
	CALL ERROR	ABCD1813
	RETURN	ABCD1814
2	IF (IAMTP .EQ. 3 .OR. IAMTP .EQ. 4) ETAR = P2 / P2T	ABCD1815
	P2 = ETAR * P2T	ABCD1816
	ITHER = 1	ABCD1817
	IF (IAMTP .EQ. 4) ITHER = 0	ABCD1818
	CALL THERMO (P2,H2,T2,S2,XX5,0,0.0D0,ITHER)	ABCD1819
	IF (INIT .EQ. 1) RETURN	ABCD1820
	IF (IDES .EQ. 1) GO TO 3	ABCD1821
	IF (MODE .EQ. 3) GO TO 4	ABCD1822
	PCNF = GUESS(MODE,T4,T4DS,PCNC,PCNCDS,WFB,WFBDS,T2,T2DS,PCNFDS)	ABCD1823
	PCNFGU = PCNF	ABCD1824
	GO TO 4	ABCD1825
3	PCNF = PCNFDS * DSQRT(T2 / TSTD)	ABCD1826
	PCNFGU = PCNF	ABCD1827
	T2DS = T2	ABCD1828
4	ZF = ZFDS	ABCD1829
	RETURN	ABCD1830
	END	ABCD1831
		ABCD1832

Subroutine COINTC

	SUBROUTINE COINTC	ABCD1833
	IMPLICIT REAL*8 (A-H,O-Z)	ABCD1834
	LOGICAL SI, DUMSPL, FXFN2M, AFTFAN, FAN	ABCD1835
	COMMON /COMALL/ COM(1062)	ABCD1836
	COMMON /COMDAT/ COMD(5423)	ABCD1837
	DIMENSION WORD(2), CNXIN(15), PRXIN(15,15), WACXIN(15,15),	ABCD1838
1	ETAXIN(15,15), CNXXI(15), PRXXI(15,15), WACXXI(15,15),	ABCD1839
2	ETAXXI(15,15), NPTI(15), NPTXI(15)	ABCD1840
	DIMENSION Q(9), WLH(2,2), AWORD(2)	ABCD1841
	EQUIVALENCE (WORD(1), COM(1)), (IDES, COM(3)), (MAPEDG, COM(22)),	ABCD1842
1	(TOLALL, COM(23)), (H22, COM(34)), (T2, COM(92)), (P2, COM(93)),	ABCD1843
2	(H2, COM(94)), (S2, COM(95)), (S22, COM(96)), (T2DS, COM(97)),	ABCD1844
3	(CNF, COM(134)), (ZI, COM(139)), (PCNI, COM(140)), (PCNIDS,	ABCD1845
4	COM(147)), (PRICF, COM(176)), (ETAICF, COM(177)), (WAICF,	ABCD1846
5	COM(178)), (PFIDS, COM(180)), (ETAIDS, COM(181)), (WAIDS,	ABCD1847
6	COM(182)), (WAICDS, COM(183)), (ETAID, COM(188)), (PRI, COM(189)),	ABCD1848
7	(WAC, COM(191)), (T21, COM(263)), (H21, COM(264)),	ABCD1849
8	(S21, COM(265)), (WA21, COM(266)), (T22, COM(269)),	ABCD1850
9	(WA22, COM(269)), (WA32, COM(271)), (PCBLI, COM(304)),	ABCD1851
1	(PCBLID, COM(305)), (CNI, COM(309)), (WACI, COM(310)),	ABCD1852
2	(WAI, COM(311)), (BLI, COM(312)), (BLF, COM(316)),	ABCD1853
3	(WAF, COM(319)), (P22, COM(375)), (P21, COM(377)),	ABCD1854
4	(U21, COM(378)), (VINTC, COM(396)), (WAIP, COM(421)),	ABCD1855
5	(ISPOOL, COM(1044)), (SI, COM(1055)), (DUMSPL, COM(1057)),	ABCD1856
6	(FXFN2M, COM(1058)), (AFTFAN, COM(1060)), (FAN, COM(1061))	ABCD1857

	EQUIVALENCE (CNXIN(1), COMD(691)), (PRXIN(1,1), COMD(706)),	ABCD1858
	1 (WACXIN(1,1), COMD(931)), (ETAXIN(1,1), COMD(1156)),	ABCD1859
	2 (CNXXI(1), COMD(1381)), (PRXXI(1,1), COMD(1396)),	ABCD1860
	3 (WACXXI(1,1), COMD(1621)), (ETAXXI(1,1), COMD(1846)),	ABCD1861
	4 (NCNI, COMD(5312)), (NPTI(1), COMD(5313)), (NCNXI, COMD(5328)),	ABCD1862
	5 (NPTXI(1), COMD(5329))	ABCD1863
	DATA AWORD, WLH /4HCOIN, 4HTC , 4H (LO, 4H) , 4H (HI, 4H) /	ABCD1864
	WORD(1) = AWORD(1)	ABCD1865
	WORD(2) = AWORD(2)	ABCD1866
	IF (SI) GO TO 100	ABCD1867
	TSTD = 518.668D0	ABCD1868
	PSTD = 1.0D0	ABCD1869
	RA = .0252D0	ABCD1870
	AJ = 2.719D0	ABCD1871
	GO TO 101	ABCD1872
100	TSTD = 288.149D0	ABCD1873
	PSTD = 101325.0D0	ABCD1874
	RA = 286.9D0	ABCD1875
	AJ = 1.0D0	ABCD1876
101	IF (.NOT. AFTFAN) GO TO 1	ABCD1877
	T22S = T22	ABCD1878
	H22S = H22	ABCD1879
	S22S = S22	ABCD1880
	P22S = P22	ABCD1881
	T22 = T2	ABCD1882
	H22 = H2	ABCD1883
	S22 = S2	ABCD1884
	P22 = P2	ABCD1885
1	THETA = DSQRT(T22 / TSTD)	ABCD1886
	DELTA = P22 / PSTD	ABCD1887
	IF (.NOT. FAN) WAI = WAF - PLF	ABCD1888
	IF (IDES .NE. 1) GO TO 2	ABCD1889
	PCNI = PCNIDS * THETA	ABCD1890
	PR1 = PRIDS	ABCD1891
	PCBLI = PCBLID	ABCD1892
	IF (FAN) GO TO 102	ABCD1893
	WAICDS = WAI * THETA / DELTA	ABCD1894
	DUMSPL = .TRUE.	ABCD1895
102	WACI = WAICDS	ABCD1896
	WAIDS = WACI * DELTA / THETA	ABCD1897
	ETAI = ETAIDS	ABCD1898
2	IF (.NOT. FXFN2M) GO TO 3	ABCD1899
C	FAN AND MIDDLE SPOOL ROTATE AT SAME SPEED	ABCD1900
	SPDFAN = CNF * DSQRT(T2 / TSTD)	ABCD1901
	CNI = SPDFAN / THETA	ABCD1902
	PCNI = 100.0D0 * THETA * CNI	ABCD1903
	IF (IDES .EQ. 1) PCNIDS = PCNI / THETA	ABCD1904
3	CNI = PCNI / (100.0D0 * THETA)	ABCD1905
	ZI = DMAX1(ZI, 0.0D0)	ABCD1906
	ZI = DMIN1(ZI, 1.0D0)	ABCD1907
	CNIS = CNI	ABCD1908
	IF (.NOT. DUMSPL) GO TO 4	ABCD1909
	CALL INDUMY (CNI, ZI, WAICDS, IDES)	ABCD1910
	CALL SEARCH (ZI, CNI, PR1, WACI, ETAI, CNXXI(1), NCNXI, PRXXI(1,1),	ABCD1911

1	WACXXI(1,1),ETAXXI(1,1),NPTXI(1),15,15,IGO)	ABCD1912
	GO TO 5	ABCD1913
4	CALL SEAPCH (ZI,CNI,PRI,WACI,ETAI,CNXIN(1),NCNI,PRXIN(1,1),	ABCD1914
1	WACXIN(1,1),ETAXIN(1,1),NPTI(1),15,15,IGO)	ABCD1915
5	IF ((CNI - CNIS) .GT. .5D0 * TOLALL * CNI) MAPEDG = 1	ABCD1916
	IF (IGO .EQ. 1 .OR. IGO .EQ. 2) WRITE (8,12) CNIS,WLH(1,IGO),	ABCD1917
1	WLH(2,IGO)	ABCD1918
	IF (.NOT. FAN) WACI = WAI * THETA / DELTA	ABCD1919
	WAI = WACI * DELTA / THETA	ABCD1920
	WA22 = WAI	ABCD1921
	IF (IDES .NE. 1) GO TO 7	ABCD1922
	T22DS = T22	ABCD1923
	IF (APTFAN) T22DS = T22S	ABCD1924
	ETAICF = ETAIDS / ETAI	ABCD1925
	WAICF = WAIDS / WAI	ABCD1926
	PRICF = (PRIDS - 1.0D0) / (PEI - 1.0D0)	ABCD1927
	IF (.NOT. DUMSPL) GO TO 5	ABCD1928
	PRICF = 1.0D0	ABCD1929
	ETAICF = 1.0D0	ABCD1930
	WAICF = 1.0D0	ABCD1931
6	WRITE (6,13) PRICF,ETAICF,WAICF,T22DS	ABCD1932
7	PRI = PRICF * (PRI - 1.0D0) + 1.0D0	ABCD1933
	ETAI = ETAICF * ETAI	ABCD1934
	WAI = WAICF * WAI	ABCD1935
	WAIP = WAI	ABCD1936
	WACI = WACI * WAICF	ABCD1937
	WA22 = WAI	ABCD1938
	CALL THCOMP (PRI,ETAI,T22,H22,S22,P22,T21,H21,S21,P21)	ABCD1939
	IF (VINTC .EQ. 0.0D0) GO TO 21	ABCD1940
	Q(2) = 0.0D0	ABCD1941
	Q(3) = 0.0D0	ABCD1942
	H21P = H21	ABCD1943
	P21DOT = DERIV(6,P21)	ABCD1944
18	CALL THERMO (P21,H21,T21,S21,XX2,0,0.0D0,0)	ABCD1945
	WAI = WAIP - P21DOT * VINTC / T21 / 1.4D0 / PA	ABCD1946
	U21 = H21 - AJ * RA * T21	ABCD1947
	U21DOT = DERIV(7,U21)	ABCD1948
	H21X = (WAIP * H21P - (WAIP - WAI) * U21 - U21DOT * P21 * VINTC /	ABCD1949
1	T21 / RA) / WAI	ABCD1950
	ERRW = (H21 - H21X) / H21	ABCD1951
	DIR = DSQRT(DABS(H21 / H21X))	ABCD1952
	CALL AFQUIR (Q(1),T21,ERRW,0.0D0,20.0D0,.1D0*TOLALL,DIR,T21T,IGO)	ABCD1953
	GO TO (19,21,20), IGO	ABCD1954
19	T21 = T21T	ABCD1955
	GO TO 18	ABCD1956
20	CALL ERROR	ABCD1957
21	IF (.NOT. DUMSPL) GO TO 9	ABCD1958
	PRI = 1.0D0	ABCD1959
	ETAI = 1.0D0	ABCD1960
	T21 = T22	ABCD1961
	H21 = H22	ABCD1962
	S21 = S22	ABCD1963
	P21 = P22	ABCD1964
	IF (ISPOOL .EQ. 1) WA21 = WAI	ABCD1965

8	IF (IDES .NE. 1) GO TO 9	ABCD1966
	BLI = PCELI * WAI	ABCD1967
	WA21 = WA22 - BLI	ABCD1968
	WA32 = BLI	ABCD1969
	IF (FAN .OR. IDES .EQ. 1) WAC = WA21	ABCD1970
9	IF (DARS(CNI - CNIS) .LE. 1.0D0 * TOLALL * CNIS) GO TO 10	ABCD1971
	WRITE (8,14) CNIS,CNI	ABCD1972
	CALL ERROR	ABCD1973
	PCNI = 100.0D0 * THETA * CNI	ABCD1974
10	IF (.NOT. AFTFAN) GO TO 11	ABCD1975
	T22 = T22S	ABCD1976
	H22 = H22S	ABCD1977
	S22 = S22S	ABCD1978
	P22 = P22S	ABCD1979
11	CALL COCOMP	ABCD1980
	RETURN	ABCD1981
C		ABCD1982
C		ABCD1983
C		ABCD1984
12	FORMAT (19H0* * * CNI OFF MAP,F10.4,2X,A4,A2,11H* * *\$\$\$\$\$)	ABCD1985
13	FORMAT(20H0MIDDLE SPOOL DESIGN,4X,8H PRICF=,E15.8,8H ETAICF=,	ABCD1986
	1 E15.8,8H WAICF=,E15.8,8H T22DS=,E15.8)	ABCD1987
14	FORMAT (10HOCNI WAS= ,E15.8,11H AND NOW= ,E15.8,12H CHECK PCNI,	ABCD1988
	1 12H INPUT\$\$\$\$\$)	ABCD1989
	END	ABCD1990

Subroutine COIPTB

SUBROUTINE COIPTB	ABCD1991
IMPLICIT REAL*8 (A-H,O-Z)	ABCD1992
LOGICAL SI, FXM2CP, AFTFAN	ABCD1993
COMMON /COMALL/ COM(1062)	ABCD1994
COMMON /COMDAT/ COMD(5423)	ABCD1995
DIMENSION WORD(2), ERR(9), TFFXH(15), CNXH(15,15), DHTCXH(15,15),	ABCD1996
1 ETATXH(15,15), TFFXI(15), CNXI(15,15), DHTCXI(15,15),	ABCD1997
2 ETATXI(15,15), NPTTFH(15), NPTTFI(15)	ABCD1998
DIMENSION Q(9), AWORD(2), WLO(2), WHI(2)	ABCD1999
EQUIVALENCE (WORD(1), COM(1)), (IDES, COM(3)), (NOMAP, COM(2)),	ABCD2000
1 (TOLALL, COM(23)), (ERR(1), COM(24)), (H22, COM(34)), (H2,	ABCD2001
2 COM(94)), (T5, COM(102)), (H5, COM(103)), (S5, COM(104)), (WG5,	ABCD2002
3 COM(105)), (FAR5, COM(106)), (TFHPDS, COM(118)), (CNHPDS,	ABCD2003
4 COM(119)), (ETHPDS, COM(120)), (HPEXT, COM(129)), (PCNI,	ABCD2004
5 COM(140)), (TFFIP, COM(141)), (CNIP, COM(142)), (ETATIP,	ABCD2005
6 COM(143)), (DHTCIP, COM(144)), (DHTI, COM(145)), (H3, COM(153)),	ABCD2006
7 (T50, COM(161)), (H50, COM(162)), (S50, COM(163)),	ABCD2007
8 (WG50, COM(164)), (FAR50, COM(165)), (H21, COM(264)),	ABCD2008
9 (TFIPDS, COM(278)), (CNIPDS, COM(279)), (ETIPDS, COM(280)),	ABCD2009
1 (TFIPCF, COM(285)), (CNIPCF, COM(286)), (ETIPCF, COM(287)),	ABCD2010
2 (DHIPCF, COM(288)), (BLIP, COM(314)), (XNIP, COM(373)),	ABCD2011
3 (P50, COM(383)), (P5, COM(385)), (U5, COM(386)),	ABCD2012
4 (VIPTRB, COM(400)), (WAIP, COM(421)), (WACP, COM(422)),	ABCD2013
5 (XNIPDS, COM(424)), (PMIIP, COM(427)), (SI, COM(1055)),	ABCD2014
6 (FXM2CP, COM(1059)), (AFTFAN, COM(1060))	ABCD2015
EQUIVALENCE (TFFXH(1), COMD(3226)), (CNXH(1,1), COMD(3241)),	ABCD2016

1	(DHTCXH(1,1), COMD(3466)), (ETATXH(1,1), COMD(3691)),	ABCD2017
2	(TFFXI(1), COMD(3916)), (CNXI(1,1), COMD(3931)),	ABCD2018
3	(DHTCXI(1,1), COMD(4156)), (ETATXI(1,1), COMD(4381)),	ABCD2019
4	(NTFFSH, COMD(5376)), (NPTTFH(1), COMD(5377)),	ABCD2020
5	(NTFFSI, COMD(5392)), (NPTTFI(1), COMD(5393))	ABCD2021
	DATA AWORD, WLO, WHI /4HCOIP, 4HTB , 4H (LO, 4H) , 4H (HI,	ABCD2022
	1 4H) /	ABCD2023
	IF (SI) GO TO 100	ABCD2024
	RA = .0252D0	ABCD2025
	AJ = 2.719D0	ABCD2026
	CONFAC = 1.4091D-5	ABCD2027
	GO TO 101	ABCD2028
100	RA = 286.9D0	ABCD2029
	AJ = 1.0D0	ABCD2030
	CONFAC = 1.0966D-2	ABCD2031
101	H22SAV = H22	ABCD2032
	IF (AFTFAN) H22 = H2	ABCD2033
	WORD(1) = AWORD(1)	ABCD2034
	WORD(2) = AWORD(2)	ABCD2035
	THDE = DSQRT(T50) / PCNI	ABCD2036
	IF (IDES .EQ. 0) GO TO 1	ABCD2037
	CNIPCF = CNIPDS * THDE	ABCD2038
	IF (FXM2CP) CNIPCF = CNHPDS * THDE	ABCD2039
1	CNIP = CNIPCF / THDE	ABCD2040
	CNIPS = CNIP	ABCD2041
	TFFIPS = TFFIP	ABCD2042
	IF (FXM2CP) GO TO 2	ABCD2043
	CALL SEARCH (-1.0D0, TFFIP, CNIP, DHTCIP, ETATIP, TFFXI(1), NTFFSI,	ABCD2044
	1 CNXI(1,1), DHTCXI(1,1), ETATXI(1,1), NPTTFI(1), 15, 15, IGO)	ABCD2045
	GO TO 104	ABCD2046
2	CALL SEARCH (-1.0D0, TFFIP, CNIP, DHTCIP, ETATIP, TFFXH(1), NTFFSH,	ABCD2047
	1 CNXH(1,1), DHTCXH(1,1), ETATXH(1,1), NPTTFH(1), 15, 15, IGO)	ABCD2048
104	IF (IGO .EQ. 1 .OR. IGO .EQ. 11 .OR. IGO .EQ. 21)	ABCD2049
	1 WRITE (8,9) TFFIPS, WLO	ABCD2050
	IF (IGO .EQ. 2 .OR. IGO .EQ. 12 .OR. IGO .EQ. 22)	ABCD2051
	1 WRITE (8,9) TFFIPS, WHI	ABCD2052
	IF (IGO .EQ. 30 .OR. IGO .EQ. 11 .OR. IGO .EQ. 12)	ABCD2053
	1 WRITE (8,10) CNIPS, WLO	ABCD2054
	IF (IGO .EQ. 50 .OR. IGO .EQ. 21 .OR. IGO .EQ. 22)	ABCD2055
	1 WRITE (8,10) CNIPS, WHI	ABCD2056
	IF (IGO .NE. 7) GO TO 3	ABCD2057
	CALL ERROR	ABCD2058
	RETURN	ABCD2059
3	NOMAP = 0	ABCD2060
	TFICAL = WG50 * DSQRT(T50) / (14.696D0 * P50)	ABCD2061
	IF (SI) TFICAL = WG50 * DSQRT(T50) / P50	ABCD2062
	XNIP = XNIPDS * PCNI / 100.0D0	ABCD2063
	XNIDOT = DERIV(2, XNIP)	ABCD2064
	BTUEXT = .706705D0 * HPEXT	ABCD2065
	IF (SI) BTUEXT = HPEXT	ABCD2066
	DHACEL = CONFAC * PMIIP * XNIP * XNIDOT	ABCD2067
	DHTIC = (WAIP * (H21 - H22) + DHACEL) / (WG50 * T50)	ABCD2068
	IF (FXM2CP) DHTIC = (BTUEXT + WACP * (H3 - H21) + WAIP *	ABCD2069
	1 (H21 - H22) + DHACEL) / (WG50 * T50)	ABCD2070

	IF (IDES .EQ. 0) GO TO 6	ABCD2071
	TFIPCF = TFIPDS / TFICAL	ABCD2072
	DHPCF = DHTIC / DHTCIP	ABCD2073
	ETPCF = ETIPDS / ETATIP	ABCD2074
	IF (.NOT. FXM2CP) GO TO 102	ABCD2075
	TFIPCF = TFHPDS / TFICAL	ABCD2076
	ETPCF = ETHPDS / ETATIP	ABCD2077
102	WRITE (6,11) CNPCF,TFIPCF,ETPCF,DHPCF	ABCD2078
6	TFICAL = TFIPCF * TFICAL	ABCD2079
	DHTCIP = DHPCF * DHTCIP	ABCD2080
	ETATIP = ETPCF * ETATIP	ABCD2081
	DHTI = DHTIC * T50	ABCD2082
	N1 = 8	ABCD2083
	N2 = 9	ABCD2084
	IF (.NOT. FXM2CP) GO TO 103	ABCD2085
	N1 = 1	ABCD2086
	N2 = 2	ABCD2087
103	ERR(N1) = (TFICAL - TFFIP) / TFICAL	ABCD2088
	ERR(N2) = (DHTIC - DHTCIP) / DHTIC	ABCD2089
	CALL THTURB (DHTI,ETATIP,FAR50,H50,S50,P50,T5,H5,S5,P5)	ABCD2090
	IF (BLIP .LE. 0.0D0) GO TO 7	ABCD2091
	FAR5 = FAR50 * WG50 / (WG50 + BLIP * (FAR50 + 1.0D0))	ABCD2092
	WG5 = WG50 + BLIP	ABCD2093
	H5 = (BLIP * H3 + WG50 * H5) / WG5	ABCD2094
	CALL THERMO (P5,H5,T5,S5,XX2,1,FAR5,1)	ABCD2095
	GO TO 8	ABCD2096
7	FAR5 = FAR50	ABCD2097
	WG5 = WG50	ABCD2098
8	IF (VIPTRB .EQ. 0.0D0) GO TO 21	ABCD2099
	Q(2) = 0.0D0	ABCD2100
	Q(3) = 0.0D0	ABCD2101
	WG5P = WG5	ABCD2102
	H5P = H5	ABCD2103
	P5DOT = DERIV(14,P5)	ABCD2104
19	CALL THERMO (P5,H5,T5,S5,XX2,1,FAR5,0)	ABCD2105
	WG5 = WG5P - P5DOT * VIPTRB / T5 / 1.4D0 / RA	ABCD2106
	U5 = H5 - RA * AJ * T5	ABCD2107
	U5DOT = DERIV(15,U5)	ABCD2108
	H5X = (WG5P * H5P - (WG5P - WG5) * U5 - U5DOT * P5 * VIPTRB /	ABCD2109
	1 T5 / RA) / WG5	ABCD2110
	EPRW = (H5 - H5X) / H5	ABCD2111
	DIR = DSQRT(DABS(H5 / H5X))	ABCD2112
	CALL AFQUIR (Q(1),T5,ERRW,0.0D0,20.0D0,.1D0*TOLALL,DIR,T5T,IGO)	ABCD2113
	GO TO (19,21,20), IGO	ABCD2114
19	T5 = T5T	ABCD2115
	GO TO 18	ABCD2116
20	CALL ERROR	ABCD2117
21	H22 = H22SAV	ABCD2118
	CALL COLPTB	ABCD2119
	RETURN	ABCD2120
C		ABCD2121
C		ABCD2122
C		ABCD2123
9	FORMAT (19H0*****TFFIP OFF MAP,F10.4,2X,A4,A2,11H*****\$\$\$\$)	ABCD2124

10	.FORMAT (19H0***** CNIP OFF MAP,F10.4,2X,A4,A2,11H*****\$\$\$\$\$\$)	ABCD2125
11	FORMAT(20H01.P. TURBINE DESIGN,5X,7HCNIPCF=,E15.8,8H TFIPCF=,	ABCD2126
	1 E15.8,8H ETIPCF=,E15.8,8H DHIPCF=,E15.8)	ABCD2127
	END	ABCD2128

Subroutine COLPTB

	SUBROUTINE COLPTB	ABCD2129
	IMPLICIT REAL*8 (A-H,O-Z)	ABCD2130
	LOGICAL SI, FXFN2M, AFTFAN	ABCD2131
	COMMON /COMALL/ COM(1062)	ABCD2132
	COMMON /COMDAT/ COMD(5423)	ABCD2133
	DIMENSION WORD(2), ERR(9), TFFXL(15), CNXL(15,15), DHTCXL(15,15),	ABCD2134
	1 ETATXL(15,15), NPTTFL(15)	ABCD2135
	DIMENSION Q(9), AWORD(2), WLO(2), WHI(2)	ABCD2136
	EQUIVALENCE (WORD(1), COM(1)), (IDES, COM(3)), (NOMAP, COM(20)),	ABCD2137
	1 (TOLALL, COM(23)), (EPR(1), COM(24)), (H22, COM(34)), (H2,	ABCD2138
	2 COM(94)), (T5, COM(102)), (H5, COM(103)), (S5, COM(104)), (WG5,	ABCD2139
	3 COM(105)), (FAR5, COM(106)), (HPEXT, COM(129)), (PCNF, COM(137)),	ABCD2140
	4 (H3, COM(153)), (H21, COM(264)), (P55, COM(272)),	ABCD2141
	5 (H55, COM(273)), (S55, COM(274)), (TFLPDS, COM(275)),	ABCD2142
	6 (CNLPDS, COM(276)), (ETLPDS, COM(277)), (TFLPCF, COM(281)),	ABCD2143
	7 (CNLPCF, COM(282)), (ETLPCF, COM(283)), (DHLPCF, COM(284)),	ABCD2144
	8 (TFFLP, COM(289)), (CNLP, COM(290)), (ETATLP, COM(291)),	ABCD2145
	9 (DHTCLP, COM(292)), (DHTF, COM(293)), (BLLP, COM(315)),	ABCD2146
	1 (WG55, COM(323)), (FAR55, COM(324)), (XNLP, COM(374)),	ABCD2147
	2 (P5, COM(385)), (P55, COM(387)), (U55, COM(388)),	ABCD2148
	3 (VLPTRB, COM(401)), (WAFP, COM(420)), (WAIP, COM(421)),	ABCD2149
	4 (XNLPDS, COM(425)), (PMILP, COM(428)), (ISPOOL, COM(1044)),	ABCD2150
	5 (SI, COM(1055)), (FXFN2M, COM(1058)), (AFTFAN, COM(1060))	ABCD2151
	EQUIVALENCE (TFFXL(1), COMD(4506)), (CNXL(1,1), COMD(4621)),	ABCD2152
	1 (DHTCXL(1,1), COMD(4846)), (ETATXL(1,1), COMD(5071)),	ABCD2153
	2 (NTFFSL, COMD(5408)), (NPTTFL(1), COMD(5409))	ABCD2154
	DATA AWORD, WLO, WHI /4HCOLP, 4HTB , 4H (LO, 4H) , 4H (HI,	ABCD2155
	1 4H) /	ABCD2156
	WORD(1) = AWORD(1)	ABCD2157
	WORD(2) = AWORD(2)	ABCD2158
	IF (SI) GO TO 100	ABCD2159
	RA = .0252D0	ABCD2160
	AJ = 2.719D0	ABCD2161
	CONFAC = 1.4091D-5	ABCD2162
	GO TO 101	ABCD2163
100	RA = 286.9D0	ABCD2164
	AJ = 1.0D0	ABCD2165
	CONFAC = 1.0966D-2	ABCD2166
101	THDE = DSQRT(T5) / PCNF	ABCD2167
	IF (IDES .EQ. 0) GO TO 1	ABCD2168
	CNLPCF = CNLPDS * THDE	ABCD2169
1	CNLP = CNLPCF / THDE	ABCD2170
	CNLPS = CNLP	ABCD2171
	TFFLPS = TFFLP	ABCD2172
	CALL SEARCH (-1.0D0, TFFLP, CNLP, DHTCLP, ETATLP, TFFXL(1), NTFFSL,	ABCD2173
	1 CNXL(1,1), DHTCXL(1,1), ETATXL(1,1), NPTTFL(1), 15, 15, IGO)	ABCD2174
	IF (IGO .EQ. 1 .OR. IGO .EQ. 11 .OR. IGO .EQ. 21)	ABCD2175

1	WRITE (8,8) TFFLPS,WLO	ABCD2176
	IF (IGO .EQ. 2 .OR. IGO .EQ. 12 .OR. IGO .EQ. 22)	ABCD2177
1	WRITE (8,8) TFFLPS,WHI	ABCD2178
	IF (IGO .EQ. 10 .OR. IGO .EQ. 11 .OR. IGO .EQ. 12)	ABCD2179
1	WRITE (8,9) CNLPS,WLO	ABCD2180
	IF (IGO .EQ. 20 .OR. IGO .EQ. 21 .OR. IGO .EQ. 22)	ABCD2181
1	WRITE (8,9) CNLPS,WHI	ABCD2182
	IF (IGO .NE. 7) GO TO 2	ABCD2183
	CALL ERROR	ABCD2184
	RETURN	ABCD2185
2	NOMAP = 0	ABCD2186
	TFLCAL = WG5 * DSQRT(T5) / (14.696D0 * P5)	ABCD2187
	IF (SI) TFLCAL = WG5 * DSQRT(T5) / P5	ABCD2188
	XNLP = XNLPDS * PCNF / 100.0D0	ABCD2189
	XNLDOT = DERIV(3,XNLP)	ABCD2190
	DHACEL = CONFAC * PMILP * XNLP * XNLDOT	ABCD2191
	DHTCF = (WAPP * (H22 - H2) + DHACEL) / (WG5 * T5)	ABCD2192
	DEXT = DHTCF	ABCD2193
	IF (FXFN2M .AND. .NOT. AFTFAN) DHTCF = DEXT + WAIP * (H21 - H22)	ABCD2194
	1 / (WG5 * T5)	ABCD2195
	IF (FXFN2M .AND. AFTFAN) DHTCF = DEXT + WAIP * (H21 - H2) /	ABCD2196
	1 (WG5 * T5)	ABCD2197
	IF (ISPOOL .GE. 2) GO TO 11	ABCD2198
	BTUEXT = 0.706705D0 * HPEXT	ABCD2199
	IF (SI) BTUEXT = HPEXT	ABCD2200
	DHTCF = DEXT + BTUEXT / (WG5 * T5)	ABCD2201
11	IF (IDES .EQ. 0) GO TO 5	ABCD2202
	TFLPCF = TFLPDS / TFLCAL	ABCD2203
	DHLPCF = DHTCF / DHTCLP	ABCD2204
	ETLPCF = ETLPDS / ETATLP	ABCD2205
	WRITE (6,10) CNLPCF,TFLPCF,ETLPCF,DHLPCF	ABCD2206
5	TFLCAL = TFLPCF * TFLCAL	ABCD2207
	DHTCLP = DHLPCF * DHTCLP	ABCD2208
	ETATLP = ETLPCF * ETATLP	ABCD2209
	DHTF = DHTCF * T5	ABCD2210
	I1 = 3	ABCD2211
	I2 = 4	ABCD2212
	IF (ISPOOL .NE. 1) GO TO 102	ABCD2213
	I1 = 1	ABCD2214
	I2 = 2	ABCD2215
102	ERR(I1) = (TFLCAL - TFFLP) / TFLCAL	ABCD2216
	ERR(I2) = (DHTCF - DHTCLP) / DHTCF	ABCD2217
	CALL THTURB (DHTF,ETATLP,FAR5,H5,S5,P5,F55,H55,S55,P55)	ABCD2218
	IF (BLLP .LE. 0.0D0) GO TO 6	ABCD2219
	FAR55 = FAR5 * WG5 / (WG5 + BLLP * (1.0D0 + FAR5))	ABCD2220
	WG55 = WG5 + BLLP	ABCD2221
	H55 = (BLLP * H3 + WG5 * H55) / WG55	ABCD2222
	CALL THERMO (P55,H55,T55,S55,XX2,1,FAR55,1)	ABCD2223
	GO TO 7	ABCD2224
6	FAR55 = FAR5	ABCD2225
	WG55 = WG5	ABCD2226
7	IF (VLPTRB .EQ. 0.0D0) GO TO 21	ABCD2227
	Q(2) = 0.0D0	ABCD2228
	Q(3) = 0.0D0	ABCD2229

	WG55P = WG55	ABCD2230
	H55P = H55	ABCD2231
	P55DOT = DERIV(16,P55)	ABCD2232
13	CALL THERMO (P55,H55,T55,S55,XX2,1,FAR55,0)	ABCD2233
	WG55 = WG55P - P55DOT * VLPTRB / T55 / 1.4D0 / RA	ABCD2234
	U55 = H55 - RA * AJ * T55	ABCD2235
	U55DOT = DERIV(17,U55)	ABCD2236
	H55X = (WG55P * H55P - (WG55P - WG55) * U55 - U55DOT * P55 *	ABCD2237
	1 VLPTRB / T55 / RA) / WG55	ABCD2238
	ERRW = (H55 - H55X) / H55	ABCD2239
	DIR = DSQRT(DABS(H55 / H55X))	ABCD2240
	CALL AFQUIR (Q(1),T55,ERRW,0.0D0,20.0D0,.1DC*TOLALL,DIR,T55T,IGO)	ABCD2241
	GO TO (19,21,20), IGO	ABCD2242
19	T55 = T55T	ABCD2243
	GO TO 18	ABCD2244
20	CALL ERROR	ABCD2245
21	CALL FRTOSD	ABCD2246
	RETURN	ABCD2247
C		ABCD2248
C		ABCD2249
8	FORMAT (19H0*****TFFLP OFF MAP,F10.4,2X,A4,A2,11H*****\$\$\$\$)	ABCD2250
9	FORMAT (19H0*****CNLP OFF MAP,F10.4,2X,A4,A2,11H*****\$\$\$\$)	ABCD2251
10	FORMAT(20H0L.P. TURBINE DESIGN,5X,7HCNLP CF=,E15.8,8H TFLPCF=,	ABCD2252
	1 E15.8,8H ETLPCF=,E15.8,8H DHLPCF=,E15.8)	ABCD2253
	END	ABCD2254

Subroutine COMIX

	SUBROUTINE COMIX	ABCD2255
	IMPLICIT REAL*8 (A-H,O-Z)	ABCD2256
	LOGICAL SI	ABCD2257
	COMMON /COMALL/ COM(1062)	ABCD2258
	DIMENSION WORD(2), ERR(9), DUMD1(15)	ABCD2259
	DIMENSION QQ(9), AWORD(2)	ABCD2260
	EQUIVALENCE (WORD(1), COM(1)), (IDES, COM(3)), (MODE, COM(6)),	ABCD2261
1	(IGASM, COM(10)), (NOMAP, COM(20)), (TOLALL, COM(23)), (EPF(1),	ABCD2262
2	COM(24)), (AM25, COM(45)), (T25, COM(46)), (P25, COM(47)), (H25,	ABCD2263
3	COM(48)), (S25, COM(49)), (A25, COM(98)), (V25, COM(99)), (AMF5,	ABCD2264
4	COM(107)), (V55, COM(108)), (A55, COM(109)), (PS55, COM(110)),	ABCD2265
5	(S6, COM(111)), (PS6, COM(112)), (V6, COM(113)),	ABCD2266
6	(PRFDS, COM(125)), (ZF, COM(136)), (PCNP, COM(137)),	ABCD2267
7	(T55, COM(272)), (H55, COM(273)), (S55, COM(274)),	ABCD2268
8	(PRCDS, COM(297)), (WG24, COM(321)), (FAR24, COM(322)),	ABCD2269
9	(WG55, COM(323)), (FAR55, COM(324)), (AM6, COM(327)),	ABCD2270
1	(A6, COM(328)), (WG6, COM(330)), (T6, COM(331)), (P6, COM(332)),	ABCD2271
2	(H6, COM(333)), (P55, COM(367)), (DUMD1(1), COM(405)),	ABCD2272
3	(PRFNEW, COM(991)), (PRCNEW, COM(992)), (ICOMIX, COM(1047)),	ABCD2273
4	(KKGO, COM(1048)), (SI, COM(1055))	ABCD2274
	DATA AWORD /4H COM, 4HIX /	ABCD2275
	WORD(1) = AWORD(1)	ABCD2276
	WORD(2) = AWORD(2)	ABCD2277
	IF (SI) GO TO 100	ABCD2278
	AJ = 778.25D0	ABCD2279
	CAPSF = 2116.2170D0	ABCD2280

	G = 32.174049D0	ABCD2281
	RDEM = 1.986375D0	ABCD2282
	GO TO 101	ABCD2283
100	AJ = 1.0D0	ABCD2284
	CAPSF = 1.0D0	ABCD2285
	G = 1.0D0	ABCD2286
	RDEM = 8316.41D0	ABCD2287
101	GAJ2 = 2.0 * G * AJ	ABCD2288
	ICOMIX = 0	ABCD2289
	CALL PROCOM (FAR55,T55,XX1,XX2,XX3,XX4,PHI55,XX5)	ABCD2290
	CALL PROCOM (FAR24,T25,XX1,XX2,XX3,XX4,PHI25,XX5)	ABCD2291
	IF (IDES .EQ. 0) GO TO 12	ABCD2292
C ***	CALCULATE A55 AND A25 WITH PS25=PS55	ABCD2293
	IF (PS55 .EQ. 0.0D0) GO TO 3	ABCD2294
	POP = PS55 / P55	ABCD2295
	ALPOPI = DLOG(1.0D0 / POP)	ABCD2296
	TS55 = T55 * POP ** .286D0	ABCD2297
	DO 1 I = 1,50	ABCD2298
	CALL PROCOM (FAR55,TS55,CS55,AK55,CP55,REX55,PHI55,HS55)	ABCD2299
	PHIS = PHI55 - REX55 * ALPOPI	ABCD2300
	DELPHI = PHIS - PHIS55	ABCD2301
	IF (DABS(DELPHI) .LE. .1D0 * TOLALL * PHIS) GO TO 6	ABCD2302
1	TS55 = TS55 * DEXP(4.0D0 * DELPHI)	ABCD2303
	ICOMIX = 1	ABCD2304
2	CALL ERROR	ABCD2305
	RETURN	ABCD2306
3	TS55 = 0.875D0 * T55	ABCD2307
	DO 4 I = 1,50	ABCD2308
	CALL PROCOM (FAR55,TS55,CS55,AK55,CP55,REX55,PHI55,HS55)	ABCD2309
	V55 = AM55 * CS55	ABCD2310
	HSCAL = H55 - V55 ** 2 / GAJ2	ABCD2311
	DELHS = HSCAL - HS55	ABCD2312
	IF (DABS(DELHS) .LE. .5D0 * TOLALL * HSCAL) GO TO 5	ABCD2313
4	TS55 = TS55 + DELHS / CP55	ABCD2314
	ICOMIX = 2	ABCD2315
	GO TO 2	ABCD2316
5	PS55 = P55 / DEXP((PHI55 - PHIS55) / REX55)	ABCD2317
	IF (PS55 .GT. P25 .AND. IDES .EQ. 1 .AND. IGASMX .GT. 0) GO TO 45	ABCD2318
6	IF (H55 .GT. HS55) GO TO 7	ABCD2319
	WRITE (8,46) P55,PS55,T55,TS55,H55,HS55	ABCD2320
	ICOMIX = 3	ABCD2321
	CALL ERROR	ABCD2322
7	V55 = DSQRT(GAJ2 * (H55 - HS55))	ABCD2323
	RHO = CAPSF * PS55 / (AJ * REX55 * TS55)	ABCD2324
	A55 = WG55 / (RHO * V55)	ABCD2325
	AM55 = V55 / CS55	ABCD2326
	IF (IGASMX .GT. 0) GO TO 8	ABCD2327
	WRITE (6,47) A55,AM55	ABCD2328
	IF (IGASMX) 35,41,8	ABCD2329
8	PS25 = PS55	ABCD2330
	POP = PS25 / P25	ABCD2331
	ALPOPI = DLOG(1.0D0 / POP)	ABCD2332
	TS25 = T25 * POP ** .286D0	ABCD2333
	DO 9 I = 1,50	ABCD2334



	CALL PFOCOM (FAR24,TS25,CS25,AK25,CP25,REX25,PHIS25,HS25)	ABCD2335
	PHIS = PHI25 - REX25 * ALPOPI	ABCD2336
	DELPHI = PHIS - PHIS25	ABCD2337
	IF (DABS(DELPHI) .LE. .1D0 * TOLALL * PHIS) GO TO 10	ABCD2338
9	TS25 = TS25 * DEXP(4.0D0 * DELPHI)	ABCD2339
	ICOMIX = 4	ABCD2340
	GO TO 2	ABCD2341
10	IF (H25 .GT. HS25) GO TO 11	ABCD2342
	WRITE (8,48) P25,PS25,T25,TS25,H25,HS25	ABCD2343
	ICOMIX = 5	ABCD2344
	CALL ERROR	ABCD2345
11	V25 = DSQRT(GAJ2 * (H25 - HS25))	ABCD2346
	RHO = CAPSF * PS25 / (AJ * REX25 * TS25)	ABCD2347
	A25 = WG24 / (RHO * V25)	ABCD2348
	AM25 = V25 / CS25	ABCD2349
	WRITE (6,49) A55,AM55,A25,AM25	ABCD2350
	GO TO 27	ABCD2351
C ***	CALCULATE PS55 AND PS25	ABCD2352
12	WQA = WG55 / A55	ABCD2353
	C1 = P55 * DSQRT(G / (T55 * AJ)) * CAPSF	ABCD2354
	MCON = 0	ABCD2355
	QQ(2) = 0.0D0	ABCD2356
	QQ(3) = 0.0D0	ABCD2357
	AM55 = 0.50D0	ABCD2358
	TS55 = 0.875D0 * T55	ABCD2359
13	DO 14 I = 1,50	ABCD2360
	CALL PROCOM (FAR55,TS55,CS55,AK55,CP55,REX55,PHIS55,HS55)	ABCD2361
	V55 = AM55 * CS55	ABCD2362
	HSCAL = H55 - V55 ** 2 / GAJ2	ABCD2363
	DELHS = HSCAL - HS55	ABCD2364
	IF (DABS(DELHS) .LE. .5D0 * TOLALL * HSCAL) GO TO 15	ABCD2365
14	TS55 = TS55 + DELHS / CP55	ABCD2366
	ICOMIX = 6	ABCD2367
	GO TO 2	ABCD2368
15	WQAT = C1 * DSQRT(AK55 / REX55) * AM55 / (1.0D0 + (AK55 - 1.0D0) * AM55 ** 2 / 2.0D0) ** ((AK55 + 1.0D0) / (2.0D0 * (AK55 - 1.0D0)))	ABCD2369
	AMX = AM55	ABCD2370
	IGOGO = 0	ABCD2371
16	DIR = WQA / WQAT	ABCD2372
	EW = (WQA - WQAT) / WQA	ABCD2373
	CALL AFQUIR (QQ(1),AMX,EW,0.0D0,30.0D0,.5D0*TOLALL,DIR,AMXT,ICON)	ABCD2374
	ICOMIX = 7	ABCD2375
	GO TO (17,22,2), ICON	ABCD2376
17	IF (AMXT .LE. 1.0D0) GO TO 20	ABCD2377
	AMXT = 0.7D0	ABCD2378
	MCON = MCON + 1	ABCD2379
	IF (MCON .LE. 1) GO TO 20	ABCD2380
	IF (MODE .EQ. 3) GO TO 19	ABCD2381
	PCNF = DUMD1(1)	ABCD2382
	WRITE (8,50) PCNF,AMX,P55,PS55,P25,PS25	ABCD2383
	PCNF = 1.01D0 * PCNF	ABCD2384
	DUMD1(1) = PCNF	ABCD2385
18	NOMAP = 7	ABCD2386
	ICOMIX = 0	ABCD2387
		ABCD2388

	RETURN	ABCD2389
19	WRITE (8,51) ZF,AMX,P55,PS55,P25,PS25	ABCD2390
	ZF = 0.99D0 * ZF	ABCD2391
	GO TO 18	ABCD2392
20	IF (IGOGO .EQ. 1) GO TO 21	ABCD2393
	AM55 = AMXT	ABCD2394
	GO TO 13	ABCD2395
21	AM25 = AMXT	ABCD2396
	GO TO 23	ABCD2397
22	IF (IGOGO .EQ. 1) GO TO 26	ABCD2398
	PS55 = P55 / DEXP((PHI55 - PHIS55) / REX55)	ABCD2399
	IF (IGASMX) 35,41,103	ABCD2400
103	WQA = WG24 / A25	ABCD2401
	C1 = P25 * DSQRT(G / (T25 * AJ)) * CAPSP	ABCD2402
	MCON = 0	ABCD2403
	QQ(2) = 0.0D0	ABCD2404
	QQ(3) = 0.0D0	ABCD2405
	AM25 = 0.25D0	ABCD2406
	TS25 = 0.875D0 * T25	ABCD2407
23	DO 24 I = 1,50	ABCD2408
	CALL PROCOM (FAR24,TS25,CS25,AK25,CP25,REX25,PHIS25,HS25)	ABCD2409
	V25 = AM25 * CS25	ABCD2410
	HSCAL = H25 - V25 ** 2 / GAJ2	ABCD2411
	DELHS = HSCAL - HS25	ABCD2412
	IF (DABS(DELHS) .LE. .5D0 * TOLALL * HSCAL) GO TO 25	ABCD2413
24	TS25 = TS25 + DELHS / CP25	ABCD2414
	ICOMIX = 8	ABCD2415
	GO TO 2	ABCD2416
25	WQAT = C1 * DSQRT(AK25 / REX25) * AM25 / (1.0D0 + (AK25 - 1.0D0) * AM25 ** 2 / 2.0D0) ** ((AK25 + 1.0D0) / (2.0D0 * (AK25 - 1.0D0)))	ABCD2417
	AMX = AM25	ABCD2418
	IGOGO = 1	ABCD2419
	GO TO 16	ABCD2420
26	PS25 = P25 / DEXP((PHI25 - PHIS25) / REX25)	ABCD2421
27	WG6 = WG24 + WG55	ABCD2422
	ERR(5) = (PS25 - PS55) / PS25	ABCD2423
	WF55 = FAR55 * WG55 / (FAR55 + 1.0D0)	ABCD2424
	WA55 = WG55 / (FAR55 + 1.0D0)	ABCD2425
	WF24 = FAR24 * WG24 / (FAR24 + 1.0D0)	ABCD2426
	WA24 = WG24 / (FAR24 + 1.0D0)	ABCD2427
	FAR6 = (WF55 + WF24) / (WA55 + WA24)	ABCD2428
	H6 = (WG24 * H25 + WG55 * H55) / WG6	ABCD2429
	CALL THERMO (1.0D0,H6,T6,PHI6,AMX,1,FAR6,1)	ABCD2430
	C1 = PS55 * A55 * (1.0D0 + AK55 * AM55 ** 2) + PS25 * A25 * (1.0D0 + AK25 * AM25 ** 2)	ABCD2431
	TS6 = 0.833D0 * T6	ABCD2432
	DO 32 I = 1,50	ABCD2433
	CALL PROCOM (FAR6,TS6,CS6,AK6,CP6,REX6,PHIS6,HS6)	ABCD2434
	C2 = WG6 * DSQRT(AJ * REX6 * T6 / (AK6 * G))	ABCD2435
	C3 = C2 / (CAPSP * C1)	ABCD2436
	C4 = (AK6 - 1.0D0) / 2.0D0 - (C3 * AK6) ** 2	ABCD2437
	C5 = 1.0D0 - 2.0D0 * AK6 * C3 ** 2	ABCD2438
	C6 = C5 ** 2 + 4.0D0 * C4 * C3 ** 2	ABCD2439
	ICOMIX = 9	ABCD2440
		ABCD2441
		ABCD2442

	IF (C6) 28,29,30	ABCD2443
28	CALL ERROR	ABCD2444
	RETURN	ABCD2445
29	AM62G = - C5 / (2.0D0 * C4)	ABCD2446
	GO TO 31	ABCD2447
30	AM62G = (DSQRT(C6) - C5) / (2.0D0 * C4)	ABCD2448
31	IF (AM62G .LE. 0.0D0) GO TO 28	ABCD2449
	AM6G = DSQRT(AM62G)	ABCD2450
	V6 = AM6G * CS6	ABCD2451
	HSCAL = H6 - V6 ** 2 / GAJ2	ABCD2452
	DELHS = HSCAL - HS6	ABCD2453
	IF (DABS(DELHS) .LE. .5D0 * TOLALL * HSCAL) GO TO 33	ABCD2454
32	TS6 = TS6 + DELHS / CP6	ABCD2455
	ICOMIX = 10	ABCD2456
	CALL ERROR	ABCD2457
33	A6G = A25 + A55	ABCD2458
	C7 = DSQRT(1.0D0 + (AK6 - 1.0D0) * AM62G / 2.0D0)	ABCD2459
	PS6 = C2 / (CAPSF * A6G * AM6G * C7)	ABCD2460
	P6 = PS6 * DEXP((PHI6 - PHIS6) / REX6)	ABCD2461
	CALL THERMO (P6,H6,T6,S6,XX1,1,FAR6,0)	ABCD2462
	S6AVE = (WG24 * S25 + WG55 * S55) / WG6	ABCD2463
	IF (S6 .GE. S6AVE) GO TO 35	ABCD2464
	S6 = S6AVE	ABCD2465
	P6 = DEXP(AMX * (PHI6 - S6) / RDEM)	ABCD2466
35	IF (IGASMX .LE. 0) GO TO 36	ABCD2467
	GO TO (43,37), IGASMX	ABCD2468
36	T6 = T55	ABCD2469
	P6 = P55	ABCD2470
	H6 = H55	ABCD2471
	S6 = S55	ABCD2472
	WG6 = WG55	ABCD2473
	PS6 = PS55	ABCD2474
	FAR6 = FAR55	ABCD2475
	AK6 = AK55	ABCD2476
37	IF (IDES .EQ. 0) GO TO 38	ABCD2477
C***	CALCULATES A6 AS A FUNCTION OF INPUT AM6	ABCD2478
	TS6 = T6 / (1.0D0 + (((AK6 - 1.0D0) / 2.0D0) * AM6 ** 2))	ABCD2479
	DO 34 JJ = 1,50	ABCD2480
	AK6P = AK6	ABCD2481
	CALL PROCOM (FAR6,TS6,CS6,AK6,CP6,REX6,PHIS6,HS6)	ABCD2482
	V6 = AM6 * CS6	ABCD2483
	DELA6 = AK6P - AK6	ABCD2484
	IF (DABS(DELA6) .LE. .5D0 * TOLALL * AK6) GO TO 54	ABCD2485
34	TS6 = T6 / (1.0D0 + (((AK6 - 1.0D0) / 2.0D0) * AM6 ** 2))	ABCD2486
	ICOMIX = 11	ABCD2487
	CALL ERROR	ABCD2488
54	PS6 = P6 / ((1.0D0 + (((AK6 - 1.0D0) / 2.0D0) * AM6 ** 2)) **	ABCD2489
	1 (AK6 / (AK6 - 1.0D0)))	ABCD2490
	AM6ABD = AM6	ABCD2491
	RHO = CAPSF * PS6 / (AJ * REX6 * TS6)	ABCD2492
	A6 = WG6 / (RHO * V6)	ABCD2493
	WRITE (6,52) A6	ABCD2494
	GO TO 44	ABCD2495
C	CALCULATES M6=F(A6DESIGN)	ABCD2496

38	TS6P = T6 / (1.0D0 + (((AK6 - 1.0D0) / 2.0D0) * AM6ABD ** 2))	ABCD2497
	DO 39 I = 1,50	ABCD2498
	CALL PROCOM (FAR6,TS6P,CS6,AK6,CP6,REX6,PHIS6,HS6)	ABCD2499
	PS6P = PS6 * (TS6P / TS6) ** (AK6 / (AK6 - 1.0D0))	ABCD2500
	RHO6 = CAPSF * PS6P / (AJ * REX6 * TS6P)	ABCD2501
	V6 = DSQRT(GAJ2 * (H6 - HS6))	ABCD2502
	IF ((H6 - HS6) .LT. 0.0D0) GO TO 42	ABCD2503
	A6P = WG6 / (RHO6 * V6)	ABCD2504
	DELA6 = A6P - A6	ABCD2505
	V6 = WG6 / (RHO6 * A6)	ABCD2506
	AM6 = V6 / CS6	ABCD2507
	AM62 = AM6 ** 2	ABCD2508
	IF (DABS(DELA6) .LE. .002D0 * A6) GO TO 40	ABCD2509
39	TS6P = T6 / (1.0D0 + (((AK5 - 1.0D0) / 2.0D0) * AM62))	ABCD2510
	ICOMIX = 12	ABCD2511
	CALL ERROR	ABCD2512
40	TS6 = TS6P	ABCD2513
	PS6 = PS6P	ABCD2514
	GO TO 44	ABCD2515
41	T6 = T55	ABCD2516
	P6 = P55	ABCD2517
	H6 = H55	ABCD2518
	S6 = S55	ABCD2519
	WG6 = WG55	ABCD2520
	PS6 = PS55	ABCD2521
	V6 = V55	ABCD2522
	AM6 = AM55	ABCD2523
	IF (IGASMX .EQ. 0) A6 = A55	ABCD2524
	GO TO 44	ABCD2525
42	WRITE (6,53) H6,HS6	ABCD2526
	ICOMIX = 13	ABCD2527
	CALL ERROR	ABCD2528
43	AM62 = AM62G	ABCD2529
	AM6 = AM6G	ABCD2530
	A6 = A25 + A55	ABCD2531
	ICOMIX = 0	ABCD2532
44	CALL COAFBN	ABCD2533
	RETURN	ABCD2534
45	KKGO = 1	ABCD2535
	OPRDS = PRFDS * PRCDS	ABCD2536
	PRFNEW = PRFDS * PS55 / P25 * 1.02D0	ABCD2537
	PRCNEW = OPRDS / PRFNEW	ABCD2538
	ICOMIX = 0	ABCD2539
	CALL ENGBAL	ABCD2540
	RETURN	ABCD2541
C		ABCD2542
C		ABCD2543
46	FORMAT (22H0SQRT OF H55-HS55 NEG ,6E15.6,6H\$\$\$\$\$)	ABCD2544
47	FORMAT (20H0TURBINE AREA DESIGN, 6X, 6H A55=, E15.8, 8H AM55=,	ABCD2545
	1 E15.8)	ABCD2546
48	FORMAT (22H0SQRT OF H25-HS25 NEG ,6E15.6,6H\$\$\$\$\$)	ABCD2547
49	FORMAT (25H0TURBINE/DUCT AREA DESIGN,7H A55=,E15.8,8H AM55=,	ABCD2548
	1 E15.8,8H A25=,E15.8,8H AM25=,E15.8)	ABCD2549
50	FORMAT (12H0COMIX PCNF=,F7.4,4H AM=,F8.6,5H P55=,F9.5,6H PS55=,	ABCD2550

	IMSHOC = ICON + 3	ABCD2602
4	ERR(6) = (P7R - P7) / P7R	ABCD2603
	IF (ISPOOL .EQ. 1) ERR(3) = ERR(6)	ABCD2604
	IF (IMNOZ .EQ. 1) WRITE (6,5) A8,AM8,A9,AM9	ABCD2605
	RETURN	ABCD2606
C		ABCD2607
C		ABCD2608
5	FORMAT (14H0NOZZLE DESIGN,10X,3H A8=,E15.8,8H AM8=,E15.8,	ABCD2609
	1 8H A9=,E15.8,8H AM9=,E15.8)	ABCD2610
	END	ABCD2611

Subroutine CONDIV

	SUBROUTINE CONDIV (TI,HI,PI,SI,FAR,WG,PA,IDES,AT,AO,PIR,TT,HT,PT,	ABCD2612
	1 ST,TO,HO,PO,SO,TST,TSO,PSI,PSO,VI,VO,AMT,AMO,ICON)	ABCD2613
C	ICON=1 SUBSONIC, COMPARE PIR WITH PI	ABCD2614
C	ICON=2 SONIC, SHOCK INSIDE NOZZLE, COMPARE PIR WITH PI	ABCD2615
C	ICON=3 SONIC, SHOCK OUTSIDE NOZZLE, COMPARE PIR WITH PI	ABCD2616
C	ICON=4 ERROR	ABCD2617
	IMPLICIT REAL*8 (A-H,O-Z)	ABCD2618
	LOGICAL ZI	ABCD2619
	COMMON /COMALL/ COM(1062)	ABCD2620
	DIMENSION Q(9)	ABCD2621
	EQUIVALENCE (TOLALL, COM(23)), (ZI, COM(1055))	ABCD2622
	Q(2) = 0.0D0	ABCD2623
	Q(3) = 0.0D0	ABCD2624
	IF (ZI) GO TO 100	ABCD2625
	AJ = 778.26D0	ABCD2626
	CAPSF = 2116.2170D0	ABCD2627
	G = 32.174049D0	ABCD2628
	GO TO 101	ABCD2629
100	AJ = 1.0D0	ABCD2630
	CAPSF = 101325.0D0	ABCD2631
	G = 1.0D0	ABCD2632
101	GAJ2 = 2.0 * G * AJ	ABCD2633
	CALL PROCOM (FAR,TI,XX1,XX2,XX3,XX4,PHII,XX6)	ABCD2634
C ***	SONIC CALCULATIONS	ABCD2635
	TSS = 0.833D0 * TI	ABCD2636
	DO 2 J = 1,50	ABCD2637
	CALL PROCOM (FAR,TSS,CSS,AK,CP,REXS,PHISS,HSS)	ABCD2638
	HSCAL = HI - CSS ** 2 / GAJ2	ABCD2639
	DELHS = HSCAL - HSS	ABCD2640
	IF (DABS(DELHS) .LE. .5D0 * TOLALL * HSCAL) GO TO 4	ABCD2641
2	TSS = TSS + DELHS / CP	ABCD2642
3	ICON = 4	ABCD2643
	RETURN	ABCD2644
4	IF (IDES .LE. 0) GO TO 11	ABCD2645
C ***	SONIC DESIGN, CALCULATE AT	ABCD2646
	VT = CSS	ABCD2647
	TST = TSS	ABCD2648
	PST = PI * (TST / TI) ** (AK / (AK - 1.0D0))	ABCD2649
	RHO = CAPSF * PST / (AJ * REXS * TST)	ABCD2650
	AT = WG / (RHO * VT)	ABCD2651
	AMT = 1.0D0	ABCD2652

C ***	IDEAL EXPANSION DESIGN, CALCULATE AO	ABCD2653
	PSO = PA	ABCD2654
	TSO = TI * (PSO / PI) ** .286D0	ABCD2655
	DO 7 J = 1,50	ABCD2656
	CALL PROCOM (FAR,TSO,CSO,AK,CP,REX,PHISO,HSO)	ABCD2657
	PHICAL = PHII - REX * DLOG(PI / PSO)	ABCD2658
	DELPHI = PHICAL - PHISO	ABCD2659
	IF (DABS(DELPHI) .LE. .1D0 * TOLALL * PHICAL) GO TO 8	ABCD2660
7	TSO = TSO * DEXP(4.0D0 * DELPHI)	ABCD2661
	GO TO 3	ABCD2662
8	VO = DSQRT(GAJ2 * (HI - HSO))	ABCD2663
	AMO = VO / CSO	ABCD2664
	AKP1 = AK + 1.0D0	ABCD2665
	AKM1 = AK - 1.0D0	ABCD2666
	AO = (AT / AMO) * (2.0D0 * (1.0D0 + AKM1 * AMO ** 2 / 2.0D0) /	ABCD2667
	1 AKP1) ** (AKP1 / (2.0D0 * AKM1))	ABCD2668
	PIR = PI	ABCD2669
	ICON = 3	ABCD2670
9	TO = TI	ABCD2671
	HO = HI	ABCD2672
	PO = PI	ABCD2673
	SO = SI	ABCD2674
10	TT = TI	ABCD2675
	HT = HI	ABCD2676
	PT = PI	ABCD2677
	ST = SI	ABCD2678
	RETURN	ABCD2679
C ***	ASSUME SONIC THROAT AND ISENTROPIC EXPANSION TO AO	ABCD2680
11	VT = CSS	ABCD2681
	AMT = 1.0D0	ABCD2682
	TST = TSS	ABCD2683
	RHO = WG / (AT * VT)	ABCD2684
	PST = RHO * AJ * REXS * TST / CAPSF	ABCD2685
	PIR = PST * (TI / TST) ** (AK / (AK - 1.0D0))	ABCD2686
	IF (PST .GE. PA) GO TO 27	ABCD2687
	TSO = 0.95D0 * TI	ABCD2688
	MAM = 0	ABCD2689
13	CALL PROCOM (FAR,TSO,CSO,AK,CP,REX,PHISO,HSO)	ABCD2690
	AKP1 = AK + 1.0D0	ABCD2691
	AKM1 = AK - 1.0D0	ABCD2692
	AMO = DSQRT(2.0D0 * ((TI / TSO) - 1.0D0) / AKM1)	ABCD2693
	AOCAL = (AT / AMO) * (2.0D0 * (1.0D0 + AKM1 * AMO ** 2 / 2.0D0) /	ABCD2694
	1 AKP1) ** (AKP1 / (2.0D0 * AKM1))	ABCD2695
	EA = (AO - AOCAL) / AO	ABCD2696
	DIR = DSQRT(AO / AOCAL)	ABCD2697
	CALL AFQUIR (Q(1),TSO,EA,0.0D0,100.0D0,.1D0*TOLALL,DIR,TSOT,JCON)	ABCD2698
	GO TO (14,18,3), JCON	ABCD2699
14	TSO = TSOT	ABCD2700
	IF (TSO - TI) 15,13,16	ABCD2701
15	TSC = 2.0D0 * TI / (AK + 1.0D0)	ABCD2702
	IF (TSO .GT. TSC) GO TO 17	ABCD2703
16	TSO = 0.98D0 * TI	ABCD2704
	GO TO 13	ABCD2705
17	IF (Q(2) .LT. 30.0D0 .OR. AMO .LT. 0.95D0 .OR. MAM .EQ. 1)	ABCD2706

1	GO TO 13	ABCD2707
	TSO = 2.0D0 * TI / (2.0D0 + 0.98D0 * (AK - 1.0D0))	ABCD2708
	MAM = 1	ABCD2709
	GO TO 13	ABCD2710
18	PSO = PIR * (TSO / TI) ** (AK / (AK - 1.0D0))	ABCD2711
	IF (PSO - PA) 20,19,27	ABCD2712
C ***	CRITICAL FLOW, ISENTROPIC EXPANSION TO PA	ABCD2713
19	VO = AMO * CSO	ABCD2714
	ICON = 1	ABCD2715
	GO TO 9	ABCD2716
C ***	SUBSONIC FLOW	ABCD2717
20	PSO = PA	ABCD2718
	Q(2) = 0.0D0	ABCD2719
	Q(3) = 0.0D0	ABCD2720
	TSO = 0.833D0 * TI	ABCD2721
	DO 22 J = 1,50	ABCD2722
	CALL PROCOM (FAR,TSO,CSO,AK,CP,REX,PHISO,HSO)	ABCD2723
	RHO = CAPSF * PSO / (AJ * REX * TSO)	ABCD2724
	VO = WG / (RHO * AO)	ABCD2725
	HSCAL = HI - VO ** 2 / GAJ2	ABCD2726
	DELHS = HSCAL - HSO	ABCD2727
	IF (DABS(DELHS) .LE. .5D0 * TOLALL * HSCAL) GO TO 23	ABCD2728
22	TSO = TSO + DELHS / CP	ABCD2729
	GO TO 3	ABCD2730
23	AMO = VO / CSO	ABCD2731
	PIR = PSO * (TI / TSO) ** (AK / (AK - 1.0D0))	ABCD2732
	TST = TSO	ABCD2733
24	CALL PROCOM (FAR,TST,CST,AK,CP,REX,PHIST,HST)	ABCD2734
	PST = PIR * (TST / TI) ** (AK / (AK - 1.0D0))	ABCD2735
	RHO = PST * CAPSF / (AJ * REX * TST)	ABCD2736
	VT = WG / (RHO * AT)	ABCD2737
	HSCAL = HI - VT ** 2 / GAJ2	ABCD2738
	EH = (HSCAL - HST) / HSCAL	ABCD2739
	DIR = 1.0D0 + (HSCAL - HST) / (CP * TST)	ABCD2740
	CALL AFQUIR (Q(1),TST,EH,0.0D0,20.0D0,.5D0*TOLALL,DIR,TSTT,JCON)	ABCD2741
	GO TO (25,26,3), JCON	ABCD2742
25	TST = TSTT	ABCD2743
	GO TO 24	ABCD2744
26	AMT = VT / CST	ABCD2745
	ICON = 1	ABCD2746
	GO TO 9	ABCD2747
C ***	SUPERCRITICAL FLOW, ISENTROPIC EXPANSION TO PA	ABCD2748
27	PSO = PA	ABCD2749
	TSO = TI * (PSO / PIR) ** .286D0	ABCD2750
	DO 29 J = 1,50	ABCD2751
	CALL PROCOM (FAR,TSO,CSO,AK,CP,REX,PHISO,HSO)	ABCD2752
	PHICAL = PHII - REX * DLOG(PIR / PSO)	ABCD2753
	DELPHI = PHICAL - PHISO	ABCD2754
	IF (DABS(DELPHI) .LE. .1D0 * TOLALL * PHICAL) GO TO 30	ABCD2755
29	TSO = TSO * DEXP(4.0D0 * DELPHI)	ABCD2756
	GO TO 3	ABCD2757
30	VO = DSQRT(GAJ2 * (HI - HSO))	ABCD2758
	AMO = VO / CSO	ABCD2759
	AKP1 = AK + 1.0D0	ABCD2760

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      AKM1 = AK - 1.0D0
      AOID = (AT / AMO) * (2.0D0 * (1.0D0 + AKM1 * AMO ** 2 / 2.0D0) /
1 AKP1) ** (AKP1 / (2.0D0 * AKM1))
      ICON = 3
      N = 0
      IF (AO - AOID) 31,9,32
C *** SUPERCRITICAL FLOW, ISENTROPIC EXPANSION TO AO
31      N = 1
32      TSO = 0.833D0 * TI
      DO 34 J = 1,100
      CALL PROCOM (FAR,TSO,CSO,AK,CP,REX,PHISO,HSO)
      AKP1 = AK + 1.0D0
      AKM1 = AK - 1.0D0
      AMO = DSQRT(2.0D0 * ((TI / TSO) - 1.0D0) / AKM1)
      AOAL = (AT / AMO) * (2.0D0 * (1.0D0 + AKM1 * AMO ** 2 / 2.0D0) /
1 AKP1) ** (AKP1 / (2.0D0 * AKM1))
      DELA = AO - AOAL
      IF (DABS(DELA) .LE. .1D0 * TOLALL * AO) GO TO 35
34      TSO = TSO * DSQRT(AOAL / AO)
      GO TO 3
35      IF (N .LE. 0) GO TO 37
C *** UNDEREXPANDED, SHOCK OUTSIDE NOZZLE
      PSO = PIR * (TSO / TI) ** (AK / (AK - 1.0D0))
      VO = AMO * CSO
      GO TO 9
C *** OVEREXPANDED, FIND SHOCK POSITION
37      PSX = PIR * (TSO / TI) ** (AK / (AK - 1.0D0))
      PSY = PSX * (2.0D0 * AK * AMO ** 2 / (AK + 1.0D0) - (AK - 1.0D0) /
1 (AK + 1.0D0))
      IF (PA .GE. PSY) GO TO 39
C *** OVEREXPANDED, SHOCK OUTSIDE NOZZLE
      PSO = PSX
      VO = AMO * CSO
      GO TO 9
C *** OVEREXPANDED, SHOCK INSIDE NOZZLE
39      PSO = PA
      TSO = 0.833D0 * TI
      DO 41 J = 1,50
      CALL PROCOM (FAR,TSO,CSO,AK,CP,REX,PHISO,HSO)
      RHO = CAPSF * PSO / (AJ * REX * TSO)
      VO = WG / (RHO * AO)
      HSCAL = HI - VO ** 2 / GAJ2
      DELHS = HSCAL - HSO
      IF (DABS(DELHS) .LE. .5D0 * TOLALL * HSCAL) GO TO 42
41      TSO = TSO + DELHS / CP
      GO TO 3
42      AMO = VO / CSO
      TO = TI
      HO = HI
      PO = PSO * (TO / TSO) ** (AK / (AK - 1.0D0))
      SO = PHII - REX * DLOG(PO)
      ICON = 2
      GO TO 10
      END

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 ABCD2810
 ABCD2811
 ABCD2812
 ABCD2813
 ABCD2814

Subroutine CONOUT

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SUBROUTINE CONOUT (ICON)
IMPLICIT REAL*8 (A-H,O-Z)
LOGICAL SI
COMMON /COMALL/ COM(1062)
DIMENSION WORDY(368,2), IOUT(150), AOUT(6), WOUT(6,2),
1 WOR11(152), WOR21(152), WOR31(64), WOR12(152), WOR22(152),
2 WOR32(64), THEEND(2), BLANK(2), AIN(2), CHANGE(2)
EQUIVALENCE (TIME,COM(993)), (ITRAN,COM(1049)), (SI,COM(1055))
EQUIVALENCE (WOR11(1),WORDY(1,1)), (WOR21(1),WORDY(153,1)),
1 (WOR31(1),WORDY(305,1)), (WOR12(1),WORDY(1,2)),
2 (WOR22(1),WORDY(153,2)), (WOR32(1),WORDY(305,2))
DATA WOR11 /
1 4HP1 , 4HH22 , 4HAM23, 4HWA23, 4HT23 , 4HP23 , 4HH23 , 4HS23 ,
2 4HA24 , 4HT24 , 4HH24 , 4HS24 , 4HAM25, 4HT25 , 4HP25 , 4HH25 ,
3 4HS25 , 4HA28 , 4HA28S, 4HAM28, 4HV28 , 4HTS28, 4HPS28, 4HT28 ,
4 4HP28 , 4HH28 , 4HS28 , 4HA29 , 4HA29S, 4HAM29, 4HV29 , 4HTS29,
5 4HPS29, 4HT29 , 4HP29 , 4HH29 , 4HS29 , 4HBYP, 4HWAD , 4HWF,
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5 4HXP1304, 4HXP1305, 4HXP1306, 4HXP1307, 4HXP1308, 4HXP1309,
6 4HXP1310, 4HXP1311, 4HXP1312, 4HXP1313, 4HXP1314, 4HXP1315,
7 4HXP1316, 4HXP1317, 4HXP1318, 4HXP1319, 4HXP1320, 4HXP1321,
8 4HXP1322, 4HXP1323, 4HXP1324, 4HXP1325, 4HXP1326, 4HXP1327,
9 4HXP1328, 4HXP1329, 4HXP1330, 4HXP1331, 4HXP1332, 4HXP1333,
1 4HXP1334, 4HXP1335, 4HXP1336, 4HXP1337, 4HXP1338, 4HXP1339,
2 4HXP1340, 4HXP1341, 4HXP1342, 4HXP1343, 4HXP1344, 4HXP1345,
3 4HXP1346, 4HXP1347, 4HXP1348, 4HXP1349, 4HXP1350, 4HXP1351,
4 4HXP1352, 4HXP1353, 4HXP1354, 4HXP1355, 4HXP1356, 4HXP1357,
5 4HXP1358, 4HXP1359, 4HXP1360, 4HXP1361, 4HXP1362, 4HXP1363,
6 4HXP1364, 4HXP1365, 4HXP1366, 4HXP1367, 4HXP1368, 4HXP1369,
7 4HXP1370, 4HXP1371, 4HXP1372, 4HXP1373, 4HXP1374, 4HXP1375,
8 4HXP1376, 4HXP1377, 4HXP1378, 4HXP1379
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DATA WOR31 /
1 4HTS7 , 4HPS7 , 4HV7 , 4HAM7 , 4HA7 , 4HT7DS, 4HT7 , 4HH7 , ABCD2866
2 4HS7 , 4HA8 , 4HA8SA, 4HTS8 , 4HPS8 , 4HV8 , 4HAM8 , 4HT8 , ABCD2867
3 4HP8 , 4HH8 , 4HS8 , 4HA9 , 4HA9SA, 4HTS9 , 4HPS9 , 4HV9 , ABCD2869
4 4HAM9 , 4HT9 , 4HP9 , 4HH9 , 4HS9 , 4HETAA, 4HDPAF, 4HWFA , ABCD2870
5 4HETAA, 4HETAA, 4HDPAF, 4HXNHP, 4HXNIP, 4HXNLP, 4HP22 , 4HU22 , ABCD2871
6 4HP21 , 4HU21 , 4HP3 , 4HU3 , 4HP4 , 4HU4 , 4HP50 , 4HU50 , ABCD2872
7 4HP5 , 4HU5 , 4HP55 , 4HU55 , 4HP7 , 4HU7 , 4HP24 , 4HU24 , ABCD2873
8 4HP37 , 4HU37 , 4HDUMS, 4HFXFN, 4HFXM2, 4HAFTF, 4HFAN , 4HISPO / ABCD2874
DATA WOR12 /
1 3 * 4H , 4HDS , 14 * 4H , 4HAV , 9 * 4H , 4HAV , ABCD2875
2 8 * 4H , 4HSS , 3 * 4H , 4HC , 4HDS , 4H , 4H4 , ABCD2876
3 4H24 , 4 * 4H , 4H5 , 4H55 , 12 * 4H , 4HS , ABCD2878
4 16 * 4H , 4 * 4HCF , 3 * 4HDS , 4HF , 4HCF , 4HF , ABCD2879
5 4HDS , 4HS , 4HDS , 4HS , 4HGU , 4HT , 4H1 , ABCD2880
6 7 * 4H , 4HF , 2 * 4H , 4HP , 4H , 2 * 4HIP , ABCD2881
7 2 * 4H , 4HDS , 4HGU , 6 * 4H , 4HDS , 9 * 4H , ABCD2882
8 4H0 , 4HHP , 4HIP , 4HLP , 4HDP , 4HOB , 4H , ABCD2883
9 2 * 4HHP , 4H , 4HP , 4HF , 4HCF , 4HF , 4HCF , ABCD2884
1 4HS , 4HDS , 4HS , 2 * 4HDS / ABCD2885
DATA WOR22 /
1 4HS , 11 * 4H , 4HDS , 4HM , 4HGU , 9 * 4H , 4HU , ABCD2887
2 17 * 4H , 4HDS , 4HNG , 4HNT , 3 * 4HNG , 4HIN , 4HFN , ABCD2889
3 4HDS , 4HG , 4HN , 4HPC , 4HNG , 2 * 4HOZ , 17 * 4H , ABCD2890
4 3 * 4HFN , 4HFD , 4 * 4H , 4HS , 7 * 4H , 6 * 4HDS , ABCD2891
5 8 * 4HCF , 4HP , 4H , 2 * 4HLP , 4H , 4HF , 4HCF , ABCD2892
6 4HP , 4HS , 4HDS , 4HS , 2 * 4H , 4HC , 4HDS , ABCD2893
7 4HI , 4HID , 16 * 4H , 4H4 , 4H , 4H5 , 4HAV , ABCD2894
8 4HSV , 2 * 4H , 4HDS , 6 * 4H , 4HSV / ABCD2895
DATA WOR32 /
1 10 * 4H , 4HV , 9 * 4H , 4HV , 8 * 4H , 2 * 4HDS , ABCD2896
2 2 * 4H , 4HSV , 4HT , 23 * 4H , 4HPL , 4H2M , 4HCP , ABCD2897
3 4HAN , 4H , 4HOL / ABCD2898
DATA THEEND, BLANK, LIMIT / 4HTHEE, 4HND , 4H , 4H , 368 / ABCD2899
IF (ICON .EQ. 1) GO TO 24 ABCD2900
IF (SI) GO TO 22 ABCD2901
WRITE (6,21) ABCD2902
GO TO 24 ABCD2903
22 WRITE (6,23) ABCD2904
24 GO TO (1,6) , ICON ABCD2905
C *** INPUT SECTION ABCD2906
1 DO 4 N = 1,150 ABCD2907
NUM = N ABCD2908
READ (5,11) AIN,CHANGE ABCD2909
IF (AIN(1) .EQ. THEEND(1) .AND. AIN(2) .EQ. THEEND(2)) GO TO 5 ABCD2910
DO 2 J = 1,LIMIT ABCD2911
JJ = J ABCD2912
IF (AIN(1) .EQ. WORDY(J,1) .AND. AIN(2) .EQ. WORDY(J,2)) GO TO 3 ABCD2913
2 CONTINUE ABCD2914
WRITE (6,12) AIN ABCD2915
GO TO 4 ABCD2916
3 IOUT(NUM) = JJ ABCD2917
IF (CHANGE(1) .EQ. BLANK(1) .AND. CHANGE(2) .EQ. BLANK(2)) ABCD2918
1 GO TO 4 ABCD2919

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	WORDY(JJ,1) = CHANGE(1)	ABCD2920
	WORDY(JJ,2) = CHANGE(2)	ABCD2921
4	CONTINUE	ABCD2922
	WRITE (6,13)	ABCD2923
5	NUM = NUM - 1	ABCD2924
	RETURN	ABCD2925
C ***	OUTPUT SECTION	ABCD2926
6	IF (NUM .EQ. 1) RETURN	ABCD2927
C		ABCD2928
C	THE FOLLOWING THREE STATEMENTS ARE USED AT LEWIS ONLY	ABCD2929
	IF (TIME .EQ. 0.0D0 .AND. ITRAN .NE. 1) GO TO 16	ABCD2930
	WRITE (50,19) TIME, COM(248), COM(257), COM(258)	ABCD2931
	WRITE (50,20) (COM(I), I = 372,394)	ABCD2932
C		ABCD2933
16	N = NUM	ABCD2934
	J = 6	ABCD2935
	DO 9 I = 1,NUM,6	ABCD2936
	IF (N .GT. 6) GO TO 7	ABCD2937
	J = N	ABCD2938
7	N = N - 6	ABCD2939
	DO 8 K = 1,J	ABCD2940
	L = I + K - 1	ABCD2941
	M = IOUT(L)	ABCD2942
	WOUT(K,1) = WORDY(M,1)	ABCD2943
	WOUT(K,2) = WORDY(M,2)	ABCD2944
	IF (M .LE. 362) AOUT(K) = COM(M+32)	ABCD2945
	IF (M .GT. 362 .AND. M .LE. 367) AOUT(K) = COM(M+694)	ABCD2946
	IF (M .GT. 367) AOUT(K) = COM(1044)	ABCD2947
8	CONTINUE	ABCD2948
	WRITE (6,14) (WOUT(K,1), WOUT(K,2), K = 1,J)	ABCD2949
	WRITE (6,15) (AOUT(K),K=1,J)	ABCD2950
	IF (N .LE. 0) RETURN	ABCD2951
9	CONTINUE	ABCD2952
	RETURN	ABCD2953
C		ABCD2954
C		ABCD2955
C		ABCD2956
11	FORMAT (A4, A2, 6X, A4, A2)	ABCD2957
12	FORMAT (1H0, 9HTHE WORD , A4, A2, 26H NOT FOUND IN COMMON ARRAY)	ABCD2958
13	FORMAT (22H0ERROR IN CONOUT INPUT)	ABCD2959
14	FORMAT (1H0, 25X, A4, A2, 5(9X, A4, A2))	ABCD2960
15	FORMAT (21X, 6E15.6)	ABCD2961
C		ABCD2962
C	THE FOLLOWING TWO FORMATS ARE USED AT LEWIS ONLY	ABCD2963
19	FORMAT (1X, 1PE20.6)	ABCD2964
20	FORMAT (1X, 1PE20.6)	ABCD2965
C		ABCD2966
21	FORMAT (1X, 30HTHE OUTPUT IS IN ENGLISH UNITS)	ABCD2967
23	FORMAT (1X, 25HTHE OUTPUT IS IN SI UNITS)	ABCD2968
	END	ABCD2969

Subroutine CONVRG

SUBROUTINE CONVRG (TI,HI,PI,SI,FAR,WG,PA,IDES,AO,PR,TO,HO,PO,SO, ABCD2970

1	TSO,PSO,VO,AMO,ICON)	ABCD2971
C	ICON=1 SUBSONIC, COMPARE PI WITH PR	ABCD2972
C	ICON=2 SONIC, COMPARE PI WITH PR	ABCD2973
C	ICON=4 ERROR	ABCD2974
	IMPLICIT REAL*8 (A-H,O-Z)	ABCD2975
	LOGICAL ZI	ABCD2976
	COMMON /COMALL/ COM(1062)	ABCD2977
	EQUIVALENCE (TOLALL, COM(23)), (ZI, COM(1055))	ABCD2978
	IF (ZI) GO TO 100	ABCD2979
	AJ = 778.26D0	ABCD2980
	CAPSF = 2116.217D0	ABCD2981
	G = 32.174049D0	ABCD2982
	CPG = .250D0	ABCD2983
	GO TO 101	ABCD2984
100	AJ = 1.0D0	ABCD2985
	CAPSF = 1.0D0	ABCD2986
	G = 1.0D0	ABCD2987
	CPG = 1048.D0	ABCD2988
101	GAJ2 = 2.0D0 * G * AJ	ABCD2989
	CALL PROCOM (FAR,TI,XX1,XX2,XX3,XX4,PHII,XX6)	ABCD2990
C ***	SONIC CALCULATIONS	ABCD2991
	TSS = 0.833D0 * TI	ABCD2992
	DO 2 J = 1,50	ABCD2993
	CALL PROCOM (FAR,TSS,CSS,AKS,CP,REXS,PHISS,HSS)	ABCD2994
	HSCAL = HI - CSS ** 2 / GAJ2	ABCD2995
	DELHS = HSCAL - HSS	ABCD2996
	IF (DABS(DELHS) .LE. .5D0 * TOLALL * HSCAL) GO TO 4	ABCD2997
2	TSS = TSS + DELHS / CP	ABCD2998
3	ICON = 4	ABCD2999
	RETURN	ABCD3000
4	IF (IDES .LE. 0) GO TO 12	ABCD3001
C ***	ISENTROPIC EXPANSION CALCULATIONS	ABCD3002
	TSI = TI * (PA / PI) ** 0.286D0	ABCD3003
	DO 7 J = 1,70	ABCD3004
	CALL THERMO (PA,HSI,TSI,SSI,XX1,1,FAR,0)	ABCD3005
	IF (DABS(SSI - SI) .LE. .1D0 * TOLALL * SI) GO TO 8	ABCD3006
7	TSI = TSI / DEXP((SSI - SI) / CPG)	ABCD3007
	GO TO 3	ABCD3008
8	VIS = DSQRT(GAJ2 * (HI - HSI))	ABCD3009
	IF (VIS .GE. CSS) GO TO 11	ABCD3010
C ***	SUBSONIC DESIGN, CALCULATE AO	ABCD3011
	VO = VIS	ABCD3012
	TSO = TSI	ABCD3013
	PSO = PA	ABCD3014
	CALL PROCOM (FAR,TSO,CSO,XX2,XX3,REX,PHISO,HSO)	ABCD3015
	RHO = CAPSF * PSO / (AJ * PEX * TSO)	ABCD3016
	AO = WG / (RHO * VO)	ABCD3017
	AMO = VO / CSO	ABCD3018
	PR = PI	ABCD3019
	ICON = 1	ABCD3020
10	TO = TI	ABCD3021
	HO = HI	ABCD3022
	PO = PI	ABCD3023
	SO = SI	ABCD3024

	RETURN	ABCD3025
C ***	SONIC DESIGN, CALCULATE AO	ABCD3026
11	VO = CSS	ABCD3027
	TSO = TSS	ABCD3028
	PSO = PI * (TSO / TI) ** (AKS / (AKS - 1.0D0))	ABCD3029
	RHO = CAPSF * PSO / (AJ * REXS * TSO)	ABCD3030
	AO = WG / (RHO * VO)	ABCD3031
	AMO = 1.0D0	ABCD3032
	PR = PI	ABCD3033
	ICON = 2	ABCD3034
	GO TO 10	ABCD3035
C ***	NON-DESIGN, CALCULATE CRITICAL CONDITIONS	ABCD3036
12	VO = CSS	ABCD3037
	TSO = TSS	ABCD3038
	PSO = PA	ABCD3039
	RHO = CAPSF * PSO / (AJ * REXS * TSO)	ABCD3040
	AOCRIT = WG / (RHO * VO)	ABCD3041
	AMO = 1.0D0	ABCD3042
	PR = PSO * (TI / TSO) ** (AKS / (AKS - 1.0D0))	ABCD3043
	IF (AO .GT. AOCRIT) GO TO 14	ABCD3044
C ***	NON-DESIGN, CRITICAL AND SUPERCRITICAL CONDITIONS	ABCD3045
	PSO = PSO * AOCRIT / AO	ABCD3046
	PR = PR * AOCRIT / AO	ABCD3047
	ICON = 2	ABCD3048
	GO TO 10	ABCD3049
C ***	NON-DESIGN, SUBSONIC CALCULATIONS	ABCD3050
14	PSO = PA	ABCD3051
	TSO = 0.833D0 * TSO	ABCD3052
	DO 16 J = 1,50	ABCD3053
	CALL PROCOM (FAR,TSO,CSO,AKO,CP,REX,PHISO,HSO)	ABCD3054
	RHO = CAPSF * PSO / (AJ * REX * TSO)	ABCD3055
	VO = WG / (RHO * AO)	ABCD3056
	HSCAL = HI - VO ** 2 / GAJ2	ABCD3057
	DELHS = HSCAL - HSO	ABCD3058
	IF (DABS(DELHS) .LE. .5D0 * TOLALL * HSCAL) GO TO 17	ABCD3059
16	TSO = TSO + DELHS / CP	ABCD3060
	GO TO 3	ABCD3061
17	AMO = VO / CSO	ABCD3062
	PR = PSO * (TI / TSO) ** (AKO / (AKO - 1.0D0))	ABCD3063
	ICON = 1	ABCD3064
	GO TO 10	ABCD3065
	END	ABCD3066

Function DERIV

FUNCTION DERIV (I,X)	ABCD3067
IMPLICIT REAL*8 (A-H,O-Z)	ABCD3068
COMMON /COMALL/ COM(1062)	ABCD3069
DIMENSION FO(50,4), PVRDOT(23), XS(23)	ABCD3070
EQUIVALENCE (FO(1,1), COM(430)), (DT, COM(994)),	ABCD3071
1 (PVRDOT(1), COM(998)), (XS(1), COM(1021)), (JTRAN, COM(1050)),	ABCD3072
2 (IVRDOT, COM(1052)), (IAMTRX, COM(1054))	ABCD3073
IF (IAMTRX .EQ. 1) GO TO 2	ABCD3074
IF (JTRAN .EQ. 1) GO TO 1	ABCD3075

	DERIV = 0.0D0	ABCD3076
	FO(I,1) = X	ABCD3077
	FO(I,2) = X	ABCD3078
	FO(I,3) = DERIV	ABCD3079
	FO(I,4) = DERIV	ABCD3080
	RETURN	ABCD3081
1	X0 = FO(I,2)	ABCD3082
	DERIV = (X - X0) / DT	ABCD3083
	IF (DABS(DERIV) .LT. 1.0D-10) DERIV = 0.0D0	ABCD3084
	FO(I,1) = X	ABCD3085
	FO(I,3) = DERIV	ABCD3086
	RETURN	ABCD3087
2	IF (I .EQ. IVRDOT) GO TO 3	ABCD3088
	DERIV = 0.0D0	ABCD3089
	RETURN	ABCD3090
3	DERIV = XS(I) * PVRDOT(I)	ABCD3091
	RETURN	ABCD3092
	END	ABCD3093

Subroutine DISTRB

	SUBROUTINE DISTRB	ABCD3094
	IMPLICIT REAL*8 (A-H,O-Z)	ABCD3095
	COMMON /COMALL/ COM(1062)	ABCD3096
	DOUBLE PRECISION LWV, MWV	ABCD3097
	DIMENSION XVAR(23), PVRDOT(23), XS(23)	ABCD3098
	DIMENSION XSAVE(1062), AINV(529), ARINV(529), A(23,23),	ABCD3099
	1 A21INV(23,23), A22INV(23,23), AR(23,23), CINT(23,23), X(23,23),	ABCD3100
	2 A12INV(23,23), DINT(23,23), BINT(50,23), CA(50,23), C(50,23),	ABCD3101
	3 CR(50,23), UVAR(50,23), AIBM(23,5), B(23,5), BR(23,5), Y(50,5),	ABCD3102
	4 D(50,5), DR(50,5), XSS(23), YI(23), USS(50), DU(5), BS(5),	ABCD3103
	5 PVRDOS(23)	ABCD3104
	DIMENSION LWV(23), MWV(23), IVARB(23), NUCOM(50)	ABCD3105
	EQUIVALENCE (IDES, COM(3)), (JDES, COM(4)), (MODE, COM(6)),	ABCD3106
	1 (INIT, COM(7)), (PS55, COM(110)), (WAFCD, COM(135)),	ABCD3107
	2 (WFB, COM(192)), (A8, COM(346)), (XVAR(1), COM(372)),	ABCD3108
	3 (PVRDOT(1), COM(998)), (XS(1), COM(1021)), (ITRAN, COM(1049)),	ABCD3109
	4 (JTRAN, COM(1050)), (IVRDOT, COM(1052)), (IDOT, COM(1053)),	ABCD3110
	5 (IAMTRX, COM(1054)), (WAFCD, COM(1062))	ABCD3111
C		ABCD3112
C	INV	ABCD3113
C	THE TOTAL NUMBER OF STATES POSSIBLE FOR THE PARTICULAR	ABCD3114
C	ENGINE BEING MODELLED, LESS THAN OR EQUAL TO 23	ABCD3115
		ABCD3116
	DATA INV / 16 /	ABCD3117
C		ABCD3118
C	INVRED	ABCD3119
C	THE TOTAL NUMBER OF STATES ACTUALLY USED IN THE MODEL	ABCD3120
C	(FULL OR REDUCED), LESS THAN OR EQUAL TO INV	ABCD3121
		ABCD3122
	DATA INVRED / 9 /	ABCD3123
C		ABCD3124
C	IVARB	ABCD3125
C	THE ORDER IN WHICH THE STATES ARE TO BE DONE. IF THIS	ABCD3126
C	IS A REDUCED MODEL, THE STATES TO BE INCLUDED ARE	
C	LISTED BEFORE THOSE NOT INCLUDED.	

C	PVRDOT(2) = 0.0D0	ABCD3181
C		ABCD3182
C	FAN ROTOR SPEED	ABCD3183
C		ABCD3184
C	PVRDOT(3) = .02D0	ABCD3185
C		ABCD3186
C	FAN EXIT PRESSURE	ABCD3187
C		ABCD3188
C		ABCD3189
C	PVRDOT(4) = .02D0	ABCD3190
C		ABCD3191
C	FAN EXIT INTERNAL ENERGY	ABCD3192
C		ABCD3193
C	PVRDOT(5) = .02D0	ABCD3194
C		ABCD3195
C	INTERMEDIATE COMPRESSOR EXIT PRESSURE	ABCD3196
C		ABCD3197
C	PVRDOT(6) = 0.0D0	ABCD3198
C		ABCD3199
C	INTERMEDIATE COMPRESSOR EXIT INTERNAL ENERGY	ABCD3200
C		ABCD3201
C	PVRDOT(7) = 0.0D0	ABCD3202
C		ABCD3203
C	COMPRESSOR EXIT PRESSURE	ABCD3204
C		ABCD3205
C	PVRDOT(8) = .02D0	ABCD3206
C		ABCD3207
C	COMPRESSOR EXIT INTERNAL ENERGY	ABCD3208
C		ABCD3209
C	PVRDOT(9) = .02D0	ABCD3210
C		ABCD3211
C	COMBUSTOR EXIT PRESSURE	ABCD3212
C		ABCD3213
C	PVRDOT(10) = .02D0	ABCD3214
C		ABCD3215
C	COMBUSTOR EXIT INTERNAL ENERGY	ABCD3216
C		ABCD3217
C	PVRDOT(11) = .02D0	ABCD3218
C		ABCD3219
C	HIGH PRESSURE TURBINE EXIT PRESSURE	ABCD3220
C		ABCD3221
C	PVRDOT(12) = .02D0	ABCD3222
C		ABCD3223
C	HIGH PRESSURE TURBINE EXIT INTERNAL ENERGY	ABCD3224
C		ABCD3225
C	PVRDOT(13) = .02D0	ABCD3226
C		ABCD3227
C	INTERMEDIATE PRESSURE TURBINE EXIT PRESSURE	ABCD3228
C		ABCD3229
C	PVRDOT(14) = 0.0D0	ABCD3230
C		ABCD3231
C	INTERMEDIATE PRESSURE TURBINE EXIT INTERNAL ENERGY	ABCD3232
C		ABCD3233
C	PVRDOT(15) = 0.0D0	ABCD3234

C		ABCD3235.
C	LOW PRESSURE TURBINE EXIT PRESSURE	ABCD3236
C		ABCD3237
	PVRDOT(16) = .02D0	ABCD3238
C		ABCD3239
C	LOW PRESSURE TURBINE EXIT INTERNAL ENERGY	ABCD3240
C		ABCD3241
	PVRDOT(17) = .02D0	ABCD3242
C		ABCD3243
C	AFTERBURNER EXIT PRESSURE	ABCD3244
C		ABCD3245
	PVRDOT(18) = .02D0	ABCD3246
C		ABCD3247
C	AFTERBURNER EXIT INTERNAL ENERGY	ABCD3248
C		ABCD3249
	PVRDOT(19) = .02D0	ABCD3250
C		ABCD3251
C	DUCT BURNER EXIT PRESSURE	ABCD3252
C		ABCD3253
	PVRDOT(20) = .02D0	ABCD3254
C		ABCD3255
C	DUCT BURNER EXIT INTERNAL ENERGY	ABCD3256
C		ABCD3257
	PVRDOT(21) = .02D0	ABCD3258
C		ABCD3259
C	THIRD STREAM EXIT PRESSURE	ABCD3260
C		ABCD3261
	PVRDOT(22) = 0.0D0	ABCD3262
C		ABCD3263
C	THIRD STREAM EXIT INTERNAL ENERGY	ABCD3264
C		ABCD3265
	PVRDOT(23) = 0.0D0	ABCD3266
7	CONTINUE	ABCD3267
	IDOT = IDOT + 1	ABCD3268
	IF (IDOT .GT. INV) GO TO 10	ABCD3269
	IVRDOT = IVARB(IDOT)	ABCD3270
	IF (IDOT .NE. 1) GO TO 10	ABCD3271
C		ABCD3272
C	SAVE STEADY STATE VALUES AND INITIALIZE	ABCD3273
C	FOR A AND C MATRIX CALCS	ABCD3274
C		ABCD3275
	DO 5 I = 1,INV	ABCD3276
	J = IVARB(I)	ABCD3277
	XS(J) = XVAR(J)	ABCD3278
	XSS(I) = XVAR(J)	ABCD3279
	IF (XSS(I) .EQ. 0.0D0) WRITE (6,50)	ABCD3280
5	CONTINUE	ABCD3281
	DO 96 I = 1,INC	ABCD3282
	IU = NUCOM(I)	ABCD3283
96	USS(I) = COM(IU)	ABCD3284
	DO 1 I = 1,1062	ABCD3285
1	XSAVE(I) = COM(I)	ABCD3286
	WRITE (6,65)	ABCD3287
	WRITE (6,44) (XSS(I), I = 1,INV)	ABCD3288

	RETURN	ABCD3289
10	IDOT1 = IDOT - 1	ABCD3290
C		ABCD3291
C	GENERATE MATRIX FOR A MATRIX CALCS	ABCD3292
C		ABCD3293
	DO 15 I = 1, INV	ABCD3294
	J = IVARB(I)	ABCD3295
15	X(I, IDOT1) = XVAR(J) - XSS(I)	ABCD3296
	J = IVARB(IDOT1)	ABCD3297
	IF (ICHOIC .EQ. 0) GO TO 23	ABCD3298
	ERRX = DABS(X(IDOT1, IDOT1) / XSS(IDOT1)) - .002D0	ABCD3299
	IF (DABS(ERRX) .LE. .00001D0) GO TO 17	ABCD3300
	IDOT = IDOT1	ABCD3301
	IVRDOT = IVARB(IDOT)	ABCD3302
	IGIN = IGIN + 1	ABCD3303
	IF (DABS(X(1, IDOT1)) .NE. 0.0D0) GO TO 18	ABCD3304
	PVRP = PVRDOT(J)	ABCD3305
	PVRDOT(J) = 2.0D0 * PVRDOT(J)	ABCD3306
	IF (ERRX .EQ. ERRXP .OR. IBCK .NE. 0) GO TO 9	ABCD3307
	PVRDOT(J) = 1.5D0 * PVRP + ABCK	ABCD3308
	ABCK = 2.0D0 * ABCK	ABCD3309
9	ERRXP = ERRX	ABCD3310
	IBCK = 1	ABCD3311
	GO TO 23	ABCD3312
18	IF (IGIN .NE. 1) GO TO 16	ABCD3313
	IBCK = 0	ABCD3314
	PVRP = PVRDOT(J)	ABCD3315
	ERRXP = ERRX	ABCD3315
	PVRDOT(J) = 1.05D0 * PVRDOT(J)	ABCD3317
	GO TO 23	ABCD3318
16	PVRNEW = (PVRDOT(J) * ERRXP - PVRP * ERRX) / (ERRXP - ERRX)	ABCD3319
	IBCK = 0	ABCD3320
	IF (PVRNEW .LE. 0.0D0) PVRNEW = .95D0 * PVRDOT(J)	ABCD3321
	IF (IGIN .EQ. 50) PVRNEW = ((PVRDOT(J) + PVRP) / 2.0D0) + .1D-3	ABCD3322
	IF (IGIN .EQ. 100) PVRNEW = ((PVRDOT(J) + PVRP) / 2.0D0) + .1D-2	ABCD3323
	PVRP = PVRDOT(J)	ABCD3324
	ERRXP = ERRX	ABCD3325
	PVRDOT(J) = PVRNEW	ABCD3325
	GO TO 23	ABCD3327
C		ABCD3328
C	GENERATE MATRIX FOR C MATRIX CALCS	ABCD3329
C		ABCD3330
17	IGIN = 0	ABCD3331
	IBCK = 0	ABCD3332
	ABCK = 1.0D-5	ABCD3333
	IF (PVRDOT(J) .LE. 0.0D0) PVRDOT(J) = ABCK	ABCD3334
23	DO 97 I = 1, INC	ABCD3335
	IU = NUCOM(I)	ABCD3336
97	UVAR(I, IDOT1) = COM(IU) - USS(I)	ABCD3337
	WRITE (6, 45) IDOT1, IVARB(IDOT1)	ABCD3338
	WRITE (6, 60)	ABCD3339
	WRITE (6, 44) (X(I, IDOT1), I = 1, INV)	ABCD3340
	WRITE (6, 282) IGIN	ABCD3341
	WRITE (6, 296) PVRDOT(J)	ABCD3342

	IAMTSV = IAMTRX	ABCD3343
	IVRSV = IVRDOT	ABCD3344
	IDOTSV = IDOT	ABCD3345
	DO 19 I = 1,23	ABCD3346
19	PVRDOS(I) = PVRDOT(I)	ABCD3347
C		ABCD3348
C	RESET STEADY STATE VALUES	ABCD3349
C		ABCD3350
	DO 21 I = 1,1062	ABCD3351
21	COM(I) = XSAVE(I)	ABCD3352
	IAMTRX = IAMTSV	ABCD3353
	IVRDOT = IVRSV	ABCD3354
	IDOT = IDOTSV	ABCD3355
	DO 22 I = 1,23	ABCD3356
22	PVRDOT(I) = PVRDOS(I)	ABCD3357
	IF (IGIN .NE. 0) RETURN	ABCD3358
	IF (IDOT .LE. INV) RETURN	ABCD3359
C		ABCD3360
C	FINAL CALCS FOR A AND C MATRICES	ABCD3361
C		ABCD3362
25	DO 24 I = 1,INV	ABCD3363
	J = IVARB(I)	ABCD3364
24	YI(I) = 1.000 / XSS(I) / PVRDOT(J)	ABCD3365
	WRITE (6,55)	ABCD3366
	WRITE (6,44) (YI(I), I = 1,INV)	ABCD3367
	WRITE (6,75)	ABCD3368
	DO 31 J = 1,INV	ABCD3369
	DO 30 I = 1,INV	ABCD3370
	K = INV * (J-1) + I	ABCD3371
30	AINV(K) = YI(J) * X(I,J)	ABCD3372
	LL = K - INV + 1	ABCD3373
	WRITE (6,44) (AINV(I), I = LL,K)	ABCD3374
31	CONTINUE	ABCD3375
	DO 46 J = 1,INVRED	ABCD3376
	DO 46 I = 1,INVRED	ABCD3377
	K = INVRED * (J - 1) + I	ABCD3378
46	ARINV(K) = YI(J) * X(I,J)	ABCD3379
	L = INVRED + 1	ABCD3380
	IF (L .GT. INV) GO TO 49	ABCD3381
C		ABCD3382
C	A12INV, A21INV, AND A22INV ARE NECESSARY FOR C AND D MATRIX	ABCD3383
C	CALCS IN REDUCED FORM	ABCD3384
C		ABCD3385
	DO 47 J = 1,INVRED	ABCD3386
	DO 47 I = L,INV	ABCD3387
	A12INV(J,I) = YI(I) * X(J,I)	ABCD3388
47	A21INV(I,J) = YI(J) * X(I,J)	ABCD3389
	DO 48 J = L,INV	ABCD3390
	DO 48 I = L,INV	ABCD3391
48	A22INV(I,J) = YI(J) * X(I,J)	ABCD3392
49	CONTINUE	ABCD3393
	DO 98 J = 1,INV	ABCD3394
	DO 98 I = 1,INC	ABCD3395
98	CA(I,J) = YI(J) * UVAR(I,J)	ABCD3396

	CALL DMINV (AINV, INV, DET, LWV, MWV)	ABCD3397
	IF (DET .EQ. 0.0D0) WRITE (6,70)	ABCD3398
	DO 32 J = 1,INV	ABCD3399
	DO 32 I = 1,INV	ABCD3400
	K = INV * (J-1) + I	ABCD3401
32	A(I,J) = AINV(K)	ABCD3402
	WRITE (6,80)	ABCD3403
C		ABCD3404
C	THE FOLLOWING STATEMENT IS USED AT LEWIS ONLY	ABCD3405
C	WRITE (10) A	ABCD3406
C		ABCD3407
	DO 100 K = 1,INV	ABCD3408
	DO 100 I = 1,INC	ABCD3409
	SUM = 0.0D0	ABCD3410
	DO 99 J = 1,INV	ABCD3411
99	SUM = SUM + CA(I,J) * A(J,K)	ABCD3412
100	C(I,K) = SUM	ABCD3413
C		ABCD3414
C	THE FOLLOWING STATEMENT IS USED AT LEWIS ONLY	ABCD3415
C	WRITE (20) C	ABCD3416
C		ABCD3417
	DO 33 J = 1,INV	ABCD3418
	WRITE (6,44) (A(J,I), I = 1,INV)	ABCD3419
33	CONTINUE	ABCD3420
	WRITE (6,81)	ABCD3421
	DO 101 J = 1,INC	ABCD3422
	WRITE (6,44) (C(J,I), I = 1,INV)	ABCD3423
101	CONTINUE	ABCD3424
C		ABCD3425
C	RESET STEADY STATE VALUES AND INITIALIZE	ABCD3426
C	FOR B AND D MATRIX CALCS	ABCD3427
C		ABCD3428
	IB = 977	ABCD3429
	JDOT = 0	ABCD3430
	DO 26 I = 1,1062	ABCD3431
26	COM(I) = XSAVE(I)	ABCD3432
	DO 76 I = 1,INC	ABCD3433
	IU = NUCOM(I)	ABCD3434
76	USS(I) = COM(IU)	ABCD3435
	DO 34 I = 1,INV	ABCD3436
34	PVRDOT(I) = 0.0D0	ABCD3437
	BS(1) = WFB	ABCD3438
	BS(2) = A8	ABCD3439
	BS(3) = X3	ABCD3440
	BS(4) = X4	ABCD3441
	BS(5) = X5	ABCD3442
	DO 27 I = 1,5	ABCD3443
27	DU(I) = BPER * BS(I)	ABCD3444
4	IF (JDOT .EQ. 1) GO TO 35	ABCD3445
	DO 2 I = 1,INV	ABCD3446
	J = IVARB(I)	ABCD3447
2	XSS(I) = XVAR(J)	ABCD3448
	DO 6 I = 1,1062	ABCD3449
6	XSAVE(I) = COM(I)	ABCD3450

	IAMTRX = 1	ABCD3451
	ITRAN = 0	ABCD3452
	IDOT = 0	ABCD3453
	IDES = 0	ABCD3454
	MODE = 2	ABCD3455
	JDOT = 1	ABCD3456
	WFB = WFB + DU(1)	ABCD3457
	RETURN	ABCD3458
35	IDOT = IDOT + 1	ABCD3459
C		ABCD3460
C	GENERATE MATRIX FOR B MATRIX CALCS	ABCD3461
C		ABCD3462
	DO 36 I = 1,INV	ABCD3463
	J = IVARB(I)	ABCD3464
36	AIBM(I,IDOT) = (XVAR(J) - XSS(I)) / DU(IDOT)	ABCD3465
C		ABCD3466
C	GENERATE MATRIX FOR D MATRIX CALCS	ABCD3467
C		ABCD3468
	DO 77 I = 1,INC	ABCD3469
	IU = NUCOM(I)	ABCD3470
77	Y(I,IDOT) = (COM(IU) - USS(I)) / DU(IDOT)	ABCD3471
C		ABCD3472
C	RESET STEADY STATE VALUES	ABCD3473
C		ABCD3474
	IAMTSV = IAMTRX	ABCD3475
	MODESV = MODE	ABCD3476
	IDESV = IDES	ABCD3477
	ITRASV = ITRAN	ABCD3478
	IDOTSV = IDOT	ABCD3479
	DO 29 I = 1,1062	ABCD3480
29	COM(I) = XSAVE(I)	ABCD3481
	IAMTRX = IAMTSV	ABCD3482
	MODE = MODESV	ABCD3483
	IDES = IDESV	ABCD3484
	ITRAN = ITRASV	ABCD3485
	IDOT = IDOTSV	ABCD3486
8	IF (IDOT .GE. INB) GO TO 28	ABCD3487
	GO TO (11,12,13,14), IDOT	ABCD3488
11	A8 = A8 + DU(2)	ABCD3489
	RETURN	ABCD3490
12	X3 = X3 + DU(3)	ABCD3491
	RETURN	ABCD3492
13	X4 = X4 + DU(4)	ABCD3493
	RETURN	ABCD3494
14	X5 = X5 + DU(5)	ABCD3495
	RETURN	ABCD3496
C		ABCD3497
C	FINAL CALCS FOR B MATRIX	ABCD3498
C		ABCD3499
28	DO 38 K = 1,INB	ABCD3500
	DO 38 I = 1,INV	ABCD3501
	SUM = 0.0D0	ABCD3502
	DO 37 J = 1,INV	ABCD3503
37	SUM = SUM - (A(I,J) * AIBM(J,K))	ABCD3504

38	B(I,K) = SUM	ABCD3505
C		ABCD3506
C	THE FOLLOWING STATEMENT IS USED AT LEWIS ONLY	ABCD3507
C	WRITE (15) B	ABCD3508
C		ABCD3509
C		ABCD3510
C	FINAL CALCS FOR D MATRIX	ABCD3511
C		ABCD3512
	DO 87 K = 1,INB	ABCD3513
	DO 87 I = 1,INC	ABCD3514
	SUM = 0.0D0	ABCD3515
	DO 86 J = 1,INV	ABCD3516
86	SUM = SUM + C(I,J) * AIBM(J,K)	ABCD3517
87	D(I,K) = Y(I,K) - SUM	ABCD3518
C		ABCD3519
C	THE FOLLOWING STATEMENT IS USED AT LEWIS ONLY	ABCD3520
C	WRITE (25) D	ABCD3521
C		ABCD3522
	WRITE (6,85)	ABCD3523
	GO TO (39,40,41,42,43), INB	ABCD3524
39	WRITE (6,91) ((B(I,J), J = 1,INB), I = 1,INV)	ABCD3525
	GO TO 110	ABCD3526
40	WRITE (6,92) ((B(I,J), J = 1,INB), I = 1,INV)	ABCD3527
	GO TO 110	ABCD3528
41	WRITE (6,93) ((B(I,J), J = 1,INB), I = 1,INV)	ABCD3529
	GO TO 110	ABCD3530
42	WRITE (6,94) ((B(I,J), J = 1,INB), I = 1,INV)	ABCD3531
	GO TO 110	ABCD3532
43	WRITE (6,95) ((B(I,J), J = 1,INB), I = 1,INV)	ABCD3533
110	WRITE (6,82)	ABCD3534
	GO TO (111,112,113,114,115), INB	ABCD3535
111	WRITE (6,91) ((D(I,J), J = 1,INB), I = 1,INC)	ABCD3536
	GO TO 200	ABCD3537
112	WRITE (6,92) ((D(I,J), J = 1,INB), I = 1,INC)	ABCD3538
	GO TO 200	ABCD3539
113	WRITE (6,93) ((D(I,J), J = 1,INB), I = 1,INC)	ABCD3540
	GO TO 200	ABCD3541
114	WRITE (6,94) ((D(I,J), J = 1,INB), I = 1,INC)	ABCD3542
	GO TO 200	ABCD3543
115	WRITE (6,95) ((D(I,J), J = 1,INB), I = 1,INC)	ABCD3544
200	IF (L .GT. INV) STOP	ABCD3545
C		ABCD3546
C	CALCULATIONS FOR ALL MATRICES OF REDUCED ORDER MODEL	ABCD3547
C		ABCD3548
C	FINAL CALCS FOR REDUCED A MATRIX	ABCD3549
C		ABCD3550
	CALL DMINV (ARINV, INVRED, DET, LWV, MWV)	ABCD3551
	DO 201 J = 1,INVRED	ABCD3552
	DO 201 I = 1,INVRED	ABCD3553
	K = INVRED * (J - 1) + I	ABCD3554
201	AR(I,J) = ARINV(K)	ABCD3555
C		ABCD3556
C	FINAL CALCS FOR REDUCED B MATRIX	ABCD3557
C		ABCD3558

	DO 203 K = 1,INB	ABCD3559
	DO 203 I = 1,INVRED	ABCD3560
	SUM = 0.0D0	ABCD3561
	DO 202 J = 1,INVRED	ABCD3562
202	SUM = SUM - AR(I,J) * AIBM(J,K)	ABCD3563
203	BR(I,K) = SUM	ABCD3564
C		ABCD3565
C	FINAL CALCS FOR REDUCED C MATRIX	ABCD3566
C		ABCD3567
	DO 205 K = 1,INVRED	ABCD3568
	DO 205 I = L,INV	ABCD3569
	SUM = 0.0D0	ABCD3570
	DO 204 J = 1,INVRED	ABCD3571
204	SUM = SUM + A21INV(I,J) * AR(J,K)	ABCD3572
205	CINT(I,K) = SUM	ABCD3573
	DO 207 K = 1,INVRED	ABCD3574
	DO 207 I = 1,INC	ABCD3575
	SUM = 0.0D0	ABCD3576
	DO 206 J = L,INV	ABCD3577
206	SUM = SUM + C(I,J) * CINT(J,K)	ABCD3578
207	CR(I,K) = C(I,K) + SUM	ABCD3579
C		ABCD3580
C	FINAL CALCS FOR REDUCED D MATRIX	ABCD3581
C		ABCD3582
	DO 209 K = L,INV	ABCD3583
	DO 209 I = 1,INVRED	ABCD3584
	SUM = 0.0D0	ABCD3585
	DO 208 J = 1,INVRED	ABCD3586
208	SUM = SUM + AR(I,J) * A12INV(J,K)	ABCD3587
209	CINT(I,K) = SUM	ABCD3588
	DO 211 K = L,INV	ABCD3589
	DO 211 I = L,INV	ABCD3590
	SUM = 0.0D0	ABCD3591
	DO 210 J = 1,INVRED	ABCD3592
210	SUM = SUM + A21INV(I,J) * CINT(J,K)	ABCD3593
211	DINT(I,K) = SUM - A22INV(I,K)	ABCD3594
	DO 213 K = L,INV	ABCD3595
	DO 213 I = 1,INC	ABCD3596
	SUM = 0.0D0	ABCD3597
	DO 212 J = L,INV	ABCD3598
212	SUM = SUM + C(I,J) * DINT(J,K)	ABCD3599
213	BINT(I,K) = SUM	ABCD3600
	DO 103 K = 1,INB	ABCD3601
	DO 103 I = 1,INC	ABCD3602
	SUM = 0.0D0	ABCD3603
	DO 102 J = L,INV	ABCD3604
102	SUM = SUM + BINT(I,J) * B(J,K)	ABCD3605
103	DR(I,K) = SUM + D(I,K)	ABCD3606
	WRITE (6,214)	ABCD3607
	DO 218 I = 1,INVRED	ABCD3608
	WRITE (6,44) (AR(I,J), J = 1,INVRED)	ABCD3609
218	CONTINUE	ABCD3610
	WRITE (6,215)	ABCD3611
	GO TO (219,220,221,222,223), INB	ABCD3612

219	WRITE (6,91) ((BR(I,J), J = 1,INB), I = 1,INVRED)	ABCD3613
	GO TO 224	ABCD3614
220	WRITE (6,92) ((BR(I,J), J = 1,INB), I = 1,INVRED)	ABCD3615
	GO TO 224	ABCD3616
221	WRITE (6,93) ((BR(I,J), J = 1,INB), I = 1,INVRED)	ABCD3617
	GO TO 224	ABCD3618
222	WRITE (6,94) ((BR(I,J), J = 1,INB), I = 1,INVRED)	ABCD3619
	GO TO 224	ABCD3620
223	WRITE (6,95) ((BR(I,J), J = 1,INB), I = 1,INVRED)	ABCD3621
224	WRITE (6,216)	ABCD3622
	DO 225 J = 1,INC	ABCD3623
	WRITE (6,44) (CR(J,I), I = 1,INVRED)	ABCD3624
225	CONTINUE	ABCD3625
	WRITE (6,217)	ABCD3626
	GO TO (226,227,228,229,230), INB	ABCD3627
226	WRITE (6,91) ((DR(I,J), J = 1,INB), I = 1,INC)	ABCD3628
	STOP	ABCD3629
227	WRITE (6,92) ((DR(I,J), J = 1,INB), I = 1,INC)	ABCD3630
	STOP	ABCD3631
228	WRITE (6,93) ((DR(I,J), J = 1,INB), I = 1,INC)	ABCD3632
	STOP	ABCD3633
229	WRITE (6,94) ((DR(I,J), J = 1,INB), I = 1,INC)	ABCD3634
	STOP	ABCD3635
230	WRITE (6,95) ((DR(I,J), J = 1,INB), I = 1,INC)	ABCD3636
	STOP	ABCD3637
44	FORMAT (1P10E12.4)	ABCD3638
45	FORMAT (1X, I5, 2X, ' THE VARIABLE IS NO. ', I3)	ABCD3639
50	FORMAT (1X, ' THE S.S. VARIABLE IS 0.0 ')	ABCD3640
55	FORMAT (1X, ' Y INVERSE = ')	ABCD3641
60	FORMAT (1X, ' THIS COLUMN OF X = ')	ABCD3642
65	FORMAT (1X, ' THIS IS THE S.S. SOLUTION ')	ABCD3643
70	FORMAT (1X, ' AINV IS SINGULAR ')	ABCD3644
75	FORMAT (1X, 7HAINV =)	ABCD3645
80	FORMAT (1X, 4HA =)	ABCD3646
81	FORMAT (1X, 4HC =)	ABCD3647
82	FORMAT (1X, 4HD =)	ABCD3648
85	FORMAT (1X, 4HB =)	ABCD3649
91	FORMAT (1X, 1PE12.4)	ABCD3650
92	FORMAT (1X, 1P2E12.4)	ABCD3651
93	FORMAT (1X, 1P3E12.4)	ABCD3652
94	FORMAT (1X, 1P4E12.4)	ABCD3653
95	FORMAT (1X, 1P5E12.4)	ABCD3654
214	FORMAT (1X, 5HAR =)	ABCD3655
215	FORMAT (1X, 5HBR =)	ABCD3656
216	FORMAT (1X, 5HCR =)	ABCD3657
217	FORMAT (1X, 5HDR =)	ABCD3658
280	FORMAT (1H1)	ABCD3659
282	FORMAT (1X, 'IGIN = ' , I5)	ABCD3660
296	FORMAT (1X, 'THE NEXT TRY FOR PVRDOT = ' , 1PE12.4)	ABCD3661
	END	ABCD3662

Subroutine ENGBAL

SUBROUTINE ENGBAL

ABCD3663

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IMPLICIT REAL*8 (A-H,O-Z)
LOGICAL ERRER, DUMSPL, FXFN2M, FXM2CP, FAN
COMMON /COMALL/ COM(1062)
DIMENSION WORD(2), ERR(9)
DIMENSION VAR(9), DEL(9), ERRB(9), DELVAR(9), EMAT(9,9), VMAT(9),
1 AMAT(9), DELSAV(9), AWORD(2)
EQUIVALENCE (WORD(1), COM(1)), (MODE, COM(6)), (INIT, COM(7)),
1 (ITRYS, COM(18)), (LOOPER, COM(19)), (NOMAP, COM(20)),
2 (NUMMAP, COM(21)), (MAPEDG, COM(22)), (TOLALL, COM(23)),
3 (ERR(1), COM(24)), (TFHPDS, COM(118)), (ZF, COM(136)),
4 (PCNF, COM(137)), (ZI, COM(139)), (PCNI, COM(140)),
5 (TFFIP, COM(141)), (T4, COM(156)), (TFFHP, COM(175)),
6 (TFLPDS, COM(275)), (TFIPDS, COM(278)), (TFFLP, COM(289)),
7 (ZC, COM(300)), (PCNC, COM(301)), (TIME, COM(993)),
8 (DT, COM(994)), (TF, COM(995)), (ISPOOL, COM(1044)),
9 (ITRAN, COM(1049)), (JTRAN, COM(1050)), (NSTEP, COM(1051)),
1 (IAMTRX, COM(1054)), (ERRER, COM(1056)), (DUMSPL, COM(1057)),
2 (FXFN2M, COM(1058)), (FXM2CP, COM(1059)), (FAN, COM(1061))
DATA AWORD /4HENG8, 4HAL /
DATA DELTA, VLIM, VCHNGE, NOMISX /1.0D-4, 0.1D0, 0.85D0, 4/
DATA DEL /9*0.0D0/
DATA DELSAV /9*1.0D-4/

C
IF (ITRAN .NE. 1) GO TO 100
CALL SYG(1)
JTRAN = 1
INIT = 1
NSTEP = NSTEP + 1
IF (IAMTRX .EQ. 1) NSTEP = NSTEP - 1
TIME = DT * DFLOAT(NSTEP)
IF (TIME .GT. TF) GO TO 100
CALL DISTRB
CALL COINLT
GO TO 101
100 IF (IAMTRX .EQ. 1) CALL DISTRB
IF (IAMTRX .EQ. 1) CALL COINLT
IF (IAMTRX .NE. 1) CALL PUTIN
101 IF (INIT .EQ. 1) GO TO 1
TFFHP = TFHPDS
TFFIP = TFIPDS
IF (FXM2CP) TFFIP = TFHPDS
TFFLP = TFLPDS
LOOPER = 0
NUMMAP = 0
NOMISS = 0
LOOP = 0
MISMAT = 0
NOMAP = 0
IGO = 2
DO 3 I = 1,9
VMAT(I) = 0.0D0
AMAT(I) = 0.0D0
DELVAR(I) = 0.0D0
DO 3 L = 1,9

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3	EMAT(I,L) = 0.0D0	ABCD3718
4	LOOPER = LOOPER + 1	ABCD3719
	CALL COFAN	ABCD3720
	WORD(1) = AWORD(1)	ABCD3721
	WORD(2) = AWORD(2)	ABCD3722
	IF (.NOT. FAN) DUMSPL = .TRUE.	ABCD3723
	IF (LOOPER .LE. ITRYS) GO TO 45	ABCD3724
	ERRER = .TRUE.	ABCD3725
	GO TO 26	ABCD3726
45	IF (NOMAP .GT. 0) GO TO 2	ABCD3727
	NUMMAP = 0	ABCD3728
5	VAR(1) = ZF * 100.0D0	ABCD3729
	VAR(2) = PCNF	ABCD3730
	IF (MODE .EQ. 3) VAR(2) = T4 / 10.0D0	ABCD3731
	VAR(3) = ZC * 100.0D0	ABCD3732
	VAR(4) = PCNC	ABCD3733
	IF (MODE .EQ. 1) VAR(4) = T4 / 10.0D0	ABCD3734
	VAR(5) = TFFHP	ABCD3735
	VAR(6) = TFFLP	ABCD3736
	VAR(7) = ZI * 100.0D0	ABCD3737
	VAR(8) = PCNI	ABCD3738
	VAR(9) = TFFIP	ABCD3739
	NMAX = 9	ABCD3740
	IF (FAN) GO TO 39	ABCD3741
	NMAX = 6	ABCD3742
	IF (ISPOOL .EQ. 2) GO TO 7	ABCD3743
	NMAX = 3	ABCD3744
	VAR(3) = TFFLP	ABCD3745
	GO TO 7	ABCD3746
39	IF (.NOT. FXFN2M .AND. (.NOT. DUMSPL)) GO TO 6	ABCD3747
	NMAX = 7	ABCD3748
	IF (DUMSPL) NMAX = 6	ABCD3749
6	IF (.NOT. FXM2CP) GO TO 7	ABCD3750
	NMAX = 7	ABCD3751
	VAR(4) = PCNI	ABCD3752
	VAR(5) = TFFIP	ABCD3753
7	DO 8 I = 1,NMAX	ABCD3754
	IF (DABS(EFR(I)) .GT. TOLALL) GO TO 9	ABCD3755
8	CONTINUE	ABCD3756
	IF (ITRAN .EQ. 1) CALL FOLL	ABCD3757
	CALL PERF	ABCD3758
	CALL ERROR	ABCD3759
9	IF (LOOP .GT. 0) GO TO 11	ABCD3760
	MAPEDG = 0	ABCD3761
	MAPSET = 0	ABCD3762
	DO 10 I = 1,NMAX	ABCD3763
	ERRB(I) = ERR(I)	ABCD3764
10	DEL(I) = VDELTA * VAR(I)	ABCD3765
	GO TO 14	ABCD3766
11	IF (MISMAT .GT. 0) GO TO 29	ABCD3767
	IF (MAPEDG .EQ. 0) GO TO 12	ABCD3768
	MAPEDG = 0	ABCD3769
	MAPSET = 1	ABCD3770
	VAR(LOOP) = VAR(LOOP) + 2.0D0 * DEL(LOOP)	ABCD3771

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12 GO TO 15
   IF (MAPSET .EQ. 0)  VAR(LOOP) = VAR(LOOP) + DEL(LOOP)
   IF (MAPSET .EQ. 1)  VAR(LOOP) = VAR(LOOP) - DEL(LOOP)
   MAPSET = 0
   DO 13 I = 1,NMAX
   IF (DEL(LOOP) .NE. 0.0D0)  DELSAV(LOOP) = DEL(LOOP)
   IF (DEL(LOOP) .EQ. 0.0D0)  DEL(LOOP) = DELSAV(LOOP)
13  EMAT(I,LOOP) = (ERRB(I) - ERR(I)) / DEL(LOOP)
14  LOOP = LOOP + 1
   IF (LOOP .GT. NMAX)  GO TO 17
   VAR(LOOP) = VAR(LOOP) - DEL(LOOP)
15  ZF = VAR(1) / 100.0D0
   IF (MODE .NE. 3)  PCNF = VAR(2)
   IF (MODE .EQ. 3)  T4 = VAR(2) * 10.0D0
   ZC = VAR(3) / 100.0D0
   IF (MODE .NE. 1)  PCNC = VAR(4)
   IF (MODE .EQ. 1)  T4 = VAR(4) * 10.0D0
   TFFHP = VAR(5)
   TFFLP = VAR(6)
   ZI = VAR(7) / 100.0D0
   PCNI = VAR(8)
   TFFIP = VAR(9)
   IF (.NOT. FXM2CP)  GO TO 16
   PCNI = VAR(4)
   TFFIP = VAR(5)
16  IF (ISPOOL .EQ. 1)  TFFLP = VAR(3)
   IF (ZI .LT. 0.0D0)  ZI = 0.05D0
   IF (ZF .LT. 0.0D0)  ZF = 0.05D0
   IF (ZC .LT. 0.0D0)  ZC = 0.05D0
   GO TO (2,4), IGO
17  DO 18 I = 1,NMAX
18  AMAT(I) = - ER RB(I)
   DO 20 I = 1,NMAX
   IZERO = 0
   DO 19 LOOP = 1,NMAX
   IF (EMAT(I,LOOP) .EQ. 0.0D0)  IZERO = IZERO + 1
19  CONTINUE
   IF (IZERO .LT. NMAX)  GO TO 20
   WRITE (6,32) I
   LOOPER = ITRY5 + 100
   GO TO 26
20  CONTINUE
   DO 22 LOOP = 1,NMAX
   IZERO = 0
   DO 21 I = 1,NMAX
   IF (EMAT(I,LOOP) .EQ. 0.0D0)  IZERO = IZERO + 1
   IF (IZERO .LT. NMAX)  GO TO 22
   WRITE (6,33) LOOP
   LOOPER = ITRY5 + 100
   GO TO 26
22  CONTINUE
23  CALL MATRIX (EMAT,VMAT,AMAT,NMAX)
   LBIG = 0
   VARBIG = 0.0D0

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ABCD3772
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ABCD3825

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	DO 24 L = 1,NMAX	ABCD3826
	ABSVAR = DABS(VMAT(L))	ABCD3827
	IF (ABSVAR .LE. V LIM * VAR(L)) GO TO 24	ABCD3828
	IF (ABSVAR .LE. VARBIG) GO TO 24	ABCD3829
	LBIG = L	ABCD3830
	VARBIG = ABSVAR	ABCD3831
24	CONTINUE	ABCD3832
	VRATIO = 1.0D0	ABCD3833
	IF (LBIG .GT. 0) VRATIO = V LIM * VAR(LBIG) / VARBIG	ABCD3834
	ERRAVE = 0.0D0	ABCD3835
	VMTAVE = 0.0D0	ABCD3836
	DELAVE = 0.0D0	ABCD3837
	FNMAX = NMAX	ABCD3838
	DO 25 L = 1,NMAX	ABCD3839
	DELVAR(L) = VRATIO * VMAT(L)	ABCD3840
	ERRAVE = ERRAVE + DABS(AMAT(L)) / FNMAX	ABCD3841
	VAR(L) = VAR(L) + DELVAR(L)	ABCD3842
	VMTAVE = VMTAVE + DABS(VMAT(L)) / FNMAX	ABCD3843
25	DELAVE = DELAVE + DABS(DELVAR(L)) / FNMAX	ABCD3844
	IF (MISMAT .GT. 0) GO TO 31	ABCD3845
	IF (NOMISS .EQ. 0) MISMAT = 1	ABCD3846
	IF (MISMAT .EQ. 0) IGO = 1	ABCD3847
26	WRITE (8,34) LOOPER	ABCD3848
	DO 27 I = 1,NMAX	ABCD3849
27	WRITE (8,35) AMAT(I), (EMAT(I,L), L=1,9), VMAT(I), DELVAR(I), VAR(I)	ABCD3850
	WRITE (8,36) ERRAVE, VMTAVE, DELAVE	ABCD3851
28	IF (LOOPER .LT. ITRY5) GO TO 15	ABCD3852
	CALL ERROR	ABCD3853
	RETURN	ABCD3854
29	VMTAVX = VMTAVE	ABCD3855
	DO 30 I = 1,NMAX	ABCD3856
30	AMAT(I) = - ERR(I)	ABCD3857
	GO TO 23	ABCD3858
31	WRITE (8,37) AMAT,ERRAVE,DELVAR,DELAVE,VMAT,VMTAVE,VAR	ABCD3859
	MISMAT = MISMAT + 1	ABCD3860
	IF (VMTAVE .LT. VCHNGE * VMTAVX) GO TO 28	ABCD3861
	WRITE (8,38)	ABCD3862
	IF (MISMAT .LT. NOMISX) NOMISS = 1	ABCD3863
	MISMAT = 0	ABCD3864
	LOOP = 0	ABCD3865
	IGO = 2	ABCD3866
	GO TO 5	ABCD3867
C		ABCD3868
C		ABCD3869
32	FORMAT (4H0ROW,I2,16H IS ZERO IN EMAT)	ABCD3870
33	FORMAT (7H0COLUMN,I2,16H IS ZERO IN EMAT)	ABCD3871
34	FORMAT (8HB ERRB,28X,23HEXFOR MATRIX AFTER LOOP,I4,29X,4HVMAT,	ABCD3872
	1 6X,6HDELVAR,7X,14HVARIA B L E\$\$\$\$\$)	ABCD3873
35	FORMAT (1H0,F8.4,10F9.3,2F11.4,6H\$\$\$\$\$)	ABCD3874
36	FORMAT (1H0,F8.4,32X,14HAVERAGE VALUES,31X,2F11.4,6H\$\$\$\$\$)	ABCD3875
37	FORMAT (12H0----- AMAT,10F11.5,6H\$\$\$\$\$,/,12H -----DELVAR,	ABCD3876
	1 10F11.6,6H\$\$\$\$\$,/,12H ----- VMAT,10F11.6,6H\$\$\$\$\$,/,	ABCD3877
	2 12H ----- VAR,9F11.6,6H\$\$\$\$\$)	ABCD3878
38	FORMAT (1H0,50X,22HCHANGE TOO SMALL\$\$\$\$\$)	ABCD3879
	END	ABCD3880

Subroutine ERROR

SUBROUTINE ERROR	ABCD3881
IMPLICIT REAL*8 (A-H,O-Z)	ABCD3882
LOGICAL ERROR, DUMSPL, FXFN2M, FXM2CP, AFTFAN, FAN	ABCD3883
COMMON /COMALL/ COM(1062)	ABCD3884
DIMENSION WORD(2)	ABCD3885
DIMENSION AWORD(2)	ABCD3886
EQUIVALENCE (WORD(1), COM(1)), (MODE, COM(6)), (IDUMP, COM(8)),	ABCD3887
1 (LOOPER, COM(19)), (ZF, COM(136)), (PCNF, COM(137)),	ABCD3888
2 (ZI, COM(139)), (PCNI, COM(140)), (T4, COM(156)), (ZC, COM(300)),	ABCD3889
3 (PCNC, COM(301)), (ISPOOL, COM(1044)), (ICOAFB, COM(1045)),	ABCD3890
4 (ICODUC, COM(1046)), (ICOMIX, COM(1047)), (ERREP, COM(1056)),	ABCD3891
5 (DUMSPL, COM(1057)), (FXFN2M, COM(1058)), (FXM2CP, COM(1059)),	ABCD3892
6 (AFTFAN, COM(1060)), (FAN, COM(1061))	ABCD3893
DATA AWORD /4HCOMM, 4HON /	ABCD3894
IF (ICOAFB .LT. 1) ICOAFB = 0	ABCD3895
IF (ICOMIX .LT. 1) ICOMIX = 0	ABCD3896
IF (ICODUC .LT. 1) ICODUC = 0	ABCD3897
IF (ICOAFB .NE. 0) WRITE (6,10) ICOAFB	ABCD3898
IF (ICODUC .NE. 0) WRITE (6,11) ICODUC	ABCD3899
IF (ICOMIX .NE. 0) WRITE (6,12) ICOMIX	ABCD3900
ERROR = .TRUE.	ABCD3901
WRITE (6,2) WORD	ABCD3902
WORD(1) = AWORD(1)	ABCD3903
WORD(2) = AWORD(2)	ABCD3904
WRITE (6,3) WORD,ZF,PCNF,ZI,PCNI,ZC,PCNC,T4,MODE	ABCD3905
WRITE (6,4)	ABCD3906
WRITE (6,5) (COM(I), I = 33,394)	ABCD3907
WRITE (6,4)	ABCD3908
WRITE (6,8) DUMSPL, FXFN2M, FXM2CP, AFTFAN, FAN, ISPOOL	ABCD3909
WRITE (6,4)	ABCD3910
WRITE (6,7) LOOPER	ABCD3911
IF (IDUMP .EQ. 0) GO TO 1	ABCD3912
WRITE (6,6)	ABCD3913
CALL SYG (2)	ABCD3914
1 CALL ENGBAL	ABCD3915
RETURN	ABCD3916
C	ABCD3917
C	ABCD3918
2 FORMAT (28H0AN ERROR HAS BEEN FOUND IN ,A4,A2)	ABCD3919
3 FORMAT (1H0,A4,A2,9X,7E15.6,I4)	ABCD3920
4 FORMAT (2H0)	ABCD3921
5 FORMAT (1H ,8E15.6)	ABCD3922
6 FORMAT (1H1)	ABCD3923
7 FORMAT (25H0FAILED TO CONVERGE AFTER ,I4,6H LOOPS)	ABCD3924
8 FORMAT (1H ,5E15.6,I12)	ABCD3925
10 FORMAT (27H THE ERROR IN COAFBN IS AT ,I3)	ABCD3926
11 FORMAT (27H THE ERROR IN CDDUCT IS AT ,I3)	ABCD3927
12 FORMAT (27H THE ERROR IN COMIX IS AT ,I3)	ABCD3928
END	ABCD3929

Subroutine ETAAB

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SUBROUTINE ETAAB (FAR,EM6,P6,ETA,ETAADS,ETAASV,P6DS,P6DSAV,AM6DS, ABCD3930
1 AM6DSV,IDES,FAR7DS,FAR7SV) ABCD3931
IMPLICIT REAL*8 (A-H,O-Z) ABCD3932
DIMENSION TFAR(25), ETABRT(25), EM6T(7), DELM6(7), P6T(14), ABCD3933
1 DELP6(14), X(3), Y(3) ABCD3934
DATA TFAR/.039D0, .0585D0, .0732D0, .0878D0, .0976D0, .1171D0, ABCD3935
1 .1268D0, .1463D0, .1619D0, .1834D0, .1951D0, .2195D0, .2439D0, ABCD3936
2 .2927D0, .3415D0, .4146D0, .4634D0, .5366D0, .6341D0, .7317D0, ABCD3937
3 .8293D0, .9268D0, 1.0D0, 1.0634D0, 1.7D0/ ABCD3938
DATA ETABRT/.94D0, .9887D0, 1.0193D0, 1.0306D0, 1.0227D0, ABCD3939
1 .9672D0, .9377D0, .9207D0, .9354D0, .9626D0, .9773D0, 1.0193D0, ABCD3940
2 1.0532D0, 1.077D0, 1.0781D0, 1.077D0, 1.0747D0, 1.0668D0, ABCD3941
3 1.0578D0, 1.051D0, 1.0374D0, 1.0192D0, 1.0D0, .9626D0, .9151D0/ ABCD3942
DATA EM6T/1.0D0, 1.071D0, 1.19D0, 1.309D0, 1.428D0, 1.547D0, ABCD3943
1 1.666D0 / ABCD3944
DATA DELM6/0.0D0, .013D0, .041D0, .073D0, .11D0, .147D0, .187D0/ ABCD3945
DATA P6T/.22D0, .2267D0, .25D0, .3D0, .3333D0, .3767D0, .4167D0, ABCD3946
1 .5D0, .5833D0, .5556D0, .75D0, .8333D0, .9167D0, 1.0D0/ ABCD3947
DATA DELP6/-.142D0, -.125D0, -.1D0, -.075D0, -.062D0, -.05D0, ABCD3948
1 -.041D0, -.027D0, -.019D0, -.013D0, -.008D0, -.004D0, -.0021D0, ABCD3949
2 0.0D0/ ABCD3950
IF (IDES .NE. 1) GO TO 5 ABCD3951
EMULT = ETAADS / ETAASV ABCD3952
FMULT = FAR7DS / FAR7SV ABCD3953
AMULT = AM6DS / AM6DSV ABCD3954
PMULT = P6DS / P6DSAV ABCD3955
DO 1 K = 1,25 ABCD3956
ETABRT(K) = ETABRT(K) * EMULT ABCD3957
1 TFAR(K) = TFAR(K) * FMULT ABCD3958
DO 3 K = 1,7 ABCD3959
3 EM6T(K) = EM6T(K) * AMULT ABCD3960
DO 4 M = 1,14 ABCD3961
4 P6T(M) = P6T(M) * PMULT ABCD3962
ETAASV = ETAADS ABCD3963
P6DSAV = P6DS ABCD3964
FAR7SV = FAR7DS ABCD3965
AM6DSV = AM6DS ABCD3966
RETURN ABCD3967
5 N = 0 ABCD3968
IF (FAR .GT. 0.067D0) GO TO 8 ABCD3969
DO 6 J = 1,25 ABCD3970
IF (FAR .GE. TFAR(J)) N = J - 1 ABCD3971
6 CONTINUE ABCD3972
IF (N .EQ. 0) N = 1 ABCD3973
IF (N .GE. 24) N = 23 ABCD3974
DO 7 I = 1,3 ABCD3975
NN = N - 1 + I ABCD3976
X(I) = TFAR(NN) ABCD3977
7 Y(I) = ETABRT(NN) ABCD3978
CALL PARABO (X,Y,FAR,ETA1) ABCD3979
GO TO 9 ABCD3980
8 ETA1 = - 2.0D0 * FAR + .1948D0 ABCD3981

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9	M = 0	ABCD3982
	DO 10 J = 1,7	ABCD3983
	IF (EM6 .GE. EM6T(J)) M = J - 1	ABCD3984
10	CONTINUE	ABCD3985
	IF (M .EQ. 0) M = 1	ABCD3986
	IF (M .GE. 6) M = 5	ABCD3987
	DO 11 I = 1,3	ABCD3988
	MM = M - 1 + I	ABCD3989
	X(I) = EM6T(MM)	ABCD3990
11	Y(I) = DELM6(MM)	ABCD3991
	CALL PARABO (X,Y,EM6,COR1)	ABCD3992
	L = 0	ABCD3993
	DO 12 J = 1,14	ABCD3994
	IF (P6 .GE. P6T(J)) L = J - 1	ABCD3995
12	CONTINUE	ABCD3996
	IF (L .EQ. 0) L = 1	ABCD3997
	IF (L .GE. 13) L = 12	ABCD3998
	DO 13 I = 1,3	ABCD3999
	LL = L - 1 + I	ABCD4000
	X(I) = P6T(LL)	ABCD4001
13	Y(I) = DELP6(LL)	ABCD4002
	CALL PARABO (X,Y,P6,COR2)	ABCD4003
	ETA = ETA1 * (1.0D0 - COR1) * (1.0D0 + COR2)	ABCD4004
	RETURN	ABCD4005
	END	ABCD4006

Subroutine FASTBK

SUBROUTINE FASTBK	ABCD4007
IMPLICIT REAL*8 (A-H,O-Z)	ABCD4008
LOGICAL FAN	ABCD4009
COMMON /COMALL/ COM(1062)	ABCD4010
EQUIVALENCE (P1, COM(33)), (T25, COM(46)), (P25, COM(47)),	ABCD4011
1 (H25, COM(48)), (S25, COM(49)), (WFD, COM(72)), (XFP1, COM(76)),	ABCD4012
2 (XWG24, COM(77)), (XFAR24, COM(78)), (XT25, COM(79)),	ABCD4013
3 (XP25, COM(80)), (XH25, COM(81)), (XS25, COM(82)),	ABCD4014
4 (XWG55, COM(83)), (XFAR55, COM(84)), (XT55, COM(85)),	ABCD4015
5 (XP55, COM(86)), (XH55, COM(87)), (XS55, COM(88)),	ABCD4016
6 (XWFB, COM(89)), (XWFD, COM(90)), (WFB, COM(192)),	ABCD4017
7 (T21, COM(263)), (H21, COM(264)), (S21, COM(265)),	ABCD4018
8 (T55, COM(272)), (H55, COM(273)), (S55, COM(274)),	ABCD4019
9 (BLF, COM(316)), (WAF, COM(319)), (WG24, COM(321)),	ABCD4020
1 (FAR24, COM(322)), (WG55, COM(323)), (FAR55, COM(324)),	ABCD4021
2 (P21, COM(377)), (P55, COM(387)), (FAN, COM(1061))	ABCD4022
XT55 = T55	ABCD4023
XP55 = P55	ABCD4024
XH55 = H55	ABCD4025
XS55 = S55	ABCD4026
IF (FAN) GO TO 1	ABCD4027
T25 = T21	ABCD4028
P25 = P21	ABCD4029
H25 = H21	ABCD4030
S25 = S21	ABCD4031
WG24 = WAF - BLF	ABCD4032

1	XT25 = T25 XP25 = P25 XH25 = H25 XS25 = S25 XWFB = WFB XWG55 = WG55 XFAR55 = FAR55 XWFD = WFD XWG24 = WG24 XFAR24 = FAR24 XXP1 = P1 CALL COMIX RETURN END	ABCD4033 ABCD4034 ABCD4035 ABCD4036 ABCD4037 ABCD4038 ABCD4039 ABCD4040 ABCD4041 ABCD4042 ABCD4043 ABCD4044 ABCD4045 ABCD4046
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Subroutine FCNTRL

SUBROUTINE FCNTRL IMPLICIT REAL*8 (A-H,O-Z) RETURN END	ABCD4047 ABCD4048 ABCD4049 ABCD4050
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Subroutine FRTOSD

SUBROUTINE FRTOSD IMPLICIT REAL*8 (A-H,O-Z) LOGICAL FAN COMMON /COMALL/ COM(1062) EQUIVALENCE (P1, COM(33)), (H3, COM(153)), (WAC, COM(191)), 1 (XP1, COM(200)), (XT21, COM(201)), (XP21, COM(202)), 2 (XH21, COM(203)), (XS21, COM(204)), (XH3, COM(205)), 3 (XWAF, COM(206)), (XWAC, COM(207)), (XBLF, COM(208)), 4 (XBLDU, COM(209)), (T21, COM(253)), (H21, COM(264)), 5 (S21, COM(265)), (BLF, COM(316)), (BLDU, COM(317)), 6 (WAF, COM(319)), (P21, COM(377)), (FAN, COM(1061)) XP1 = P1 XWAF = WAF XWAC = WAC XBLF = BLF XBLDU = BLDU XH3 = H3 XT21 = T21 XP21 = P21 XH21 = H21 XS21 = S21 IF (FAN) CALL CODUCT IF (.NOT. FAN) CALL FASTBK RETURN END	ABCD4051 ABCD4052 ABCD4053 ABCD4054 ABCD4055 ABCD4056 ABCD4057 ABCD4058 ABCD4059 ABCD4060 ABCD4061 ABCD4062 ABCD4063 ABCD4064 ABCD4065 ABCD4066 ABCD4067 ABCD4068 ABCD4069 ABCD4070 ABCD4071 ABCD4072 ABCD4073 ABCD4074 ABCD4075
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Function GUESS

FUNCTION GUESS (M, T, TD, P, PD, W, WD, D, DD, VD) IMPLICIT REAL*8 (A-H,O-Z)	ABCD4076 ABCD4077
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	IF (M .EQ. 0) GUESS = VD * ((T / TD) ** 1.6D0) * ((DD / D) **	ABCD4078
1	0.5D0)	ABCD4079
	IF (M .LE. 0 .OR. M .GT. 9) RETURN	ABCD4080
	GO TO (1,2,3,3,5,6,7,8,9), M	ABCD4081
1	GUESS = VD * ((P / PD) ** 1.8D0) * ((DD / D) ** 0.33D0)	ABCD4082
	RETURN	ABCD4083
2	GUESS = VD * ((W / WD) ** 0.33D0) * DD / D	ABCD4084
	RETURN	ABCD4085
3	GUESS = VD * ((P / PD) ** .5D0)	ABCD4086
	RETURN	ABCD4087
5	GUESS = VD * ((T / TD) ** 1.1D0) * ((DD / D) ** .7D0)	ABCD4088
	RETURN	ABCD4089
6	GUESS = VD * P / PD * ((D / DD) ** 0.25D0)	ABCD4090
	RETURN	ABCD4091
7	GUESS = VD * ((P / PD) ** 0.62D0) * ((D / DD) ** 0.31D0)	ABCD4092
	RETURN	ABCD4093
8	GUESS = VD * ((T / TD) ** 1.2D0) * DD / D	ABCD4094
	RETURN	ABCD4095
9	GUESS = VD * P / PD * ((D / DD) ** 1.5D0)	ABCD4096
	RETURN	ABCD4097
	END	ABCD4098

Subroutine INDUMY

	SUBROUTINE INDUMY (CNI,ZI,WACI,IDES)	ABCD4099
	IMPLICIT REAL*8 (A-H,O-Z)	ABCD4100
	COMMON /COMDAT/ COMD(5423)	ABCD4101
	DIMENSION CNXXI(15), PRXXI(15,15), WACXXI(15,15), ETAXXI(15,15),	ABCD4102
1	NPTXI(15)	ABCD4103
	DIMENSION XCNXX(15), WACAR(15)	ABCD4104
	EQUIVALENCE (CNXXI(1), COMD(1381)), (PRXXI(1,1), COMD(1396)),	ABCD4105
1	(WACXXI(1,1), COMD(1621)), (ETAXXI(1,1), COMD(1846)),	ABCD4106
2	(NCNXXI, COMD(5328)), (NPTXI(1), COMD(5329))	ABCD4107
	DATA XCNXX / .001D0, .1D0, .2D0, .3D0, .5D0, .8D0, 1.0D0, 1.5D0,	ABCD4108
1	2.0D0, 3.0D0, 4.0D0, 5.0D0, 6.0D0, 7.0D0, 9.0D0 /	ABCD4109
	DATA WACAR / 5.0D0, 4.5D0, 4.0D0, 3.5D0, 3.0D0, 2.5D0, 2.0D0,	ABCD4110
1	1.5D0, 1.0D0, .8D0, .6D0, .4D0, .25D0, .1D0, .05D0 /	ABCD4111
	IF (IDES .NE. 1) GO TO 1	ABCD4112
	WAIDS = WACI	ABCD4113
	CNIDS = CNI	ABCD4114
	ZI = 2.0D0 / 3.5D0	ABCD4115
1	NCNXXI = 15	ABCD4116
	DO 2 I = 1,15	ABCD4117
	NPTXI(I) = 15	ABCD4118
	CNXXI(I) = XCNXX(I) * CNIDS	ABCD4119
	DO 2 J = 1,15	ABCD4120
	PRXXI(I,J) = FLOAT(J + 3) / 4.0D0	ABCD4121
	ETAXXI(I,J) = 1.0D0	ABCD4122
2	WACXXI(J,I) = WACAR(I) * (.993D0 + .001D0 * FLOAT(J)) * WAIDS	ABCD4123
	RETURN	ABCD4124
	END	ABCD4125

	SUBROUTINE MATRIX (E,V,A,N)	ABCD4126
	IMPLICIT REAL*8 (A-H,O-Z)	ABCD4127
	DIMENSION E(9,9), V(9), A(9), PIV(10), T(9,10)	ABCD4128
	NN = N + 1	ABCD4129
	NM = N - 1	ABCD4130
	DO 1 I = 1,N	ABCD4131
	T(I,NN) = A(I)	ABCD4132
1	DO 1 J = 1,N	ABCD4133
	T(I,J) = E(I,J)	ABCD4134
	DO 7 I = 1,N	ABCD4135
	TEMP = 0.0D0	ABCD4136
	DO 2 J = 1,N	ABCD4137
	IF (TEMP .GT. DABS(T(J,I))) GO TO 2	ABCD4138
	TEMP = DABS(T(J,I))	ABCD4139
	IPIV = J	ABCD4140
2	CONTINUE	ABCD4141
	IP1 = I + 1	ABCD4142
	DO 3 J = IP1,NN	ABCD4143
3	PIV(J) = T(IPIV,J) / T(IPIV,I)	ABCD4144
	IFROM = N	ABCD4145
	ITO = N	ABCD4146
4	IF (IFROM .EQ. IPIV) GO TO 6	ABCD4147
	RM = - T(IFROM,I)	ABCD4148
	DO 5 J = IP1,NN	ABCD4149
5	T(ITO,J) = T(IFROM,J) + RM * PIV(J)	ABCD4150
	ITO = ITO - 1	ABCD4151
6	IFROM = IFROM - 1	ABCD4152
	IF (IFROM .GE. I) GO TO 4	ABCD4153
	DO 7 J = IP1,NN	ABCD4154
7	T(I,J) = PIV(J)	ABCD4155
	DO 8 I = 1,NM	ABCD4156
	J = NN - I	ABCD4157
	K = N - I	ABCD4158
	DO 8 L = J,N	ABCD4159
8	T(K,NN) = T(K,NN) - T(K,L) * T(L,NN)	ABCD4160
	DO 9 I = 1,N	ABCD4161
9	V(I) = T(I,NN)	ABCD4162
	RETURN	ABCD4163
	END	ABCD4164

Subroutine NOZCTR

SUBROUTINE NOZCTR	ABCD4165
IMPLICIT REAL*8 (A-H,O-Z)	ABCD4166
RETURN	ABCD4167
END	ABCD4168

Subroutine OUTPUT

SUBROUTINE OUTPUT	ABCD4169
IMPLICIT REAL*8 (A-H,O-Z)	ABCD4170
LOGICAL DUMSPL, FXFN2M, FXM2CP, A*TFAN, FAN	ABCD4171
COMMON /COMALL/ COM(1062)	ABCD4172
DIMENSION WORD(2)	ABCD4173

	DIMENSION W(6,5), AWORD1(2), AWORD2(2)	ABCD4174
	EQUIVALENCE (WORD(1), COM(1)), (IDES, COM(3)), (MODE, COM(6)),	ABCD4175
1	(IDUMP, COM(8)), (IGASM, COM(10)), (IDBURN, COM(11)),	ABCD4176
2	(IAFTBN, COM(12)), (IDSHOC, COM(15)), (IMSHOC, COM(16)),	ABCD4177
3	(LOOPER, COM(19)), (T24, COM(42)), (A28, COM(50)),	ABCD4178
4	(A28SAV, COM(51)), (A29, COM(60)), (A29SAV, COM(61)),	ABCD4179
5	(ZF, COM(136)), (PCNF, COM(137)), (ZI, COM(139)),	ABCD4180
6	(PCNI, COM(140)), (T4, COM(155)), (ETAR, COM(187)),	ABCD4181
7	(AM, COM(195)), (ALTP, COM(196)), (SPC, COM(248)),	ABCD4182
8	(FG, COM(257)), (FN, COM(258)), (ZC, COM(300)), (PCNC, COM(301)),	ABCD4183
9	(PCBLID, COM(305)), (T7, COM(343)), (A8, COM(346)),	ABCD4184
1	(A8SAV, COM(347)), (A9, COM(356)), (A9SAV, COM(357)),	ABCD4185
2	(TIME, COM(993)), (TPRINT, COM(996)), (DTPRNT, COM(997)),	ABCD4186
3	(ISPOOL, COM(1044)), (ITRAN, COM(1049)), (IAMTRX, COM(1054)),	ABCD4187
4	(DUMSPL, COM(1057)), (FXFN2M, COM(1058)), (FXM2CP, COM(1059)),	ABCD4188
5	(AFTFAN, COM(1060)), (FAN, COM(1061))	ABCD4189
	DATA AWORD1, AWORD2 /4HOUTP, 4HUT , 4HCOMM, 4HON /	ABCD4190
	DATA W / 4HSUBS, 4HONIC, 4H C-D, 4H NOZ, 4HZLE , 4H ,	ABCD4191
1	4HSHOC, 4HK IN, 4HSIDE, 4H C-D, 4H NOZ, 4HZLE ,	ABCD4192
2	4HSHOC, 4HK OU, 4HTSID, 4HE C-, 4HD NO, 4HZZLE,	ABCD4193
3	4HSUBS, 4HONIC, 4H CON, 4HVERG, 4H. NO, 4HZZLE,	ABCD4194
4	4HSONI, 4HC CO, 4HNVER, 4HGERG, 4H NOZ, 4HZLE /	ABCD4195
	IF (IAMTRX .EQ. 1 .AND. ITRAN .EQ. 1) GO TO 24	ABCD4196
	TPRINT = TPRINT + DTPRNT	ABCD4197
	IF (ITRAN .EQ. 1) WRITE(6,29) TIME	ABCD4198
	WORD(1) = AWORD1(1)	ABCD4199
	WORD(2) = AWORD1(2)	ABCD4200
	IF (IDBURN .GT. 0) GO TO 2	ABCD4201
	IF (IAFTBN .GT. 0) GO TO 1	ABCD4202
	WRITE (6,7) WORD,AM,ALTP,T4,ETAR	ABCD4203
	GO TO 3	ABCD4204
1	WRITE (6,8) WORD,AM,ALTP,T4,T7,ETAR	ABCD4205
	GO TO 3	ABCD4206
2	WRITE (6,9) WORD,AM,ALTP,T4,T24,ETAR	ABCD4207
3	IF (FXFN2M) WRITE (6,17)	ABCD4208
	IF (FXM2CP) WRITE (6,18)	ABCD4209
	IF (FAN) GO TO 25	ABCD4210
	WRITE(6,26) ISPOOL	ABCD4211
	GO TO 27	ABCD4212
25	IF (.NOT. FXFN2M .AND. (.NOT. FXM2CP) .AND. (.NOT. DUMSPL))	ABCD4213
1	WRITE (6,19)	ABCD4214
	IF (DUMSPL) WRITE (6,23)	ABCD4215
	IF (PCBLID .EQ. 0.0D0) WRITE (6,20)	ABCD4216
	IF (PCBLID .EQ. 0.0D0 .AND. AFTFAN) WRITE (6,21)	ABCD4217
	IF (PCBLID .NE. 0.0D0 .AND. AFTFAN) WRITE (6,22)	ABCD4218
27	CALL CONOUT(2)	ABCD4219
	WRITE (6,10) (W(I,IMSHOC),I=1,6),FG,FN,SPC	ABCD4220
	IF (IGASM .GT. 0 .OR. .NOT. FAN) GO TO 4	ABCD4221
	WRITE (6,11) (W(I,IDSHOC),I=1,6)	ABCD4222
4	WRITE (6,12) LOOPER	ABCD4223
	IF (IDES .NE. 1) GO TO 5	ABCD4224
	WORD(1) = AWORD2(1)	ABCD4225
	WORD(2) = AWORD2(2)	ABCD4226
	WRITE (6,13) WORD,ZF,PCNF,ZI,PCNI,ZC,PCNC,T4,MODE	ABCD4227

	WRITE (6,14)	ABCD4228
	WRITE (6,15) (COM(I), I = 33,394)	ABCD4229
	WRITE (6,14)	ABCD4230
	WRITE (6,15) DUMSPL, FXFN2M, FXM2CP, APTFAN, FAN	ABCD4231
	WRITE (6,14)	ABCD4232
	WRITE (6,16)	ABCD4233
24	IF (IDES .EQ. 1) GO TO 6	ABCD4234
5	A8 = A8SAV	ABCD4235
	A9 = A9SAV	ABCD4236
	A28 = A28SAV	ABCD4237
	A29 = A29SAV	ABCD4238
	IF (IDUMP .NE. 2) GO TO 6	ABCD4239
	WRITE (6,16)	ABCD4240
	CALL SYG (2)	ABCD4241
6	CALL ENGBAL	ABCD4242
	RETURN	ABCD4243
C		ABCD4244
C		ABCD4245
C		ABCD4246
7	FORMAT (1H , A4, A2, 14X, 7H AM=, F7.3, 6X, 7H ALTP=, F7.0,	ABCD4247
	1 6X, 7H T4=, F8.2, 25X, 7H ETAR=, F7.4)	ABCD4248
8	FORMAT (1H , A4, A2, 14X, 7H AM=, F7.3, 6X, 7H ALTP=, F7.0,	ABCD4249
	1 6X, 7H T4=, F8.2, 5X, 7H T7=, F8.2, 5X, 7H ETAR=, F7.4)	ABCD4250
9	FORMAT (1H , A4, A2, 14X, 7H AM=, F7.3, 6X, 7H ALTP=, F7.0,	ABCD4251
	1 6X, 7H T4=, F8.2, 5X, 7H T24=, F8.2, 5X, 7H ETAR=, F7.4)	ABCD4252
10	FORMAT (1H0, 5HMAIN , 6A4, 9X, 3HFG=, F9.2, 18X, 3HPN=, F9.2,	ABCD4253
	1 18X, 4HSFC=, F8.5)	ABCD4254
11	FORMAT (6H DUCT ,6A4)	ABCD4255
12	FORMAT (16H0CONVERGED AFTER,I4,6H LOOPS,/,1H1)	ABCD4256
13	FORMAT (1H ,A4,A2,9X,7E15.6,I4)	ABCD4257
14	FORMAT (1H)	ABCD4258
15	FORMAT (1H ,8E15.6)	ABCD4259
16	FORMAT (1H1)	ABCD4250
17	FORMAT (51H0FAN AND MIDDLE SPOOL ARE ATTACHED , USE INNER AND ,	ABCD4261
	1 14HOUTER TURBINES)	ABCD4262
18	FORMAT (49H0MIDDLE AND COMPRESSOR SPOOLS ARE ATTACHED , USE ,	ABCD4263
	1 25HMIDDLE AND OUTER TURBINES)	ABCD4264
19	FORMAT (19H0THREE SPOOL ENGINE)	ABCD4265
20	FORMAT (21H0NO AIRFLOW INTO WING)	ABCD4266
21	FORMAT (1H+,22X,14H, AFT-TURBOFAN)	ABCD4267
22	FORMAT (14H0 AFT-TURBOFAN)	ABCD4268
23	FORMAT (22H0MIDDLE SPOOL IS DUMMY)	ABCD4269
26	FORMAT(1H0,I4,15H SPOOL TURBOJET)	ABCD4270
29	FORMAT(1H1,20X,7H TIME=,F7.4)	ABCD4271
	END	ABCD4272

Subroutine PARABO

SUBROUTINE PARABO (X,Y,XD,YANS)	ABCD4273
IMPLICIT REAL*8 (A-H,O-Z)	ABCD4274
DIMENSION X(3), Y(3)	ABCD4275
X1M2 = X(1) - X(2)	ABCD4276
X1M3 = X(1) - X(3)	ABCD4277
X2M1 = X(2) - X(1)	ABCD4278

X2M3 = X(2) - X(3)	ABCD4279
X3M2 = X(3) - X(2)	ABCD4280
X1SQ = X(1) * X(1)	ABCD4281
X2SQ = X(2) * X(2)	ABCD4282
X3SQ = X(3) * X(3)	ABCD4283
Y1M2 = Y(1) - Y(2)	ABCD4284
Y1M3 = Y(1) - Y(3)	ABCD4285
A = (X1M2 * Y1M3 - X1M3 * Y1M2) / X1M2 / X1M3 / X3M2	ABCD4286
B = ((X1SQ - X2SQ) * Y1M3 - (X1SQ - X3SQ) * Y1M2) / X1M2 / X1M3 /	ABCD4287
1 X2M3	ABCD4288
D = (Y(1) * X2SQ - Y(2) * X1SQ - B * X(2) * X(1) * X2M1) / (X2SQ	ABCD4289
1 - X1SQ)	ABCD4290
YANS = (A * XD + B) * XD + D	ABCD4291
RETURN	ABCD4292
END	ABCD4293

Subroutine PERF

SUBROUTINE PERF	ABCD4294
IMPLICIT REAL*8 (A-H,O-Z)	ABCD4295
LOGICAL SI, DUMSPL, AFTFAN, FAN	ABCD4296
COMMON /COMALL/ COM(1062)	ABCD4297
DIMENSION WORD(2)	ABCD4298
DIMENSION AWORD(2)	ABCD4299
EQUIVALENCE (WORD(1), 'COM(1)', (IDES, COM(3)), (IGASM, COM(10)),	ABCD4300
1 (P1, COM(33)), (A29, COM(50)), (V29, COM(63)), (PS29, COM(65)),	ABCD4301
2 (WAD, COM(71)), (WFD, COM(72)), (PCNI, COM(140)),	ABCD4302
3 (WFB, COM(192)), (CS, COM(194)), (AM, COM(195)),	ABCD4303
4 (WG37, COM(210)), (A39, COM(219)), (V39, COM(221)),	ABCD4304
5 (PS39, COM(226)), (FGMWNG, COM(230)), (FGPWNG, COM(231)),	ABCD4305
6 (FNWNG, COM(232)), (FNMAIN, COM(233)), (FWOVFN, COM(234)),	ABCD4306
7 (DELFG, COM(236)), (DELFN, COM(237)), (DELSFC, COM(238)),	ABCD4307
8 (CVDWNG, COM(239)), (CVDNOZ, COM(240)), (CVMNOZ, COM(241)),	ABCD4308
9 (VA, COM(242)), (VJD, COM(243)), (VJV, COM(244)),	ABCD4309
1 (VJM, COM(245)), (WFT, COM(246)), (WGT, COM(247)),	ABCD4310
2 (SFC, COM(248)), (TFAR, COM(249)), (FRD, COM(250)),	ABCD4311
3 (FGMD, COM(251)), (FGMM, COM(252)), (FGPD, COM(253)),	ABCD4312
4 (FGPM, COM(254)), (FGM, COM(255)), (FGP, COM(256)),	ABCD4313
5 (FG, COM(257)), (FN, COM(258)), (FFOVFN, COM(259)),	ABCD4314
6 (FCOVFN, COM(260)), (FMNOFN, COM(261)), (FNOVFD, COM(262)),	ABCD4315
7 (WA32, COM(271)), (PCBLID, COM(305)), (CNI, COM(309)),	ABCD4316
8 (WAI, COM(311)), (BLOB, COM(318)), (WAF, COM(319)),	ABCD4317
9 (WG24, COM(321)), (WG7, COM(334)), (A9, COM(356)),	ABCD4318
1 (PS9, COM(359)), (V9, COM(360)), (WFA, COM(368))	ABCD4319
EQUIVALENCE (TIME, COM(993)), (TPRINT, COM(996)),	ABCD4320
1 (ITRAN, COM(1049)), (SI, COM(1055)), (DUMSPL, COM(1057)),	ABCD4321
2 (AFTFAN, COM(1060)), (FAN, COM(1061))	ABCD4322
DATA AWORD /4H PE, 4HRF /	ABCD4323
WORD(1) = AWORD(1)	ABCD4324
WORD(2) = AWORD(2)	ABCD4325
IF (SI) GO TO 100	ABCD4326
G = 32.174049D0	ABCD4327
CAPSF = 2116.2170D0	ABCD4328
GO TO 101	ABCD4329

100	G = 1.0D0	ABCD4330
	CAPSF = 1.0D0	ABCD4331
101	WFT = WFB + WFD + WFA	ABCD4332
	WAT = WAF - BLOB	ABCD4333
	IF (AFTFAN) WAT = WAT + WAI	ABCD4334
	WGT = WAT + WFT	ABCD4335
	TFAR = WFT / WAT	ABCD4336
	VA = AM * CS	ABCD4337
	FRD = VA * WAF / G	ABCD4338
	IF (AFTFAN) FRD = FRD + VA * WAI / G	ABCD4339
	VJM = CVMNOZ * V9	ABCD4340
	FGMM = VJM * WG7 / G	ABCD4341
	FGPM = CAPSF * (PS9 - P1) * A9	ABCD4342
	IF (IGASM * .GT. 0 .OR. .NOT. FAN) GO TO 1	ABCD4343
	VJD = CVDNOZ * V29	ABCD4344
	FGMD = VJD * WG24 / G	ABCD4345
	FGPD = CAPSF * (PS29 - P1) * A29	ABCD4346
1	VJW = 0.0D0	ABCD4347
	FGMWNG = 0.0D0	ABCD4348
	FGPWNG = 0.0D0	ABCD4349
	FGWING = 0.0D0	ABCD4350
	FNWING = 0.0D0	ABCD4351
	IF (PCBLID .EQ. 0.0D0) GO TO 2	ABCD4352
	VJW = CVDWNG * V39	ABCD4353
	FGMWNG = VJW * WG37 / G	ABCD4354
	FGPWNG = CAPSF * (PS39 - P1) * A39	ABCD4355
	FGWING = FGMWNG + FGPWNG	ABCD4356
	FNWING = FGWING - VA * WA32 / G	ABCD4357
2	FGM1 = FGMM + FGMD	ABCD4358
	FGM = FGM1 + FGMWNG	ABCD4359
	FGP1 = FGPM + FGPD	ABCD4360
	FGP = FGP1 + FGPWNG	ABCD4361
	FNMAIN = FGM1 + FGP1 - VA * (WAF - WA32) / G	ABCD4362
	IF (AFTFAN) FNMAIN = FNMAIN - VA * WAI / G	ABCD4363
	FG = FGM + FGP	ABCD4364
	FN = FG - FRD	ABCD4365
	SFC = 3600.0D0 * WFT / FN	ABCD4366
	FG = DELFG * FG	ABCD4367
	FN = DELFN * FN	ABCD4368
	SFC = DELSFC * SFC	ABCD4369
	FFAN = FGMD + FGPD - VA * WAD / G	ABCD4370
	FCORE = FNMAIN - FFAN	ABCD4371
	FFOVFN = FFAN / FN	ABCD4372
	FCOVFN = FCORE / FN	ABCD4373
	FWOVFN = FNWING / FN	ABCD4374
	FMNOFN = FNMAIN / FN	ABCD4375
	IF (IDES .EQ. 1) FDES = FN	ABCD4376
	FNQVFD = FN / FDES	ABCD4377
	IF (.NOT. DUMSPL) GO TO 3	ABCD4378
	PCNI = 1.0D0	ABCD4379
	CNI = 0.0D0	ABCD4380
3	IF (ITRAN .EQ. 1 .AND. TIME .LT. TPFINT) CALL ENGBAL	ABCD4381
	CALL OUTPUT	ABCD4382
	CALL ERROR	ABCD4383
	RETURN	ABCD4384
	END	ABCD4385

Subroutine PROCOM

	SUBROUTINE PROCOM (FARX,TEX,CSEX,AKEX,CPEX,REX,PHI,HEX)	ABCD4395
	IMPLICIT REAL*8 (A-H,O-Z)	ABCD4397
	LOGICAL SI	ABCD4398
	COMMON /COMALL/ COM(1062)	ABCD4399
	EQUIVALENCE (SI, COM(1055))	ABCD4390
C	IF SI UNITS ARE USED, CONVERT TEX TO DEGREES RANKINE	ABCD4391
	IF (SI) TEX = TEX * 9.0D0 / 5.0D0	ABCD4392
	IF (FARX .GT. .067623D0) FARX = .067623D0	ABCD4393
	IF (TEX .LT. 300.0D0) TEX = 300.0D0	ABCD4394
	IF (TEX .GT. 4000.0D0) TEX = 4000.0D0	ABCD4395
	IF (FARX .LT. 0.0D0) FARX = 0.0D0	ABCD4396
C	AIR PATH	ABCD4397
	CPA = ((((((1.011554D-25 * TEX - 1.452677D-21) * TEX +	ABCD4398
	1 7.6215767D-18) * TEX - 1.5128259D-14) * TEX - 6.7178376D-12) *	ABCD4399
	2 TEX + 6.5519486D-08) * TEX - 5.1536879D-05) * TEX + 2.5020051D-01	ABCD4400
	HEA = ((((((1.2644425D-26 * TEX - 2.0752522D-22) * TEX +	ABCD4401
	1 1.270263D-18) * TEX - 3.0256518D-15) * TEX - 1.6794594D-12) *	ABCD4402
	2 TEX + 2.1839826D-08) * TEX - 2.576844D-05) * TEX +	ABCD4403
	3 2.5020051D-01) * TEX - 1.7558886D+00	ABCD4404
	SEA = 2.5020051D-01 * DLOG(TEX) + ((((((1.4450767D-26 * TEX -	ABCD4405
	1 2.4211288D-22) * TEX + 1.5243153D-18) * TEX - 3.7920648D-15) *	ABCD4406
	2 TEX - 2.239279D-12) * TEX + 3.2759743D-08) * TEX -	ABCD4407
	3 5.1576879D-05) * TEX + 4.54323D-02	ABCD4408
	IF (FARX .LE. 0.0D0) GO TO 5	ABCD4409
C	FUEL/AIR PATH	ABCD4410
	CPF = ((((((7.267871D-25 * TEX - 1.3335668D-20) * TEX +	ABCD4411
	1 1.0212913D-16) * TEX - 4.2051104D-13) * TEX + 9.9685793D-10) *	ABCD4412
	2 TEX - 1.3771901D-06) * TEX + 1.225863D-03) * TEX + 7.3815638D-02	ABCD4413
	HEF = ((((((9.0848388D-26 * TEX - 1.9050949D-21) * TEX +	ABCD4414
	1 1.7021525D-17) * TEX - 8.4102208D-14) * TEX + 2.4921698D-10) *	ABCD4415
	2 TEX - 4.5906332D-07) * TEX + 6.129315D-04) * TEX +	ABCD4416
	3 7.3816638D-02) * TEX + 3.058153D+01	ABCD4417
	SEF = 7.3816638D-02 * DLOG(TEX) + ((((((1.038267D-25 * TEX -	ABCD4418
	1 2.2226118D-21) * TEX + 2.0425826D-17) * TEX - 1.0512776D-13) *	ABCD4419
	2 TEX + 3.3228928D-10) * TEX - 5.8859505D-07) * TEX +	ABCD4420
	3 1.225863D-03) * TEX + 6.483398D-01	ABCD4421
5	CPEX = (CPA + FARX * CPF) / (1.0D0 + FARX)	ABCD4422
	HEX = (HEA + FARX * HEF) / (1.0D0 + FARX)	ABCD4423
	PHI = (SEA + FARX * SEF) / (1.0D0 + FARX)	ABCD4424
	AMW = 28.97D0 - .946186D0 * FARX	ABCD4425
	REX = 1.986375D0 / AMW	ABCD4426
	AKEX = CPEX / (CPEX - REX)	ABCD4427
	CSEX = DSQRT(AKEX * REX * TEX * 25031.37D0)	ABCD4428
	IF (.NOT. SI) RETURN	ABCD4429
	CPEX = CPEX * 4185.7666D0	ABCD4430
	HEX = HEX * 2325.4259D0	ABCD4431
	PHI = PHI * 4185.7666D0	ABCD4432
	REX = REX * 4185.7666D0	ABCD4433
	CSEX = CSEX * .3048D0	ABCD4434

TEX = TEX * 5.0DC / 9.0DC
 RETURN
 END

ABCD4435
 ABCD4436
 ABCD4437

Subroutine PUTIN

SUBROUTINE PUTIN	ABCD4438
IMPLICIT REAL*8 (A-H,O-Z)	ABCD4439
LOGICAL SI, ERRER, DUMSPL, FXFN2M, FXM2CP, AFTFAN, FAN	ABCD4440
COMMON /COMALL/ COM(1062)	ABCD4441
DIMENSION WORD(2), TIMEPT(50)	ABCD4442
DIMENSION XSAVE(396), AWORD(2)	ABCD4443
EQUIVALENCE (WORD(1), COM(1)), (IDES, COM(3)), (MODE, COM(6)),	ABCD4444
1 (INIT, COM(7)), (IDUMP, COM(8)), (IAMTP, COM(9)),	ABCD4445
2 (IGASM, COM(10)), (IDBURN, COM(11)), (IAFTBN, COM(12)),	ABCD4446
3 (IDCD, COM(13)), (IMCD, COM(14)), (NOZFLT, COM(17)),	ABCD4447
4 (ITRYS, COM(18)), (TOLALL, COM(23)), (AM23, COM(35)),	ABCD4448
5 (I24, COM(42)), (A28, COM(50)), (ETAD, COM(73)),	ABCD4449
6 (DPDUDS, COM(75)), (T2, COM(92)), (P2, COM(93)),	ABCD4450
7 (I4DS, COM(101)), (AM55, COM(107)), (PS55, COM(110)),	ABCD4451
8 (IFHPDS, COM(118)), (CNHPDS, COM(119)), (ETHPDS, COM(120)),	ABCD4452
9 (PCNFPDS, COM(124)), (PRFPDS, COM(125)), (ETAPDS, COM(126)),	ABCD4453
1 (HPEXT, COM(129)), (WACCDS, COM(130)), (ZCDS, COM(133)),	ABCD4454
2 (WAFCD, COM(135)), (PCNFD, COM(137)), (PCBLF, COM(138)),	ABCD4455
3 (ZIDS, COM(146)), (PCNIDS, COM(147)), (T4, COM(156)),	ABCD4455
4 (PCBLHP, COM(166)), (PCBLIP, COM(167)), (PCBLLP, COM(168)),	ABCD4457
5 (PCBLDU, COM(169)), (PCBLOB, COM(170)), (PRIDS, COM(180)),	ABCD4458
6 (ETAIDS, COM(181)), (WAICDS, COM(183)), (ETARDS, COM(184)),	ABCD4459
7 (WFBDS, COM(185)), (ZFDS, COM(186)), (ETAR, COM(187)),	ABCD4460
8 (WFB, COM(192)), (AM, COM(195)), (ALTP, COM(196)), (DPCDS, COM(197)),	ABCD4461
9 (A38, COM(211)), (DPWGDS, COM(235)), (DELFG, COM(236)),	ABCD4462
1 (DELFN, COM(237)), (DELSFC, COM(238)), (CVDWNG, COM(239))	ABCD4463
EQUIVALENCE (CVDNOZ, COM(240)), (CVMNOZ, COM(241)),	ABCD4464
1 (TFLPDS, COM(275)), (CNLPDS, COM(276)), (ETLPDS, COM(277)),	ABCD4465
2 (TFIPDS, COM(278)), (CNIPDS, COM(279)), (ETIPDS, COM(280)),	ABCD4466
3 (PRCDS, COM(297)), (ETACDS, COM(298)), (PCNC, COM(301)),	ABCD4467
4 (PCBLCD, COM(302)), (PCNCDS, COM(303)), (PCBLI, COM(304)),	ABCD4468
5 (PCBLID, COM(305)), (WACI, COM(310)), (WACC, COM(320)),	ABCD4469
6 (AM6, COM(327)), (A6, COM(328)), (T7DS, COM(342)),	ABCD4470
7 (T7, COM(343)), (A8, COM(346)), (ETAADS, COM(366)),	ABCD4471
8 (DPAFDS, COM(367)), (WFA, COM(368)), (ETAA, COM(369)),	ABCD4472
9 (VFAN, COM(395)), (VINTC, COM(396)), (VCOMP, COM(397)),	ABCD4473
1 (VCOMB, COM(398)), (VHPTRB, COM(399)), (VIPTRB, COM(400)),	ABCD4474
2 (VLPTRB, COM(401)), (VAFIBN, COM(402)), (VFDUCT, COM(403)),	ABCD4475
3 (VWDUCT, COM(404)), (XNHPDS, COM(423)), (XNIPDS, COM(424)),	ABCD4476
4 (XNLPDS, COM(425)), (PMIHP, COM(426)), (PMIIP, COM(427)),	ABCD4477
5 (PMILP, COM(428)), (DELT1, COM(429)), (TIMEPT(1), COM(941)),	ABCD4478
6 (PRFNEW, COM(991)), (PRCNEW, COM(992)), (TIME, COM(993)),	ABCD4479
7 (DT, COM(994)), (TF, COM(995)), (TPRINT, COM(996)),	ABCD4480
8 (DTPRNT, COM(997)), (ISPOL, COM(1044)), (KKG0, COM(1048)),	ABCD4481
9 (ITRAN, COM(1049)), (JTRAN, COM(1050)), (NSTEP, COM(1051)),	ABCD4482
1 (IAMTRX, COM(1054)), (SI, COM(1055)), (ERRER, COM(1056))	ABCD4483
EQUIVALENCE (DUMSPL, COM(1057)), (FXFN2M, COM(1058)),	ABCD4484
1 (FXM2CP, COM(1059)), (AFTFAN, COM(1060)), (FAN, COM(1061)),	ABCD4485

2 (WAFCDs, COM(1062))	ABCD4485
DATA AWORD /4HPUTI, 4HN /	ABCD4487
C *** IDES =1 FOR CALCULATING DESIGN POINT	ABCD4488
C *** MODE =0 FOR CONSTANT T4	ABCD4489
C *** MODE =1 FOR CONSTANT PCNC	ABCD4490
C *** MODE =2 FOR CONSTANT WFB	ABCD4491
C *** MODE =3 FOR CONSTANT PCNF	ABCD4492
C *** INIT =1 WILL NOT INITIALIZE POINT	ABCD4493
C *** IDUMP =1 WILL DUMP LOOPING WRITE-OUTS IF ERROR OCCURS	ABCD4494
C *** IDUMP =2 WILL DUMP LOOPING WRITE-OUTS AFTER EVERY POINT	ABCD4495
C *** IAMTP =0 WILL USE INPUT AM AND MIL SPEC ETAR	ABCD4496
C *** IAMTP =1 WILL USE INPUT AM AND INPUT ETAR	ABCD4497
C *** IAMTP =2 WILL USE T2 AS T1=T1+T2 AND STANDARD P1	ABCD4498
C *** IAMTP =3 WILL USE P2 AND STANDARD T1	ABCD4499
C *** IAMTP =4 WILL USE T2 AND P2	ABCD4500
C *** IAMTP =5 WILL USE RAM2 FOR SPECIAL RECOVERY	ABCD4501
C *** IGASMx=-1 SEPARATE FLOW, INPUT A6	ABCD4502
C *** IGASMx=0 SEPARATE FLOW, A6=A55	ABCD4503
C *** IGASMx=1 WILL MIX DUCT AND MAIN STREAMS, A6=A25+A55	ABCD4504
C *** IGASMx=2 WILL MIX DUCT AND MAIN STREAMS, INPUT A6	ABCD4505
C *** IDBURN=1 FOR DUCT BURNING, INPUT T24	ABCD4506
C *** IDBURN=2 FOR DUCT BURNING, INPUT WFD	ABCD4507
C *** IAFTBN=1 FOR AFTERBURNING, INPUT T7	ABCD4508
C *** IAFTBN=2 FOR AFTERBURNING, INPUT WFA	ABCD4509
C *** IDCD =1 DUCT NOZZLE WILL BE C-D	ABCD4510
C *** IMCD =1 MAIN NOZZLE WILL BE C-D	ABCD4511
C *** NOZFLT=1 FOR FLOATING MAIN NOZZLE	ABCD4512
C *** NOZFLT=2 FOR FLOATING DUCT NOZZLE	ABCD4513
C *** NOZFLT=3 FOR FLOATING MAIN AND DUCT NOZZLES	ABCD4514
C *** ITRYs =N NUMBER OF PASSES THRU ENGINE BEFORE QUITTING	ABCD4515
NAMELIST /DATAIN/ ISPOOL,FAN,SI,DELT1,IDES,MODE,IDUMP,IAMTP,	ABCD4516
1 IGASMx,IDBURN,IAFTBN,IDCD,IMCD,NOZFLT,ITRYS,FXFN2M,FXM2CP,	ABCD4517
2 APTFAN,DUMSPL,TOLALL,DELFG,DELFP,DELSFC,PCNFDS,PRFDS,ETAFDS,	ABCD4518
3 PCNCDS,PRCDS,ETACDS,T4DS,WFBDS,ETABDS,DPCDS,ETHPDS,ETLPDS,	ABCD4519
4 DEDUDS,T7DS,ETAADS,DPAFDS,A6,A8,A28,PS55,AM55,CVDNOZ,CVMNOZ,T2,	ABCD4520
5 P2,T4,WAFCDs,WACCDs,HPEXT,AM,ALTP,ETAR,PCNF,PCNC,WFB,PCBLF,PCNI,	ABCD4521
6 PCBLC,PCBLDU,PCBLOB,PCBLHP,PCBLLP,T24,ETAD,T7,WFA,ETAA,AM6,AM23,	ABCD4522
7 DPMGDS,A38,PCNIDS,PCBLIP,ZFDS,ZCDS,ZIDS,PCBLID,TFHPDS,CNHPDS,	ABCD4523
8 TFIPLS,CNIPDS,TFLPDS,CNLPDS,PRIDS,ETAIDS,ETIPDS,WAICDS,PCBLI,	ABCD4524
9 CVDWNG,ITRAN,DTPRNT,TF,INIT,DT,XNHPDS,XNIPDS,XNLPDS,PMIHP,PMIIP,	ABCD4525
1 PMILP,VFAN,VINTC,VCOMP,VCOMB,VHPTRB,VIPTRB,VLPTRB,VAFTBN,VFDUCT,	ABCD4526
2 VWDUCT,IAMTRX	ABCD4527
WORD(1) = AWORD(1)	ABCD4528
WORD(2) = AWORD(2)	ABCD4529
ITRAN = 0	ABCD4530
JTRAN = 0	ABCD4531
TIME = 0.000	ABCD4532
NSTEP = 0	ABCD4533
TPRINT = 0.000	ABCD4534
DTPRNT = 0.000	ABCD4535
1 CALL ZERO	ABCD4536
IF (KKGO .EQ. 1) GO TO 5	ABCD4537
IDES = 0	ABCD4538
READ (5,DATAIN)	ABCD4539

	IF (.NOT. ERRER) GO TO 102	ABCD4540
	IF (IAFTBN .GT. 0 .OR. IDBURN .GT. 0 .OR. NOZFLT .GT. 0) GO TO 1	ABCD4541
102	ERRER = .FALSE.	ABCD4542
C	TABLE IS REFERENCED TO COMMON/ALL/FIRST ENTRY	ABCD4543
	IF (IDES .EQ. 0) GO TO 7	ABCD4544
	IF (KKGO .NE. 2) GO TO 3	ABCD4545
	TEMP1 = COM(325)	ABCD4546
	TEMP2 = COM(326)	ABCD4547
	TEMP3 = COM(336)	ABCD4548
	TEMP4 = COM(370)	ABCD4549
	DO 2 I = 1,392	ABCD4550
2	COM(I+2) = XSAVE(I)	ABCD4551
	DO 205 I = 1,4	ABCD4552
205	COM(I+1056) = XSAVE(I+392)	ABCD4553
	COM(325) = TEMP1	ABCD4554
	COM(326) = TEMP2	ABCD4555
	COM(336) = TEMP3	ABCD4556
	COM(370) = TEMP4	ABCD4557
	READ (5,DATAIN)	ABCD4558
C	SAVE INPUT IN CASE OF LOOP ON PRESSURE PATIOS	ABCD4559
3	TEMP1 = XSAVE(323)	ABCD4560
	TEMP2 = XSAVE(324)	ABCD4561
	TEMP3 = XSAVE(334)	ABCD4562
	TEMP4 = XSAVE(368)	ABCD4563
	DO 4 I = 1,392	ABCD4564
4	XSAVE(I) = COM(I+2)	ABCD4565
	DO 405 I = 1,4	ABCD4566
405	XSAVE(I+392) = COM(I+1056)	ABCD4567
	XSAVE(323) = TEMP1	ABCD4568
	XSAVE(324) = TEMP2	ABCD4569
	XSAVE(334) = TEMP3	ABCD4570
	XSAVE(368) = TEMP4	ABCD4571
	GO TO 7	ABCD4572
5	TEMP1 = COM(325)	ABCD4573
	TEMP2 = COM(326)	ABCD4574
	TEMP3 = COM(336)	ABCD4575
	TEMP4 = COM(370)	ABCD4576
	DO 6 I = 1,392	ABCD4577
6	COM(I+2) = XSAVE(I)	ABCD4578
	DO 605 I = 1,4	ABCD4579
605	COM(I+1056) = XSAVE(I+392)	ABCD4580
	COM(325) = TEMP1	ABCD4581
	COM(326) = TEMP2	ABCD4582
	COM(336) = TEMP3	ABCD4583
	COM(370) = TEMP4	ABCD4584
	WRITE (6,8) PRFDS,PRFNEW,PRCDS,PRCNEW	ABCD4585
	PRCDS = PRCNEW	ABCD4586
	PRFDS = PRFNEW	ABCD4587
7	KKGO = 2	ABCD4588
	IF (IAFTBN .GT. 0 .OR. IDBURN .GT. 0 .OR. NOZFLT .GT. 0) INIT = 1	ABCD4589
	IF (MODE .EQ. 0) WRITE (8,9) IDES,AM,ALTP,T4,T24,T7	ABCD4590
	IF (MODE .EQ. 1) WRITE (8,10) IDES,AM,ALTP,PCNC,T24,T7	ABCD4591
	IF (MODE .EQ. 2) WRITE (8,11) IDES,AM,ALTP,WFB,T24,T7	ABCD4592
	IF (DUMSPL) WAICDS = WACCDS	ABCD4593

	IF (IDES .NE. 1) GO TO 101	ABCD4594
	WAPC = WAPCDS	ABCD4595
	WACI = WAICDS	ABCD4596
	WACC = WACCD5	ABCD4597
101	CALL COINLT	ABCD4598
	RETURN	ABCD4599
C		ABCD4600
C		ABCD4601
8	FORMAT (18HOCHANGE PRFDS FROM, F9.3, 4H TO, F9.3, 17H AND PRCD5	ABCD4602
	1 FROM, F10.3, 4H TO, F10.3)	ABCD4603
9	FORMAT (1H0, 7H ID5=, I3, 10X, 7H AM=, F7.3, 6X, 7H ALTP=,	ABCD4604
	1 F7.0, 6X, 7H T4=, F8.2, 5X, 7H T24=, F8.2, 5X, 7H T7=,	ABCD4605
	2 F8.2, 6H\$\$\$\$\$)	ABCD4606
10	FORMAT (1H0, 7H ID5=, I3, 10X, 7H AM=, F7.3, 6X, 7H ALTP=,	ABCD4607
	1 F7.0, 6X, 7H PCNC=, F8.3, 5X, 7H T24=, F8.2, 5X, 7H T7=,	ABCD4608
	2 F8.2, 6H\$\$\$\$\$)	ABCD4609
11	FORMAT (1H0, 7H ID5=, I3, 10X, 7H AM=, F7.3, 6X, 7H ALTP=,	ABCD4610
	1 F7.0, 6X, 7H WFB=, F8.4, 5X, 7H T24=, F8.2, 5X, 7H T7=,	ABCD4611
	2 F8.2, 6H\$\$\$\$\$)	ABCD4612
	END	ABCD4613

Subroutine RAM

	SUBROUTINE RAM (AM,ETAR)	ABCD4614
	IMPLICIT REAL*8 (A-H,O-Z)	ABCD4615
	ETAR = 1.0D0	ABCD4616
	IF (AM .LE. 1.0D0) RETURN	ABCD4617
	IF (AM .GT. 5.0D0) GO TO 3	ABCD4618
	ETAR = 1.0D0 - 0.075D0 * ((AM - 1.0D0) ** 1.35D0)	ABCD4619
	RETURN	ABCD4620
3	ETAR = 800.0D0 / ((AM ** 4) + 935.0D0)	ABCD4621
	RETURN	ABCD4622
	END	ABCD4623

Subroutine RAM2

	SUBROUTINE FAM2 (AM,ETAR)	ABCD4624
	IMPLICIT REAL*8 (A-H,O-Z)	ABCD4625
	DIMENSION PRINLT(15), FMN(15), X(3), Y(3)	ABCD4626
	DATA FMN /0.0D0, .1D0, .2D0, .3D0, .4D0, .5D0, .6D0, 1.1D0,	ABCD4627
	1 1.2D0, 1.4D0, 1.6D0, 1.8D0, 2.2D0, 2.4D0, 2.7D0/	ABCD4628
	DATA PRINLT / .9D0, .932D0, .95D0, .961D0, .968D0, .97D0, .9791D0,	ABCD4629
	1 .97D0, .9681D0, .958D0, .94D0, .9181D0, .858D0, .8201D0, .75D0/	ABCD4630
	M = 0	ABCD4631
	DO 1 J = 1,15	ABCD4632
	IF (AM .GE. FMN(J)) M = J - 1	ABCD4633
1	CONTINUE	ABCD4634
	IF (M .EQ. 0) M = 1	ABCD4635
	IF (M .GE. 14) M = 13	ABCD4636
	DO 2 I = 1,3	ABCD4637
	MM = M - 1 + I	ABCD4638
	X(I) = FMN(MM)	ABCD4639
2	Y(I) = PRINLT(MM)	ABCD4640
	CALL PARABO (X,Y,AM,ETAR)	ABCD4641
	RETURN	ABCD4642
	END	ABCD4643

Subroutine ROLL

	SUBROUTINE ROLL	ABCD4644
	IMPLICIT REAL*8 (A-H,O-Z)	ABCD4645
	COMMON /COMALL/ COM(1062)	ABCD4646
	DIMENSION FO(50,4), SO(10,6), PDATA(5,50), TIMEPT(50)	ABCD4647
	EQUIVALENCE (FO(1,1), COM(430)), (SO(1,1), COM(631)),	ABCD4648
	1 (PDATA(1,1), COM(691)), (TIMEPT(1), COM(941))	ABCD4649
	DO 1 I = 1,50	ABCD4650
	FO(I,2) = FO(I,1)	ABCD4651
1	FO(I,4) = FO(I,3)	ABCD4652
	DO 2 I = 1,10	ABCD4653
	SO(I,6) = SO(I,5)	ABCD4654
	SO(I,5) = SO(I,4)	ABCD4655
	SO(I,3) = SO(I,2)	ABCD4656
2	SO(I,2) = SO(I,1)	ABCD4657
	DO 3 I = 1,49	ABCD4658
	N1 = 51 - I	ABCD4659
	N0 = 50 - I	ABCD4660
	TIMEPT(N1) = TIMEPT(N0)	ABCD4661
	DO 3 J = 1,5	ABCD4662
3	PDATA(J,N1) = PDATA(J,N0)	ABCD4663
	RETURN	ABCD4664
	END	ABCD4665

Subroutine SEARCH

	SUBROUTINE SEARCH (P,A,B,C,D,AX,NA,BX,CX,DX,NO,NAM,NOM,NCODE)	ABCD4666
	IMPLICIT REAL*8 (A-H,O-Z)	ABCD4667
	COMMON /COMALL/ COM(1062)	ABCD4668
	DIMENSION AX(NAM), BX(NAM,NOM), CX(NAM,NOM), DX(NAM,NOM),	ABCD4669
	1 NO(NAM), Q(9)	ABCD4670
	EQUIVALENCE (TOLALL, COM(23))	ABCD4671
C ***	NEEDS SUBROUTINE AFQUIR	ABCD4672
C ***	AX AND BX MUST BE STORED LO TO HI	ABCD4673
C ***	P=INPUT PROPORTION BETWEEN 0.0 AND 1.0	ABCD4674
C	IF NOT INPUT, P MUST EQUAL -1.	ABCD4675
C ***	NCODE=00 OK	ABCD4676
C	NCODE=01 A LO	ABCD4677
C	NCODE=02 A HI	ABCD4678
C	NCODE=07 ERROR	ABCD4679
C	NCODE=10 B LO	ABCD4680
C	NCODE=20 B HI	ABCD4681
	EXTR(AAA,EBB,CCC) = AAA + BBE * (CCC - AAA)	ABCD4682
	NCODE = 0	ABCD4683
	C = 0.0D0	ABCD4684
	D = 0.0D0	ABCD4685
C ***	FIND A	ABCD4686
	DO 1 I = 1,NA	ABCD4687
	IH = I	ABCD4688
	IF (A .LT. AX(I)) GO TO 2	ABCD4689

1	CONTINUE	ABCD4690
	IF (A .GT. AX(IH)) NCODE = 2	ABCD4691
	A = AX(IH)	ABCD4692
	GO TO 3	ABCD4693
2	IF (IH .GT. 1) GO TO 3	ABCD4694
	NCODE = 1	ABCD4695
	IH = 2	ABCD4696
	A = AX(1)	ABCD4697
3	IL = IH - 1	ABCD4698
	LIMH = NO(IH)	ABCD4699
	LIML = NO(IL)	ABCD4700
C ***	FIND B	ABCD4701
	PRM = (A - AX(IL)) / (AX(IH) - AX(IL))	ABCD4702
	PP = P	ABCD4703
	IF (P .GE. 0.0D0) GO TO 5	ABCD4704
	BL = EXTR(BX(IL,1), PRM, BX(IH,1))	ABCD4705
	BH = EXTR(BX(IL,LIML), PRM, BX(IH,LIMH))	ABCD4706
	IF (B .GE. BL) GO TO 4	ABCD4707
	NCODE = NCODE + 10	ABCD4708
	B = BL	ABCD4709
	GO TO 5	ABCD4710
4	IF (B .LE. BH) GO TO 5	ABCD4711
	NCODE = NCODE + 20	ABCD4712
	BHM = EXTR(BX(IL,LIML-1), PRM, BX(IH,LIMH-1))	ABCD4713
	CHM = EXTR(CX(IL,LIML-1), PRM, CX(IH,LIMH-1))	ABCD4714
	DHM = EXTR(DX(IL,LIML-1), PRM, DX(IH,LIMH-1))	ABCD4715
	CH = EXTR(CX(IL,LIML), PRM, CX(IH,LIMH))	ABCD4716
	DH = EXTR(DX(IL,LIML), PRM, DX(IH,LIMH))	ABCD4717
	CSLOPE = (CH - CHM) / (BH - BHM)	ABCD4718
	DSLOPE = (DH - DHM) / (BH - BHM)	ABCD4719
	C = CH + CSLOPE * (B - BH)	ABCD4720
	D = DH + DSLOPE * (B - BH)	ABCD4721
	RETURN	ABCD4722
5	PP = 0.5D0	ABCD4723
	Q(2) = 0.0D0	ABCD4724
	Q(3) = 0.0D0	ABCD4725
6	BH = EXTR(BX(IH,1), PP, BX(IH,LIMH))	ABCD4726
	BL = EXTR(BX(IL,1), PP, BX(IL,LIML))	ABCD4727
	DO 7 J = 2,LIMH	ABCD4728
	JH = J	ABCD4729
	IF (BH .LT. BX(IH,J)) GO TO 8	ABCD4730
7	CONTINUE	ABCD4731
8	JL = JH - 1	ABCD4732
	DO 9 K = 2,LIML	ABCD4733
	KH = K	ABCD4734
	IF (BL .LT. BX(IL,K)) GO TO 10	ABCD4735
9	CONTINUE	ABCD4736
10	KL = KH - 1	ABCD4737
	PR = (BX(IH,JL) - BH) / (BX(IH,JH) - BX(IH,JL))	ABCD4738
	CH = EXTR(CX(IH,JL), -PR, CX(IH,JH))	ABCD4739
	DH = EXTR(DX(IH,JL), -PR, DX(IH,JH))	ABCD4740
	PR = (BX(IL,KL) - BL) / (BX(IL,KH) - BX(IL,KL))	ABCD4741
	CL = EXTR(CX(IL,KL), -PR, CX(IL,KH))	ABCD4742
	DL = EXTR(DX(IL,KL), -PR, DX(IL,KH))	ABCD4743

	BT = EXTR(BL, PRM, BH)	ABCD4744
	CT = EXTR(CL, PRM, CH)	ABCD4745
	DT = EXTR(DL, PRM, DH)	ABCD4746
	IF (P .GE. 0.0D0) GO TO 13	ABCD4747
	DIR = DSQRT(B / BT)	ABCD4748
	ERR = (B - BT) / B	ABCD4749
	CALL AFQUIR (Q(1), PP, ERR, 0.0D0, 25.0D0, 1.0D0*TOLALL, DIR, PT, ICON)	ABCD4750
	GO TO (11, 13, 12), ICON	ABCD4751
11	PP = PT	ABCD4752
	IF (PP .LT. 0.0D0) PP = 0.0D0	ABCD4753
	IF (PP .GT. 1.0D0) PP = 1.0D0	ABCD4754
	GO TO 6	ABCD4755
12	NCODE = 7	ABCD4756
13	B = BT	ABCD4757
	C = CT	ABCD4758
	D = DT	ABCD4759
	RETURN	ABCD4760
	END	ABCD4761

Subroutine SYG

	SUBROUTINE SYG (ICON)	ABCD4762
	DIMENSION WORD(132)	ABCD4763
	DATA ONEDOL /4H\$ /	ABCD4764
	GO TO (1, 2), ICON	ABCD4765
1	REWIND 8	ABCD4766
	RETURN	ABCD4767
C	TERMINATE THE FILE	ABCD4768
2	WRITE (8, 10)	ABCD4769
	REWIND 8	ABCD4770
C	READ RECORD	ABCD4771
3	READ (8, 11) (WORD(I), I=1, 132)	ABCD4772
C	CHECK FOR 12 LEADING DOLLAR SIGNS	ABCD4773
	DO 4 I = 1, 12	ABCD4774
	IF (WORD(I) .NE. ONEDOL) GO TO 5	ABCD4775
4	CONTINUE	ABCD4776
	RETURN	ABCD4777
C	CHECK FOR 6 TRAILING DOLLAR SIGNS	ABCD4778
5	DO 8 I = 1, 132	ABCD4779
	IF (WORD(I) .NE. ONEDOL) GO TO 8	ABCD4780
	K = I + 5	ABCD4781
	DO 7 J = I, K	ABCD4782
	IF (WORD(J) .NE. ONEDOL) GO TO 8	ABCD4783
7	CONTINUE	ABCD4784
	GO TO 9	ABCD4785
8	CONTINUE	ABCD4786
	WRITE (6, 12)	ABCD4787
	RETURN	ABCD4788
C	PRINT LINE	ABCD4789
9	I = I - 1	ABCD4790
	WRITE (6, 11) (WORD(M), M=1, I)	ABCD4791
	GO TO 3	ABCD4792
C		ABCD4793
C		ABCD4794

10	FORMAT (12H\$\$\$\$\$\$\$\$\$)	ABCD4795
11	FORMAT (132A1)	ABCD4796
12	FORMAT (1H0,12HERROR IN SYG)	ABCD4797
	END	ABCD4798

Subroutine THCOMP

	SUBROUTINE THCOMP (PR,ETA,T,H,S,P,TO,HO,SO,PO)	ABCD4799
	IMPLICIT REAL*8 (A-H,O-Z)	ABCD4800
	LOGICAL SI	ABCD4801
	COMMON /COMALL/ COM(1062)	ABCD4802
	EQUIVALENCE (TOLALL, COM(23)), (SI, COM(1055))	ABCD4803
	CPG = .25D0	ABCD4804
	IF (SI) CPG = 1048.0D0	ABCD4805
	PO = P * PR	ABCD4806
	TP = T * PR ** 0.28572D0	ABCD4807
	DO 1 I = 1,25	ABCD4808
	CALL THERMO (PO,HP,TP,SP,X1,0,X2,0)	ABCD4809
	DELS = SP - S	ABCD4810
	IF (DABS(DELS) .LE. .05D0 * TOLALL * S) GO TO 2	ABCD4811
1	TP = TP / DEXP(DELS / CPG)	ABCD4812
	CALL ERROR	ABCD4813
2	HO = H + ((HP - H) / ETA)	ABCD4814
	CALL THERMO (PO,HO,TO,SO,X1,0,X2,1)	ABCD4815
	RETURN	ABCD4816
	END	ABCD4817

Subroutine THERMO

	SUBROUTINE THERMO (PX,HX,FX,SX,AMX,L,FAR,K)	ABCD4818
	IMPLICIT REAL*8 (A-H,O-Z)	ABCD4819
	LOGICAL SI	ABCD4820
	COMMON /COMALL/ COM(1062)	ABCD4821
	EQUIVALENCE (TOLALL, COM(23)), (SI, COM(1055))	ABCD4822
	IF (SI) GO TO 100	ABCD4823
	DEM = 1.986375D0	ABCD4824
	CPG = .25D0	ABCD4825
	PSTD = 1.0D0	ABCD4826
	GO TO 101	ABCD4827
100	DEM = 8316.41D0	ABCD4828
	CPG = 1048.0D0	ABCD4829
	PSTD = 101325.0D0	ABCD4830
101	FX = 0.0D0	ABCD4831
	IF (L .EQ. 1) FX = FAR	ABCD4832
	IF (K .EQ. 1) GO TO 1	ABCD4833
	CALL PROCOM (FX,FX,CS,AK,CP,P,PHI,HX)	ABCD4834
	GO TO 3	ABCD4835
1	TX = HX / CPG	ABCD4836
	DO 2 I = 1,50	ABCD4837
	CALL PROCOM (FX,FX,CS,AK,CP,P,PHI,H)	ABCD4838
	DELH = HX - H	ABCD4839
	IF (DABS(DELH) .LE. .01D0 * TOLALL * HX) GO TO 3	ABCD4840
2	TX = TX + DELH / CPG	ABCD4841
	WRITE (8,4)	ABCD4842

3	SX = PHI - R * DLOG(PX / PSTD)	ABCD4843
	AMX = DEM / R	ABCD4844
	RETURN	ABCD4845
C		ABCD4846
C		ABCD4847
4	FORMAT (31HONO CONVERGENCE IN THERMO\$\$\$\$\$)	ABCD4848
	END	ABCD4849

Subroutine THTURB

	SUBROUTINE THTURB (DH,ETA,FAR,H,S,P,TO,HO,SO,PO)	ABCD4850
	IMPLICIT REAL*8 (A-H,O-Z)	ABCD4851
	LOGICAL SI	ABCD4852
	COMMON /COMALL/ COM(1062)	ABCD4853
	EQUIVALENCE (TOLALL, COM(23)), (SI, COM(1055))	ABCD4854
	DEM = 1.986375D0	ABCD4855
	IF (SI) DEM = 8316.41D0	ABCD4856
	HO = H - DH	ABCD4857
	HOP = H - DH / ETA	ABCD4858
	PT = P / 2.0D0	ABCD4859
	DO 1 I = 1,25	ABCD4860
	CALL THERMO (PT,HOP,TT,ST,AMWT,1,FAR,1)	ABCD4861
	DELS = ST - S	ABCD4862
	IF (DABS(DELS) .LE. .05D0 * TOLALL * S) GO TO 2	ABCD4863
1	PT = P * DEXP(DELS * AMWT / DEM + DLOG(PT / P))	ABCD4864
	CALL ERROR	ABCD4865
2	PO = PT	ABCD4866
	CALL THERMO (PO,HO,TO,SO,X1,1,FAR,1)	ABCD4867
	RETURN	ABCD4868
	END	ABCD4869

Subroutine WDUCTI

	SUBROUTINE WDUCTI	ABCD4870
	IMPLICIT REAL*8 (A-H,O-Z)	ABCD4871
	LOGICAL SI	ABCD4872
	COMMON /COMALL/ COM(1062)	ABCD4873
	DIMENSION WORD(2), ERR(9)	ABCD4874
	DIMENSION Q(9), XZERO(25), AWORD(2)	ABCD4875
	EQUIVALENCE (WORD(1), COM(1)), (IDES, COM(3)), (IDSHOC, COM(15)),	ABCD4876
1	(TOLALL, COM(23)), (EPR(1), COM(24)), (P1, COM(33)), (WAC,	ABCD4877
2	COM(191)), (WG37, COM(210)), (XZERO(1), COM(210)), (A38,	ABCD4878
3	COM(211)), (AM38, COM(212)), (V38, COM(213)), (T38, COM(214)),	ABCD4879
4	(H38, COM(215)), (P38, COM(216)), (TS38, COM(217)),	ABCD4880
5	(PS38, COM(218)), (A39, COM(219)), (AM39, COM(220)),	ABCD4881
6	(V39, COM(221)), (T39, COM(222)), (H39, COM(223)),	ABCD4882
7	(P39, COM(224)), (TS39, COM(225)), (PS39, COM(226)),	ABCD4883
8	(WA32DS, COM(227)), (DPWING, COM(228)), (BPRINT, COM(229)),	ABCD4884
9	(DPWGDS, COM(235)), (T21, COM(263)), (H21, COM(264)),	ABCD4885
1	(WA32, COM(271)), (PCBLID, COM(305)), (P21, COM(377)),	ABCD4886
2	(P37, COM(393)), (U37, COM(394)), (VWDUCT, COM(404)),	ABCD4887
3	(SI, COM(1055))	ABCD4888
	DATA AWORD /4HWDUC, 4HTI /	ABCD4889
	WORD(1) = AWORD(1)	ABCD4890

	WORD(2) = AWORD(2)	ABCD4891
	IF (SI) GO TO 100	ABCD4892
	RA = .0252D0	ABCD4893
	AJ = 2.719D0	ABCD4894
	GO TO 101	ABCD4895
100	RA = 286.9D0	ABCD4896
	AJ = 1.0D0	ABCD4897
101	IF (PCBLID .GT. 0.0D0) GO TO 3	ABCD4898
	DO 1 I = 1,25	ABCD4899
1	XZERO(I) = 0.0D0	ABCD4900
	RETURN	ABCD4901
3	P32 = P21	ABCD4902
	H32 = H21	ABCD4903
	T32 = T21	ABCD4904
	BPRINT = WA32 / WAC	ABCD4905
	WA32C = WA32 * DSQRT(T32) / P32	ABCD4906
	IF (IDES .EQ. 1) WA32DS = WA32C	ABCD4907
	DPWING = DPWGDS * WA32C / WA32DS	ABCD4908
	DPWING = DMIN1(1.0D0,DPWING)	ABCD4909
	P36 = P32 * (1.0D0 - DPWING)	ABCD4910
	T36 = T32	ABCD4911
	H36 = H32	ABCD4912
	CALL THERMO (P36,H36,T36,S36,XX2,1,0.0D0,0)	ABCD4913
	WG37 = WA32	ABCD4914
	T37 = T36	ABCD4915
	P37 = P36	ABCD4916
	H37 = H36	ABCD4917
	S37 = S36	ABCD4918
	IF (VWDUCT .EQ. 0.0D0) GO TO 21	ABCD4919
	Q(2) = 0.0D0	ABCD4920
	Q(3) = 0.0D0	ABCD4921
	WG37P = WG37	ABCD4922
	H37P = H37	ABCD4923
	P37DOT = DERIV(22,P37)	ABCD4924
18	CALL THERMO (P37,H37,T37,S37,XX2,1,0.0D0,0)	ABCD4925
	WG37 = WG37P - P37DOT * VWDUCT / T37 / 1.4D0 / RA	ABCD4926
	U37 = H37 - RA * AJ * T37	ABCD4927
	U37DOT = DERIV(23,U37)	ABCD4928
	H37X = (WG37P * H37P - (WG37P - WG37) * U37 - U37DOT * P37 *	ABCD4929
	1 VWDUCT / T37 / RA) / WG37	ABCD4930
	ERRW = (H37 - H37X) / H37	ABCD4931
	DIR = DSQRT(DABS(H37 / H37X))	ABCD4932
	CALL AFQUIR (Q(1),T37,ERRW,0.0D0,20.0D0,.1D0*TOLALL,DIR,T37T,IGO)	ABCD4933
	GO TO (19,21,20), IGO	ABCD4934
19	T37 = T37T	ABCD4935
	GO TO 18	ABCD4936
20	CALL ERROR	ABCD4937
21	CALL CONVRG (T37,H37,P37,S37,0.0D0,WG37,P1,IDES,A38,P38R,T38,H38,	ABCD4938
	1 P38,S38,TS38,PS38,V38,AM38,ICON)	ABCD4939
	GO TO (5,5,5,4), ICON	ABCD4940
4	CALL ERROR	ABCD4941
5	T39 = T38	ABCD4942
	H39 = H38	ABCD4943
	P39 = P38	ABCD4944

```

TS39 = TS38
V39 = V38
AM39 = AM38
A39 = A38
PS39 = PS38
IDSHOC = ICON + 3
ERR(7) = (P38R - P38) / P38R
IF (IDES .EQ. 1) WRITE (6,6) A38,AM38,A39,AM39
RETURN

```

```

ABCD4945
ABCD4946
ABCD4947
ABCD4948
ABCD4949
ABCD4950
ABCD4951
ABCD4952
ABCD4953
ABCD4954
ABCD4955
ABCD4956
ABCD4957
ABCD4958

```

C
C
6

```

FORMAT (18H0INTER DUCT DESIGN,5X,8H      A38=,E15.8,8H      AM38=,
1 E15.8,8H      A39=,E15.8,8H      AM39=,E15.8)
END

```

Subroutine ZERO

```

SUBROUTINE ZERO
IMPLICIT REAL*8 (A-H,O-Z)
COMMON /COMALL/ COM(1062)
EQUIVALENCE (IDES, COM(3)), (JDES, COM(4)), (INIT, COM(7)),
1 (IDBURN, COM(11)), (IAFTBN, COM(12)), (IDSHOC, COM(15)),
2 (IMSHOC, COM(16)), (NOZFLT, COM(17))
IDES = 0
JDES = 0
INIT = 0
IDBURN = 0
IAFTBN = 0
IDSHOC = 3
IMSHOC = 3
NOZFLT = 0
COM(33) = 0.0D0
DO 5 I = 37,90
IF (I .EQ. 41 .OR. I .EQ. 50 .OR. I .EQ. 51) GO TO 5
IF (I .EQ. 60 .OR. I .EQ. 61 .OR. I .EQ. 75) GO TO 5
COM(I) = 0.0D0
5 CONTINUE
COM(94) = 0.0D0
COM(95) = 0.0D0
COM(99) = 0.0D0
DO 6 I = 102,113
IF (I .EQ. 107 .OR. I .EQ. 109 .OR. I .EQ. 110) GO TO 6
COM(I) = 0.0D0
6 CONTINUE
DO 7 I = 131,135
IF (I .EQ. 133) GO TO 7
COM(I) = 0.0D0
7 CONTINUE
DO 8 I = 149,160
IF (I .EQ. 155 .OR. I .EQ. 156) GO TO 8
COM(I) = 0.0D0
8 CONTINUE
DO 9 I = 171,174
COM(I) = 0.0D0
9

```

```

ABCD4959
ABCD4960
ABCD4961
ABCD4962
ABCD4963
ABCD4964
ABCD4965
ABCD4966
ABCD4967
ABCD4968
ABCD4969
ABCD4970
ABCD4971
ABCD4972
ABCD4973
ABCD4974
ABCD4975
ABCD4976
ABCD4977
ABCD4978
ABCD4979
ABCD4980
ABCD4981
ABCD4982
ABCD4983
ABCD4984
ABCD4985
ABCD4986
ABCD4987
ABCD4988
ABCD4989
ABCD4990
ABCD4991
ABCD4992
ABCD4993
ABCD4994
ABCD4995

```

	DO 10 I = 190,209	ABCD4996
	IF (I .EQ. 192 .OR. (I .GE. 195 .AND. I .LE. 197) .OR. I .EQ. 199)	ABCD4997
	1 GO TO 10	ABCD4998
	COM(I) = 0.0D0	ABCD4999
10	CONTINUE	ABCD5000
	DO 11 I = 242,258	ABCD5001
	IF (I .EQ. 244) GO TO 11	ABCD5002
	COM(I) = 0.0D0	ABCD5003
11	CONTINUE	ABCD5004
	DO 12 I = 263,265	ABCD5005
12	COM(I) = 0.0D0	ABCD5006
	DO 13 I = 270,274	ABCD5007
	IF (I .EQ. 271) GO TO 13	ABCD5008
	COM(I) = 0.0D0	ABCD5009
13	CONTINUE	ABCD5010
	DO 14 I = 290,293	ABCD5011
14	COM(I) = 0.0D0	ABCD5012
	DO 15 I = 306,320	ABCD5013
	IF ((I .GE. 309 .AND. I .LE. 312) .OR. I .EQ. 314) GO TO 15	ABCD5014
	COM(I) = 0.0D0	ABCD5015
15	CONTINUE	ABCD5016
	DO 16 I = 321,355	ABCD5017
	IF (I .EQ. 325 .OR. I .EQ. 326 .OR. I .EQ. 328) GO TO 16	ABCD5018
	IF (I .EQ. 329 .OR. I .EQ. 336 .OR. I .EQ. 341) GO TO 16	ABCD5019
	IF (I .EQ. 342 .OR. I .EQ. 346 .OR. I .EQ. 347) GO TO 16	ABCD5020
	COM(I) = 0.0D0	ABCD5021
15	CONTINUE	ABCD5022
	DO 17 I = 358,371	ABCD5023
	IF (I .EQ. 366 .OR. I .EQ. 367 .OR. I .EQ. 370) GO TO 17	ABCD5024
	COM(I) = 0.0D0	ABCD5025
17	CONTINUE	ABCD5026
	CALL SYG (1)	ABCD5027
	RETURN	ABCD5028
	END	ABCD5029

APPENDIX C

SAMPLE CASE INPUT AND OUTPUT

PCNF
CNF
ZF
PRF
WAF
WAF
PCNC
CNC
ZC
PRC
WACC
WAC
T2
P2
T21
P21
T3
P3
PCBLF
BLF
PCBLC
BLC
PCBLOB
BLOB
PCBLHP
BLHP
PCBLLP
BLLP
T4
P4
WA3
WFB
WG4
FAR4
ETAB
DPCOM
TFFHP
CNHP
DHTCHP
DHTC
T5
P5
TFFLP
CNLP
DHTCLP
DHTF
T55
P55
PCBLDU
BLDU
T24
P24
T25
P25

WAD
 WFD
 WG24
 FAR24
 ETAD
 DPDUC
 ETAF
 ETAC
 ETATHP
 ETATLP
 AM55
 AM25
 T6
 P6
 PS6
 AM6
 V6
 WG6
 T7
 WFA
 WG7
 FAR7
 ETAA
 DPAFT
 PS8
 AM8
 V8
 PS9
 AM9
 V9
 PS28
 AM28
 V28
 PS29
 AM29
 V29
 BYPASS
 HPEXT
 WFT
 WGT
 VA
 FRD
 CVMNOZ
 VJM
 CVDNOZ
 VJD
 FGM
 FGP
 THEEND
 \$DATAIN ISPOOL=2,FAN=.TRUE.,SI=.FALSE.,IDES=1,MODE=0,IDUMP=1,IAMTP=0,
 IGASMX=2,ITRYS=200,FXFN2M=.FALSE.,FXM2CP=.FALSE.,AFTFAN=.FALSE.,
 DUMSPL=.TRUE.,TOLALL=.0001,DELFG=1.0,DELFN=1.0,DELSFC=1.0,PCNFDS=102.31,
 PRFDS=2.996,ETAFFDS=.8499,PCNCDS=98.73,PRCDS=8.462,ETACDS=.8136,T4DS=2892.04,
 ETABDS=1.00,DPCODS=.0561,ETHPDS=.8713,ETLPDS=.9021,DPDUDS=.0584,T7DS=3583.6,

ETAADS=.8430,DPAFDS=.0599,AM55=.283,AM6=.243,CVMNOZ=.9494,WAFCDs=221.573,
WACCDs=54.988,HPEXT=0.0,AM=0.0,ALTP=0.0,PCBLF=0.0,PCBLC=.16,PCBLDU=.208,
PCBLOB=0.0,PCBLHP=.726,PCBLLP=.066,AM23=.170,ZFDS=.8333,ZCDS=.8143,
TFHPDS=50.0,CNHPDS=2.0,TFLPDS=130.0,CNLPDS=2.3,XNHPDS=10070.,XNLPDS=9651.,
PMIHP=3.80,PMILP=4.50,VFAN=2.31,VCOMP=1.65,VCOMB=1.65,VHPTRB=.505,
VLPTRB=.618,VAFTBN=49.77,VFDUCT=10.08 &END
\$DATAIN MODE=2,WFB=2.75,ITRAN=0,IDES=0 &END
\$DATAIN MODE=2,WFB=2.75,ITRAN=1,IAMTRX=1 &END

PAN DESIGN PRFCF= 0.47523476E 01 ETAPCF= 0.98548257E 00 WAPCF= 0.35527831E 00 T2DS= 0.51865992E 03
 MIDDLE SPOOL DESIGN PFICF= 0.10000000E 01 ETACF= 0.10000000E 01 WAICF= 0.10000000E 01 T22DS= 0.74215402E 03
 COMPRESSOR DESIGN PFCCF= 0.10922125E 01 ETACCF= 0.95051735E 00 WACCF= 0.56173771E 00 T21DS= 0.74296402E 03
 COMBUSTOR DESIGN WA3CDS= 0.11338571E 02 ETABCF= 0.10000000E 01
 H.P. TURBINE DESIGN CNHPCF= 0.91021469E 00 TFHPCF= 0.27621708E 01 ETHPCF= 0.96811114E 00 DHHPCF= 0.12239288E 01
 L.P. TURBINE DESIGN CNLPCF= 0.10310318E 01 TFLPCF= 0.17567140E 01 ETLPCF= 0.10225143E 01 DHLPCF= 0.24622325E 01
 TURBINE/DUCT AREA DESIGN A55= 0.41817585E 01 AM55= 0.29335887E 00 A25= 0.12855634E 01 AM25= 0.38353284E 00
 AFTERBURNER DESIGN AREA A6 6.943
 NOZZLE DESIGN A8= 0.29437834E 01 AM8= 0.10000000E 01 A9= 0.29437884E 01 AM9= 0.10000000E 01
 OUTPUT AM= 0.000 ALTP= 0. T4= 2892.04 ETAR= 1.0000

MIDDLE SPOOL IS DUMMY

NO AIRFLOW INTO WING
 THE OUTPUT IS IN ENGLISH UNITS

PCNF 0.102310E 03	CNF 0.102310E 01	ZF 0.833300E 00	PRF 0.299600E 01	WAPC 0.221573E 03	WAP 0.221573E 03
PCNC 0.119165E 03	CNC 0.997300E 00	ZC 0.814300E 00	PRC 0.846200E 01	WACC 0.549880E 02	WAC 0.137543E 03
T2 0.518670E 03	P2 0.100000E 01	T21 0.742964E 03	P21 0.299600E 01	T3 0.145753E 04	P3 0.253522E 02
PCBLF 0.000000	BLF 0.000000	PCBLC 0.160000E 00	BLC 0.220237E 02	PCBLCB 0.000000	BLCB 0.000000
PCBLHP 0.726000E 00	BLHP 0.159892E 02	PCBLLP 0.660000E-01	RLLP 0.145357E 01	T4 0.239204E 04	P4 0.239293E 02
WA3 0.115624E 03	WFB 0.274976E 01	WGH 0.118374E 03	PARH 0.237819E-01	ETAB 0.100000E 01	DPCOM 0.561000E-01
TFHHP 0.500000E 02	CNHP 0.200000E 01	DHTCHP 0.734297E-01	DHTC 0.212362E 03	T5 0.210382E 04	P5 0.566634E 01
TFFLP 0.130000E 03	CNLP 0.230000E 01	DHTCLP 0.422988E-01	DHTF 0.889511E 02	P55 0.178909E 04	P55 0.259704E 01
PCBLDU 0.208000E 00	BLDU 0.458093E 01	T24 0.781926E 03	P24 0.232103E 01	P25 0.781926E 03	P25 0.292103E 01
WAD 0.885053E 02	WPD 0.000000	W32H 0.885053E 02	PAR2H 0.000000	ETAD 0.000000	DPDHC 0.584000E-01
ETAP 0.849900E 00	ETAC 0.813600E 00	ETAPHP 0.871300E 00	ETATLP 0.902100E 00	AM55 0.293359E 00	AM25 0.383683E 00
T6 0.141349E 04	P6 0.271359E 01	P56 0.260928E 01	AM6 0.243000E 00	V5 0.437209E 03	W36 0.224322E 03

T7 0.141349E 00	WPA 0.000000	WG7 0.224322E 03	FAR7 0.124102E-01	ETAA 0.000000	DPAFT 0.599000E-01
PS8 0.137620E 01	AM8 0.100000E 01	V8 0.167416E 04	PS9 0.137620E 01	AM9 0.100000E 01	V9 0.157415E 04
PS28 0.000000	AM28 0.000000	V28 0.000000	PS29 0.000000	AM29 0.000000	V29 0.000000
BYPASS 0.609702E 00	HDEXT 0.000000	WPT 0.274975E 01	WST 0.224322E 03	VA 0.000000	PRD 0.000000
CVMNQZ 0.949400E 00	VJM 0.158944E 04	CVDNQZ 0.000000	VJD 0.000000	FGM 0.110319E 05	F3P 0.234760E 04

MAIN SONIC CONVERGENT NOZZLE

PG= 13429.44

PN= 13429.44

SFC= 0.73712

CONVERGED AFTER 1 LOOPS

COMMON	0.833300E 00	0.112310E 03	0.571429E 00	0.100000E 01	0.814300E 00	0.118165E 03	0.239204E 0
0.100000E 01	0.177859E 03	0.170000E 00	0.826058E 03	0.781926E 03	0.299600E 01	0.197312E 03	0.161458E 0
0.254881E 01	0.781926E 03	0.187311E 03	0.161871E 01	0.383683E 00	0.731926E 03	0.282103E 01	0.187311E 0
0.161871E 01	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000
0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000
0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000
0.000000	0.584000E-01	0.534000E-01	0.100000E 01	0.885053E 02	0.000000	0.791925E 03	0.232103E 0
0.187311E 03	0.161871E 01	0.135817E 03	0.206645E-01	0.178909E 04	0.258794E 01	0.457067E 03	0.184187E 0
0.274976E 01	0.000000	0.518670E 03	0.518670E 03	0.100000E 01	0.123918E 03	0.159103E 01	0.160218E 0
0.742964E 03	0.128557E 01	0.517369E 03	0.289204E 04	0.289204E 04	0.210342E 04	0.547054E 03	0.183735E 0
0.134363E 03	0.208927E-01	0.283359E 00	0.567671E 03	0.418175E 01	0.254984E 01	0.177375E 01	0.260828E 0
0.437208E 03	0.276217E 01	0.910215E 00	0.968111E 00	0.122383E 01	0.500000E 02	0.209000E 01	0.371300E 0
0.475235E 01	0.985483E 00	0.356278E 00	0.102310E 03	0.299600E 01	0.849900E 00	0.221573E 03	0.000000
0.000000	0.549880E 02	0.239600E 01	0.849900E 00	0.814300E 00	0.102310E 01	0.221573E 03	0.833300E 0
0.102310E 03	0.000000	0.571429E 00	0.100000E 01	0.000000	0.000000	0.000000	0.000000
0.000000	0.750000E 00	0.100000E 03	0.000000	0.518670E 03	0.123918E 03	0.159103E 01	0.146753E 0
0.360485E 03	0.115624E 03	0.113895E 02	0.289204E 04	0.784627E 03	0.183459E 01	0.118374E 03	0.237313E-0
0.210342E 04	0.547064E 03	0.133705E 01	0.134363E 03	0.208927E-01	0.726000E 00	0.000000	0.550000E-0
0.208000E 00	0.000000	0.200000E 01	0.871300E 00	0.734297E-01	0.212352E 03	0.500000E 02	0.100000E 0
0.100000E 01	0.100000E 01	0.100000E 01	0.150000E 01	0.100000E 01	0.137648E 03	0.549880E 02	0.100000E 0
0.274976E 01	0.833300E 00	0.100000E 01	0.100000E 01	0.100000E 01	0.100000E 01	0.137648E 03	0.274976E 0
0.220237E 02	0.111699E 04	0.000000	0.000000	0.561000E-01	0.561000E-01	0.102310E 03	0.100000E 0
0.742964E 03	0.299600E 01	0.177859E 03	0.160218E 01	0.360485E 03	0.221573E 03	0.137648E 03	0.000000
0.458093E 01	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000
0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000
0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000
0.134294E 05	0.000000	0.000000	0.100000E 01	0.100000E 01	0.100000E 01	0.000000	0.000000
0.949400E 00	0.000000	0.000000	0.000000	0.158944E 04	0.274976E 01	0.224322E 03	0.737123E 0
0.124102E-01	0.000000	0.000000	0.110818E 05	0.000000	0.234760E 04	0.110818E 05	0.234760E 0
0.134294E 05	0.134294E 05	0.000000	0.100000E 01	0.100000E 01	0.100000E 01	0.742954E 03	0.177359E 0
0.160218E 01	0.137648E 03	0.742964E 03	0.742964E 03	0.137648E 03	0.152547E 01	0.000000	0.178909E 0
0.457067E 03	0.184187E 01	0.130000E 03	0.230000E 01	0.902100E 00	0.000000	0.000000	0.000000
0.175671E 01	0.103103E 01	0.102251E 01	0.246223E 01	0.000000	0.000000	0.000000	0.000000
0.130000E 03	0.230000E 01	0.902100E 00	0.422888E-01	0.889511E 02	0.109221E 01	0.950517E 00	0.561738E 0
0.846200E 01	0.813600E 00	0.137648E 03	0.814300E 00	0.118165E 03	0.160000E 00	0.987300E 02	0.000000
0.000000	0.987300E 00	0.846200E 01	0.813600E 00	0.000000	0.000000	0.137648E 03	0.000000
0.159392E 02	0.000000	0.145357E 01	0.000000	0.458093E 01	0.000000	0.221573E 03	0.549390E 0
0.885053E 02	0.000000	0.135817E 03	0.206645E-01	0.398790E 02	0.243000E 00	0.243000E 00	0.594234E 0
0.310795E 04	0.224322E 03	0.141349E 04	0.271359E 01	0.350635E 03	0.224322E 03	0.124102E-01	0.463560E-0
0.139714E 04	0.243842E 01	0.455903E 03	0.259681E 00	0.694294E 01	0.358360E 04	0.141349E 04	0.350636E 0
0.177798E 01	0.294879E 01	0.000000	0.120059E 04	0.137620E 01	0.157415E 04	0.100000E 01	0.141349E 0
0.255105E 01	0.350636E 03	0.177798E 01	0.294879E 01	0.000000	0.120059E 04	0.137620E 01	0.167416E 0
0.100000E 01	0.141349E 04	0.255105E 01	0.350636E 03	0.177798E 01	0.843000E 00	0.599000E-01	0.000000
0.000000	0.843000E 00	0.599000E-01	0.118992E 05	0.000000	0.987395E 04	0.299600E 01	0.126952E 0
0.299600E 01	0.000000	0.253522E 02	0.259932E 03	0.239299E 02	0.586467E 03	0.556534E 01	0.000000
0.566534E 01	0.000000	0.268794E 01	0.334481E 03	0.255105E 01	0.253785E 03	0.282103E 01	0.133735E 0
0.000000	0.000000						
0.514756E-84	0.000000	0.000000	0.000000	0.514756E-84			

OUTPUT AM= 0.000 ALT= 0. T4= 2892.13 ETAR= 1.0000

MIDDLE SPOOL IS DUMMY

NO AIRFLOW INTO WING
THE OUTPUT IS IN ENGLISH UNITS

PCNF 0.102310E 03	CNF 0.102310E 01	ZP 0.913378E 00	PRF 0.299619E 01	WAPC 0.221553E 03	WAP 0.221553E 03
PCNC 0.113165E 03	CNC 0.997289E 00	ZC 0.814304E 00	PRC 0.846187E 01	WACC 0.549970E 02	WAC 0.137553E 03
T2 0.518670E 03	P2 0.100000E 01	T21 0.742991E 03	P21 0.299619E 01	T3 0.146756E 04	P3 0.253533E 02
PCBLP 0.000000	BLP 0.000000	PCBLC 0.160000E 00	BLC 0.220244E 02	PCBLCB 0.000000	BLCB 0.000000
PCBLHP 0.725000E 00	FLHP 0.159897E 02	PCBLLP 0.650000E-01	BLLP 0.145361E 01	T4 0.299213E 04	P4 0.239313E 02
WA3 0.115628E 03	WPB 0.275000E 01	WG4 0.118378E 03	FAP4 0.237931E-01	ETAB 0.100000E 01	DPCCM 0.560995E-01
TFFHP 0.500001E 02	CNHP 0.199997E 01	DHTCHP 0.734333E-01	DHTC 0.212365E 03	T5 0.210350E 04	P5 0.566568E 01
TFFLP 0.130000E 03	CNLP 0.229996E 01	DHTCLP 0.422991E-01	DHTF 0.889531E 02	T55 0.179316E 04	P55 0.259313E 01
PCBLDU 0.209000E 00	PLDU 0.458108E 01	T24 0.781949E 03	P24 0.282123E 01	T25 0.791949E 03	P25 0.232123E 01
WAD 0.884967E 02	WPD 0.000000	WG24 0.884967E 02	FAR24 0.000000	ETAD 0.000000	DPDUC 0.583915E-01
ETAF 0.849891E 00	ETAC 0.813597E 00	ETATHP 0.871292E 00	ETATLP 0.902100E 00	AM55 0.283247E 00	AM25 0.393563E 00
T6 0.141358E 04	P6 0.271363E 01	PS6 0.260914E 01	AM6 0.243014E 00	V6 0.437243E 03	WG6 0.224318E 03
T7 0.141358E 04	WFA 0.000000	WG7 0.224318E 03	FAP7 0.124115E-01	ETAA 0.000000	DPAPT 0.598998E-01
PS8 0.137622E 01	AM8 0.100000E 01	V8 0.167421E 04	PS9 0.137622E 01	AM9 0.100000E 01	V9 0.167421E 04
PS28 0.000000	AM28 0.000000	V28 0.000000	PS29 0.000000	AM29 0.000000	V29 0.000000
RYPASS 0.609619E 00	HPEXT 0.000000	WPT 0.275000E 01	WGT 0.224318E 03	VA 0.000000	FRD 0.000000
CVVNOZ 0.949400E 00	VJM 0.158949E 04	CVDNOZ 0.000000	VJD 0.000000	FGM 0.110320E 05	FGP 0.234772E 04

MAIN SONIC CONVERGENT NOZZLE

FG= 13429.68

FN= 13429.53

SFC= 0.73717

CONVERGED AFTER 44 LOOPS

THIS IS THE S.S. SOLUTION
1.1899E 04 9.8740E 03 1.3374E 02 2.5511E 00 2.5380E 02 2.5994E 02 2.5353E 01 5.8549E 02 2.3212E 00 1.2695E 02
4.0296E 02 3.3450E 02 5.6667E 00 2.3931E 01 2.9962E 00 2.6881E 00
1 THE VARIABLE IS NO. 1
THIS COLUMN OF X =
-7.3171E 01 -3.0739E 01 -3.2766E-01 -1.1803E-02 4.1193E-01 -6.2664E-01 -2.4549E-01 3.1092E 00 -9.3225E-03 -2.3577E-01
2.2132E 00 2.1314E 00 -4.8520E-02 -2.2784E-01 -8.9229E-03 -1.3619E-02
IGIN = 1
THE NEXT TRY FOR PVRDOT = 2.1000E-02
1 THE VARIABLE IS NO. 1
THIS COLUMN OF X =
-7.6818E 01 -3.2274E 01 -3.4394E-01 -1.2393E-02 4.3283E-01 -6.5794E-01 -2.5772E-01 3.2555E 00 -9.7893E-03 -2.1706E-01
2.3252E 00 2.2392E 00 -5.0937E-02 -2.3920E-01 -9.3700E-03 -1.4299E-02
IGIN = 2
THE NEXT TRY FOR PVRDOT = 6.4675E-03
1 THE VARIABLE IS NO. 1
THIS COLUMN OF X =
-2.3305E 01 -9.7902E 00 -1.0484E-01 -3.8113E-03 1.2784E-01 -2.0025E-01 -7.8123E-02 9.9134E-01 -2.3705E-03 -5.6122E-02
6.9470E-01 6.6957E-01 -1.5597E-02 -7.2506E-02 -2.8418E-03 -4.4042E-03
IGIN = 3
THE NEXT TRY FOR PVRDOT = 6.5946E-03
1 THE VARIABLE IS NO. 1
THIS COLUMN OF X =
-2.3825E 01 -1.0019E 01 -1.0736E-01 -3.9733E-03 1.3139E-01 -2.0512E-01 -7.9945E-02 1.0033E 00 -3.0451E-03 -6.7770E-02
7.1127E-01 6.8585E-01 -1.5908E-02 -7.4196E-02 -2.9137E-03 -4.4701E-03
IGIN = 0
THE NEXT TRY FOR PVRDOT = 6.5946E-03
2 THE VARIABLE IS NO. 3
THIS COLUMN OF X =
1.8782E 01 -2.0343E 01 -1.6850E-01 -7.1504E-03 7.8330E-02 -1.8911E-01 1.3975E-02 -4.7353E-01 -1.0910E-02 -2.3541E-01
-4.9248E-01 -5.1828E-01 -8.0747E-03 1.3228E-02 -1.2515E-02 -6.3936E-03
IGIN = 1
THE NEXT TRY FOR PVRDOT = 2.1000E-02
2 THE VARIABLE IS NO. 3
THIS COLUMN OF X =
1.9717E 01 -2.1369E 01 -1.7688E-01 -7.5106E-03 8.2510E-02 -1.9845E-01 1.4638E-02 -4.9554E-01 -1.1457E-02 -2.4718E-01
-5.1662E-01 -5.4375E-01 -8.4892E-03 1.3855E-02 -1.3142E-02 -6.7167E-03
IGIN = 2
THE NEXT TRY FOR PVRDOT = 1.9419E-02
2 THE VARIABLE IS NO. 3
THIS COLUMN OF X =
1.9239E 01 -1.9748E 01 -1.6362E-01 -5.9412E-03 7.5908E-02 -1.8368E-01 1.3591E-02 -4.5017E-01 -1.0592E-02 -2.2359E-01
-4.7846E-01 -5.0350E-01 -7.9342E-03 1.2964E-02 -1.2151E-02 -6.2061E-03
IGIN = 0
THE NEXT TRY FOR PVRDOT = 1.9419E-02

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      3 THE VARIABLE IS NO. 21
THIS COLUMN OF X =
  0.0000 -1.8190E-12 -3.1338E-02 -3.0195E-06 -1.2791E-02 -5.5843E-14 -1.0559E-14 5.5943E-14 -9.3819E-15 -3.1974E-14
  1.1369E-13 1.7053E-13 -2.6645E-15 -1.0658E-14 -1.1102E-15 7.5495E-15
IGIN = 1
THE NEXT TRY FOR PVRDOT = 3.0010E-02
      3 THE VARIABLE IS NO. 21
THIS COLUMN OF X =
  0.0000 -1.8190E-12 -4.7036E-02 -4.5319E-06 -1.9198E-02 -5.6943E-14 -1.0658E-14 5.5943E-14 -8.9818E-15 -3.1974E-14
  1.1369E-13 1.7053E-13 -2.6645E-15 -1.0658E-14 -1.1102E-15 7.5495E-15
IGIN = 2
THE NEXT TRY FOR PVRDOT = 6.0020E-02
      3 THE VARIABLE IS NO. 21
THIS COLUMN OF X =
  0.0000 -1.8190E-12 -9.4153E-02 -9.0710E-06 -3.8429E-02 -5.5843E-14 -1.0658E-14 5.5943E-14 -9.3913E-15 -3.1374E-14
  1.1369E-13 1.7053E-13 -2.6645E-15 -1.0559E-14 -1.1102E-15 7.5495E-15
IGIN = 3
THE NEXT TRY FOR PVRDOT = 1.2004E-01
      3 THE VARIABLE IS NO. 21
THIS COLUMN OF X =
  4.0185E-01 3.9502E-01 -1.9268E-01 -2.1106E-04 -9.3159E-02 -5.5546E-07 -2.0421E-04 6.4551E-03 -3.2376E-04 -2.2589E-03
  3.1548E-03 -7.5327E-04 -6.1424E-05 -1.8479E-04 -2.7794E-04 -1.4439E-04
IGIN = 4
THE NEXT TRY FOR PVRDOT = 1.6561E-01
      3 THE VARIABLE IS NO. 21
THIS COLUMN OF X =
  5.3336E-01 5.4212E-01 -2.6585E-01 -3.0777E-04 -1.2829E-01 4.2093E-04 -3.7640E-04 1.1053E-02 -4.4530E-04 -2.7974E-03
  6.1796E-03 6.3404E-06 -9.9338E-05 -3.4170E-04 -3.8156E-04 -2.2155E-04
IGIN = 5
THE NEXT TRY FOR PVRDOT = 1.6662E-01
      3 THE VARIABLE IS NO. 21
THIS COLUMN OF X =
  5.3630E-01 5.4541E-01 -2.6748E-01 -3.0397E-04 -1.2907E-01 4.3032E-04 -3.8023E-04 1.1155E-02 -4.4802E-04 -2.8095E-03
  6.2472E-03 2.3337E-05 -9.9260E-05 -3.4521E-04 -3.8387E-04 -2.2332E-04
IGIN = 0
THE NEXT TRY FOR PVRDOT = 1.6562E-01
      4 THE VARIABLE IS NO. 18
THIS COLUMN OF X =
  4.8549E-01 5.9564E-01 -8.0090E-04 -3.0337E-04 -4.2444E-03 4.5776E-03 6.9387E-04 -3.9955E-03 -1.4725E-04 5.3672E-04
  -7.1111E-03 -1.4450E-02 -1.4293E-04 5.4181E-04 -1.0061E-04 -3.3633E-04
IGIN = 1
THE NEXT TRY FOR PVRDOT = 2.1000E-02
      4 THE VARIABLE IS NO. 18
THIS COLUMN OF X =
  5.0691E-01 6.1446E-01 -8.0422E-04 -3.2066E-04 -4.4055E-03 4.9619E-03 7.1635E-04 -3.9158E-03 -1.5436E-04 7.1102E-04
  -7.2232E-03 -1.5036E-02 -1.5185E-04 5.6260E-04 -1.0532E-04 -3.5605E-04
IGIN = 2
THE NEXT TRY FOR PVRDOT = 2.9749E-01

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4 THE VARIABLE IS NO. 18
THIS COLUMN OF X =
7.4853E 00 7.6371E 00 -1.1174E-02 -1.6389E-03 -2.9016E-02 7.0791E-02 7.0036E-03 -1.1935E-02 -2.7414E-03 3.9188E-03
-6.7440E-02 -1.7154E-01 -3.2351E-03 6.4545E-03 -2.1053E-03 -5.1110E-03
IGIN = 3
THE NEXT TRY FOR PVRDOT = 3.2296E-01
4 THE VARIABLE IS NO. 18
THIS COLUMN OF X =
8.1189E 00 8.2885E 00 -1.2105E-02 -5.1039E-03 -3.1395E-02 7.6857E-02 7.5681E-03 -1.2485E-02 -2.3770E-03 9.6040E-03
-7.2774E-02 -1.8588E-01 -3.5186E-03 6.9745E-03 -2.2865E-03 -5.5522E-03
IGIN = 0
THE NEXT TRY FOR PVRDOT = 3.2296E-01
5 THE VARIABLE IS NO. 19
THIS COLUMN OF X =
2.9764E-01 3.3295E-01 -7.7204E-04 -1.5171E-04 -7.1944E-02 2.0837E-03 4.9677E-04 -4.6943E-03 -9.5005E-05 -1.5115E-05
-6.0843E-03 -9.3137E-03 -6.4744E-05 4.5946E-04 -5.9319E-05 -1.5342E-04
IGIN = 1
THE NEXT TRY FOR PVRDOT = 2.1000E-02
5 THE VARIABLE IS NO. 19
THIS COLUMN OF X =
3.0968E-01 3.4915E-01 -7.7388E-04 -1.5143E-04 -7.5492E-02 2.2435E-03 5.0940E-04 -4.6495E-03 -8.3995E-05 2.6675E-05
-6.1501E-03 -9.6429E-03 -6.9755E-05 4.7114E-04 -6.1965E-05 -1.7450E-04
IGIN = 2
THE NEXT TRY FOR PVRDOT = 1.4280E-01
5 THE VARIABLE IS NO. 19
THIS COLUMN OF X =
2.0673E 00 2.0963E 00 -3.3099E-03 -1.2482E-03 -5.0414E-01 1.8802E-02 2.1195E-03 -7.6445E-03 -7.3376E-04 2.0611E-03
-2.2128E-02 -4.9459E-02 -8.2344E-04 1.9540E-03 -5.6105E-04 -1.3538E-03
IGIN = 3
THE NEXT TRY FOR PVRDOT = 1.4378E-01
5 THE VARIABLE IS NO. 19
THIS COLUMN OF X =
2.0806E 00 2.1100E 00 -3.3360E-03 -1.2569E-03 -5.0760E-01 1.8923E-02 2.1286E-03 -7.6311E-03 -7.3916E-04 2.0739E-03
-2.2217E-02 -4.9741E-02 -8.2946E-04 1.9523E-03 -5.6526E-04 -1.3631E-03
IGIN = 0
THE NEXT TRY FOR PVRDOT = 1.4378E-01
6 THE VARIABLE IS NO. 9
THIS COLUMN OF X =
1.8406E 00 6.6172E-01 5.1501E-03 2.4570E-04 -1.9900E-02 -1.5722E-02 5.1967E-03 -1.0335E-01 1.3953E-04 3.5753E-03
-7.2034E-02 -6.7192E-02 1.1057E-03 4.8496E-03 1.2492E-04 2.9655E-04
IGIN = 1
THE NEXT TRY FOR PVRDOT = 2.1000E-02
6 THE VARIABLE IS NO. 9
THIS COLUMN OF X =
1.9285E 00 6.9367E-01 5.4355E-03 2.5570E-04 -2.0846E-02 -1.6475E-02 5.4387E-03 -1.0876E-01 1.4664E-04 3.7921E-03
-7.5376E-02 -7.0390E-02 1.1584E-03 5.0755E-03 1.3121E-04 3.0843E-04
IGIN = 2
THE NEXT TRY FOR PVRDOT = 6.9021E-01

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6 THE VARIABLE IS NO. 9
THIS COLUMN OF X =
5.4457E 01 2.2088E 01 1.9765E-01 5.8094E-03 -6.5715E-01 -5.1162E-01 1.7537E-01 -3.4958E 00 4.3349E-03 1.4168E-01
-2.4174E 00 -2.2798E 00 3.5173E-02 1.6364E-01 3.8307E-03 8.1555E-03
IGIN = 3
THE NEXT TRY FOR PVRDOT = 7.0137E-01
6 THE VARIABLE IS NO. 9
THIS COLUMN OF X =
6.5490E 01 2.2441E 01 2.0082E-01 5.9177E-03 -6.6760E-01 -5.1973E-01 1.7817E-01 -3.5513E 00 4.4647E-03 1.4395E-01
-2.4557E 00 -2.3159E 00 3.5735E-02 1.6625E-01 3.8914E-03 8.2852E-03
IGIN = 0
THE NEXT TRY FOR PVRDOT = 7.0137E-01
7 THE VARIABLE IS NO. 8
THIS COLUMN OF X =
-7.0654E-01 -6.1130E-01 -6.3327E-03 -2.3381E-04 1.0078E-02 -6.7603E-03 -4.7135E-03 7.1450E-02 -1.3711E-04 -4.1435E-03
4.7439E-02 4.5692E-02 -9.8905E-04 -4.3726E-03 -1.7809E-04 -2.6809E-04
IGIN = 1
THE NEXT TRY FOR PVRDOT = 2.1000E-02
7 THE VARIABLE IS NO. 8
THIS COLUMN OF X =
-7.4542E-01 -6.4280E-01 -6.6548E-03 -2.4621E-04 1.0595E-02 -7.1215E-03 -4.9591E-03 7.5125E-02 -1.3642E-04 -4.3555E-03
4.9915E-02 4.8059E-02 -1.0403E-03 -4.6004E-03 -1.8691E-04 -2.3247E-04
IGIN = 2
THE NEXT TRY FOR PVRDOT = 2.0730E-01
7 THE VARIABLE IS NO. 8
THIS COLUMN OF X =
-9.3066E 00 -7.1411E 00 -7.2577E-02 -2.7067E-03 1.1190E-01 -8.9587E-02 -5.5507E-02 7.8255E-01 -2.3945E-03 -4.5758E-02
5.4264E-01 5.2051E-01 -1.1326E-02 -3.1507E-02 -1.9949E-03 -3.1325E-03
IGIN = 3
THE NEXT TRY FOR PVRDOT = 1.8961E-01
7 THE VARIABLE IS NO. 8
THIS COLUMN OF X =
-9.5012E 00 -6.5277E 00 -6.6355E-02 -2.4745E-03 1.0225E-01 -8.1834E-02 -5.0733E-02 7.1534E-01 -1.3152E-03 -4.2756E-02
4.9592E-01 4.7563E-01 -1.0356E-02 -4.7077E-02 -1.8240E-03 -2.8636E-03
IGIN = 0
THE NEXT TRY FOR PVRDOT = 1.8961E-01
8 THE VARIABLE IS NO. 11
THIS COLUMN OF X =
-3.5174E-01 -2.9757E-01 -4.4384E-03 -1.5810E-04 -1.3499E-02 -9.3136E-03 -2.2992E-03 -2.7042E-02 -1.7015E-04 -3.6535E-03
-1.8618E-02 -1.3897E-02 -4.7123E-04 -1.765E-03 -1.7268E-04 -1.7090E-04
IGIN = 1
THE NEXT TRY FOR PVRDOT = 2.1000E-02
8 THE VARIABLE IS NO. 11
THIS COLUMN OF X =
-3.8259E-01 -3.1296E-01 -4.5602E-03 -1.5704E-04 -1.4181E-02 -9.7882E-03 -2.4205E-03 -2.8349E-02 -1.7843E-04 -3.8476E-03
-1.9495E-02 -1.4561E-02 -4.9692E-04 -2.2912E-03 -1.8106E-04 -1.8089E-04
IGIN = 2
THE NEXT TRY FOR PVRDOT = 9.9727E-01

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      8 THE VARIABLE IS NO. 11
      THIS COLUMN OF X =
-1.9214E 01 -1.4494E 01 -1.9529E-01 -3.2114E-03 -5.8079E-01 -4.2135E-01 -1.1405E-01 -1.0363E 00 -7.7539E-03 -1.5599E-01
-7.1142E-01 -5.3335E-01 -2.3360E-02 -1.0775E-01 -7.8561E-03 -9.1385E-03
      IGIN = 3
      THE NEXT TRY FOR PVRDOT = 9.6865E-01
      8 THE VARIABLE IS NO. 11
      THIS COLUMN OF X =
-2.0750E 01 -1.5653E 01 -2.1079E-01 -3.8548E-03 -6.2668E-01 -4.5485E-01 -1.2315E-01 -1.1725E 00 -8.3774E-03 -1.6926E-01
-7.6735E-01 -5.7521E-01 -2.5219E-02 -1.1635E-01 -8.4824E-03 -9.8655E-03
      IGIN = 0
      THE NEXT TRY FOR PVRDOT = 9.6955E-01
      9 THE VARIABLE IS NO. 20
      THIS COLUMN OF X =
0.0000 -1.8190E-12 8.9617E-03 8.5175E-06 1.4912E-02 -5.5843E-14 -1.0658E-14 5.5843E-14 -8.3313E-15 -3.1374E-14
1.1369E-13 1.7053E-13 -2.6645E-15 -1.3558E-14 -1.1102E-15 7.5495E-15
      IGIN = 1
      THE NEXT TRY FOR PVRDOT = 3.0010E-02
      9 THE VARIABLE IS NO. 20
      THIS COLUMN OF X =
0.0000 -3.6380E-12 9.2855E-03 3.7789E-05 1.9986E-02 -5.2849E-03 -1.1735E-03 7.9125E-03 -2.1449E-04 -3.1190E-03
8.4588E-03 9.9725E-03 3.5079E-07 -1.1116E-03 -1.9962E-04 9.7371E-05
      IGIN = 2
      THE NEXT TRY FOR PVRDOT = 6.0320E-02
      9 THE VARIABLE IS NO. 20
      THIS COLUMN OF X =
5.4729E-01 6.0113E-01 2.3183E-02 -2.9048E-04 2.1840E-02 2.3942E-03 5.5384E-05 5.5545E-03 -3.4451E-04 -1.4055E-03
1.0454E-03 -6.2582E-03 -1.2821E-04 5.5207E-05 -2.8370E-04 -2.9365E-04
      IGIN = 3
      THE NEXT TRY FOR PVRDOT = 1.2866E 00
      9 THE VARIABLE IS NO. 20
      THIS COLUMN OF X =
1.1725E 01 9.8375E 00 4.7984E-01 -5.2927E-03 5.4140E-01 4.7602E-02 -7.9595E-03 2.1043E-01 -8.9429E-03 -4.7408E-02
8.7273E-02 -2.9457E-02 -5.8257E-03 -7.3874E-03 -7.7876E-03 -5.9902E-03
      IGIN = 4
      THE NEXT TRY FOR PVRDOT = 8.1576E-01
      9 THE VARIABLE IS NO. 20
      THIS COLUMN OF X =
7.5117E 00 6.4114E 00 3.0664E-01 -4.0748E-03 3.3765E-01 3.2000E-02 -4.2747E-03 1.2143E-01 -5.5039E-03 -2.9533E-02
4.4781E-02 -3.1347E-02 -3.6815E-03 -3.9566E-03 -4.8658E-03 -3.9246E-03
      IGIN = 5
      THE NEXT TRY FOR PVRDOT = 8.2120E-01
      9 THE VARIABLE IS NO. 20
      THIS COLUMN OF X =
7.6608E 00 6.4536E 00 3.0867E-01 -4.1022E-03 3.3991E-01 3.2221E-02 -4.3089E-03 1.2234E-01 -5.5414E-03 -2.8775E-02
4.5156E-02 -3.1488E-02 -3.7071E-03 -3.9984E-03 -4.8984E-03 -3.9510E-03
      IGIN = 0
      THE NEXT TRY FOR PVRDOT = 8.2120E-01

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10 THE VARIABLE IS NO. 5
THIS COLUMN OF X =
0.0000 -1.8190E-12 -2.6030E-03 1.4415E-04 -3.7263E-04 -5.1384E-03 5.0135E-04 -1.5291E-02 9.9429E-06 -3.0326E-03
-1.2695E-02 -5.2099E-03 1.1571E-05 4.6941E-04 -1.1102E-15 1.8515E-04
IGIN = 1
THE NEXT TRY FOR PVRDOT = 3.0010E-02
10 THE VARIABLE IS NO. 5
THIS COLUMN OF X =
-2.7209E-01 2.8711E-01 -2.6338E-03 1.1297E-04 -6.4521E-03 -5.6752E-03 2.4645E-04 -1.0745E-02 1.0135E-04 -2.0190E-03
-5.6660E-03 -3.8532E-03 2.1621E-04 2.3069E-04 1.1417E-03 1.2241E-04
IGIN = 2
THE NEXT TRY FOR PVRDOT = 2.8510E-02
10 THE VARIABLE IS NO. 5
THIS COLUMN OF X =
-2.5536E-01 2.7342E-01 -2.4997E-03 1.0823E-04 -6.1344E-03 -5.3770E-03 2.4199E-04 -9.5157E-03 9.5847E-05 -1.9207E-03
-5.4644E-03 -3.7201E-03 2.0747E-04 2.2638E-04 1.0827E-04 1.1754E-04
IGIN = 3
THE NEXT TRY FOR PVRDOT = 3.8728E 00
10 THE VARIABLE IS NO. 5
THIS COLUMN OF X =
-4.3430E 01 3.5910E 01 -3.3321E-01 9.7761E-03 -9.3519E-01 -7.4909E-01 1.4317E-02 -1.3103E 00 1.4035E-02 -2.4153E-01
-7.0357E-01 -5.4429E-01 1.8621E-02 1.3924E-02 1.5841E-02 9.1294E-03
IGIN = 4
THE NEXT TRY FOR PVRDOT = 4.0697E 00
10 THE VARIABLE IS NO. 5
THIS COLUMN OF X =
-4.5638E 01 3.7737E 01 -3.5009E-01 1.0274E-02 -9.8253E-01 -7.8717E-01 1.5019E-02 -1.3771E 00 1.4751E-02 -2.5399E-01
-7.3901E-01 -5.7167E-01 1.9568E-02 1.4503E-02 1.6648E-02 9.5942E-03
IGIN = 0
THE NEXT TRY FOR PVRDOT = 4.0597E 00
11 THE VARIABLE IS NO. 13
THIS COLUMN OF X =
0.0000 -1.8190E-12 -3.9080E-14 -2.2204E-16 8.1712E-14 -5.5843E-14 -1.0658E-14 5.5943E-14 -9.3919E-15 -3.1974E-14
1.1369E-13 1.7053E-13 -2.6645E-15 -1.0558E-14 -1.1102E-15 7.5495E-15
IGIN = 1
THE NEXT TRY FOR PVRDOT = 3.0010E-02
11 THE VARIABLE IS NO. 13
THIS COLUMN OF X =
0.0000 -1.8190E-12 -3.9080E-14 -2.2204E-16 8.1712E-14 -5.5843E-14 -1.0658E-14 5.5943E-14 -9.3919E-15 -3.1974E-14
1.1369E-13 1.7053E-13 -2.6645E-15 -1.0558E-14 -1.1102E-15 7.5495E-15
IGIN = 2
THE NEXT TRY FOR PVRDOT = 6.0020E-02
11 THE VARIABLE IS NO. 13
THIS COLUMN OF X =
0.0000 -1.8190E-12 -3.9080E-14 -2.7330E-05 -4.5072E-03 -5.5843E-14 -1.0659E-14 5.5943E-14 -9.3919E-15 -3.1974E-14
-7.7347E-03 -7.5829E-03 -2.6645E-15 -1.0558E-14 -1.1102E-15 -3.7880E-05
IGIN = 3
THE NEXT TRY FOR PVRDOT = 1.2004E-01

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11 THE VARIABLE IS NO. 13
THIS COLUMN OF X =
0.0000 -1.8190E-12 -3.9080E-14 -5.3552E-05 -8.8316E-03 -5.5843E-14 -1.0658E-14 5.5843E-14 -8.8316E-03 -3.9080E-14
-1.5156E-02 -1.4858E-02 -2.6645E-15 -1.0658E-14 -1.1102E-15 -7.4225E-05
IGIN = 4
THE NEXT TRY FOR PVRDOT = 2.4208E-01
11 THE VARIABLE IS NO. 13
THIS COLUMN OF X =
0.0000 -1.8190E-12 -3.9080E-14 -1.0601E-04 -1.7481E-02 -5.5843E-14 -1.0658E-14 5.5843E-14 -8.8316E-03 -3.9080E-14
-2.9999E-02 -2.9411E-02 -2.6645E-15 -1.0658E-14 -1.1102E-15 -1.4693E-04
IGIN = 5
THE NEXT TRY FOR PVRDOT = 4.8016E-01
11 THE VARIABLE IS NO. 13
THIS COLUMN OF X =
0.0000 -3.6380E-12 -4.1595E-03 -1.8593E-04 -3.7174E-02 -5.2849E-03 -1.1735E-03 7.9125E-03 -2.1490E-04 -3.1190E-03
-5.1237E-02 -4.8551E-02 3.5079E-07 -1.1116E-03 -1.9962E-04 -1.9500E-04
IGIN = 6
THE NEXT TRY FOR PVRDOT = 9.6032E-01
11 THE VARIABLE IS NO. 13
THIS COLUMN OF X =
1.0859E 00 -1.8118E-01 -4.6142E-03 -3.3352E-04 -6.9070E-02 -1.9642E-03 1.6783E-03 -2.9232E-02 -3.7441E-04 -5.2295E-03
-1.4873E-01 -1.2969E-01 -3.2917E-04 1.5640E-03 -3.9927E-04 -3.5480E-04
IGIN = 7
THE NEXT TRY FOR PVRDOT = 4.1972E 00
11 THE VARIABLE IS NO. 13
THIS COLUMN OF X =
4.8427E 00 -1.0551E 00 -1.9953E-02 -1.5346E-03 -2.9521E-01 -7.7446E-03 6.5998E-03 -1.1573E-01 -1.7758E-03 -2.7393E-02
-5.4421E-01 -5.5954E-01 -1.7660E-03 6.1499E-03 -1.8968E-03 -1.6174E-03
IGIN = 8
THE NEXT TRY FOR PVRDOT = 5.2535E 00
11 THE VARIABLE IS NO. 13
THIS COLUMN OF X =
5.0222E 00 -1.3477E 00 -2.5029E-02 -1.9348E-03 -3.6885E-01 -9.3468E-03 8.0852E-03 -1.4133E-01 -2.2320E-03 -3.4312E-02
-8.0437E-01 -6.9857E-01 -2.2544E-03 7.5344E-03 -2.3838E-03 -2.0408E-03
IGIN = 0
THE NEXT TRY FOR PVRDOT = 5.2535E 00
12 THE VARIABLE IS NO. 17
THIS COLUMN OF X =
0.0000 -1.8190E-12 -3.9080E-14 -2.2204E-16 8.1712E-14 -5.5843E-14 -1.0658E-14 5.5843E-14 -8.8316E-03 -3.9080E-14
1.1369E-13 1.7053E-13 -2.6645E-15 -1.0658E-14 -1.1102E-15 7.5495E-15
IGIN = 1
THE NEXT TRY FOR PVRDOT = 3.0010E-02
12 THE VARIABLE IS NO. 17
THIS COLUMN OF X =
0.0000 -1.8190E-12 -3.9080E-14 -2.2204E-16 8.1712E-14 -5.5843E-14 -1.0658E-14 5.5843E-14 -8.8316E-03 -3.9080E-14
1.1369E-13 1.7053E-13 -2.6645E-15 -1.0658E-14 -1.1102E-15 7.5495E-15
IGIN = 2
THE NEXT TRY FOR PVRDOT = 6.0020E-02

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12 THE VARIABLE IS NO. 17
THIS COLUMN OF X =
0.0000 -1.8190E-12 -3.9080E-14 1.0397E-06 -2.2858E-03 -5.5843E-14 -1.0653E-14 5.5343E-14 -8.3818E-16 -3.1974E-14
1.1369E-13 -3.8457E-03 -2.6645E-15 -1.0658E-14 -1.1102E-15 7.5495E-15
IGIN = 3
THE NEXT TRY FOR PVRDOT = 1.2204E-01
12 THE VARIABLE IS NO. 17
THIS COLUMN OF X =
0.0000 -1.8190E-12 -3.9080E-14 2.1541E-06 -4.7358E-03 -5.5843E-14 -1.0658E-14 5.5343E-14 -8.3818E-15 -3.1974E-14
1.1369E-13 -7.9674E-03 -2.6645E-15 -1.0658E-14 -1.1102E-15 7.5495E-15
IGIN = 4
THE NEXT TRY FOR PVRDOT = 2.4008E-01
12 THE VARIABLE IS NO. 17
THIS COLUMN OF X =
0.0000 -1.8190E-12 -3.9080E-14 4.3830E-06 -9.6360E-03 -5.5843E-14 -1.0658E-14 5.5343E-14 -8.3818E-15 -3.1974E-14
1.1369E-13 -1.6212E-02 -2.6645E-15 -1.0658E-14 -1.1102E-15 7.5495E-15
IGIN = 5
THE NEXT TRY FOR PVRDOT = 4.8016E-01
12 THE VARIABLE IS NO. 17
THIS COLUMN OF X =
0.0000 -1.8190E-12 -3.9080E-14 8.8417E-06 -1.9438E-02 -5.5843E-14 -1.0658E-14 5.5343E-14 -8.3818E-15 -3.1974E-14
1.1369E-13 -3.2703E-02 -2.6645E-15 -1.0658E-14 -1.1102E-15 7.5495E-15
IGIN = 6
THE NEXT TRY FOR PVRDOT = 9.6032E-01
12 THE VARIABLE IS NO. 17
THIS COLUMN OF X =
0.0000 -1.8190E-12 -3.9080E-14 1.7762E-05 -3.9049E-02 -5.5843E-14 -1.0658E-14 5.5343E-14 -8.3818E-16 -3.1974E-14
1.1369E-13 -6.5695E-02 -2.6645E-15 -1.0658E-14 -1.1102E-15 7.5495E-15
IGIN = 7
THE NEXT TRY FOR PVRDOT = 1.9206E 00
12 THE VARIABLE IS NO. 17
THIS COLUMN OF X =
3.9552E-01 4.7398E-01 -3.8744E-04 -2.0027E-04 -9.4820E-02 3.7991E-03 6.9572E-04 -5.5205E-03 -9.2949E-05 5.3702E-04
-7.7955E-03 -1.4507E-01 -1.1108E-04 5.4386E-04 -5.7360E-05 -2.6730E-04
IGIN = 8
THE NEXT TRY FOR PVRDOT = 8.2593E 00
12 THE VARIABLE IS NO. 17
THIS COLUMN OF X =
1.5193E 00 2.0168E 00 7.6251E-04 -1.0128E-03 -4.0596E-01 2.0086E-02 2.1978E-03 -5.7387E-03 -3.9423E-04 5.5663E-03
-1.7851E-02 -6.1737E-01 -6.1637E-04 2.0306E-03 -2.2664E-04 -1.3558E-03
IGIN = 9
THE NEXT TRY FOR PVRDOT = 8.9522E 00
12 THE VARIABLE IS NO. 17
THIS COLUMN OF X =
1.8955E 00 2.0020E 00 -9.1089E-04 -1.0094E-03 -4.3617E-01 1.9679E-02 2.4932E-03 -1.2742E-02 -5.1258E-04 3.6500E-03
-2.5673E-02 -6.6903E-01 -7.5975E-04 2.2994E-03 -3.8696E-04 -1.3196E-03
IGIN = 0
THE NEXT TRY FOR PVRDOT = 8.9522E 00

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13 THE VARIABLE IS NO. 12
THIS COLUMN OF X =
0.0000 -1.8190E-12 -3.9080E-14 -8.8678E-06 -5.0423E-04 -5.5843E-14 -1.0558E-14 5.5943E-14 -8.3818E-16 -3.1974E-14
1.1369E-13 -3.8686E-04 -2.6645E-15 -1.0658E-14 -1.1102E-15 -1.2609E-05
IGIN = 1
THE NEXT TRY FOR PVRDOT = 3.0010E-02
13 THE VARIABLE IS NO. 12
THIS COLUMN OF X =
0.0000 -1.8190E-12 -3.9080E-14 -1.3306E-05 -7.5660E-04 -5.5843E-14 -1.0558E-14 5.5943E-14 -8.3818E-16 -3.1974E-14
1.1369E-13 -5.8049E-04 -2.6645E-15 -1.0658E-14 -1.1102E-15 -1.8919E-05
IGIN = 2
THE NEXT TRY FOR PVRDOT = 6.0020E-02
13 THE VARIABLE IS NO. 12
THIS COLUMN OF X =
0.0000 -1.8190E-12 -3.9080E-14 -2.6612E-05 -1.5132E-03 -5.5843E-14 -1.0658E-14 5.5943E-14 -8.3818E-16 -3.1974E-14
1.1369E-13 -1.1610E-03 -2.6645E-15 -1.0658E-14 -1.1102E-15 -3.7839E-05
IGIN = 3
THE NEXT TRY FOR PVRDOT = 1.2004E-01
13 THE VARIABLE IS NO. 12
THIS COLUMN OF X =
0.0000 -1.8190E-12 -3.9080E-14 -5.3226E-05 -3.0265E-03 -5.5843E-14 -1.0658E-14 5.5943E-14 -8.3818E-16 -3.1974E-14
1.1369E-13 -2.3220E-03 -2.6645E-15 -1.0658E-14 -1.1102E-15 -7.5678E-05
IGIN = 4
THE NEXT TRY FOR PVRDOT = 2.4008E-01
13 THE VARIABLE IS NO. 12
THIS COLUMN OF X =
0.0000 -1.8190E-12 -3.9080E-14 -8.0770E-05 -1.9176E-03 -5.5943E-14 -1.0658E-14 5.5943E-14 -8.3818E-16 -3.1974E-14
7.2683E-03 2.4816E-03 -2.6645E-15 -1.0658E-14 -1.1102E-15 -1.1576E-04
IGIN = 5
THE NEXT TRY FOR PVRDOT = 4.8016E-01
13 THE VARIABLE IS NO. 12
THIS COLUMN OF X =
9.3247E-01 1.7515E-02 -1.8998E-03 -1.7536E-04 -7.2601E-03 1.4806E-03 2.0194E-03 -2.9532E-02 -2.1343E-04 -3.3925E-03
-1.6184E-02 -1.4545E-02 -3.1541E-04 1.9749E-03 -2.2926E-04 -1.7893E-04
IGIN = 6
THE NEXT TRY FOR PVRDOT = 8.8666E-01
13 THE VARIABLE IS NO. 12
THIS COLUMN OF X =
1.8107E-01 -6.4604E-01 -3.0056E-02 -3.7930E-03 -1.0301E-01 3.5734E-02 3.2839E-02 -4.3557E-01 -4.3510E-03 -5.7700E-02
-2.4168E-01 -2.2034E-01 -7.2746E-03 3.0486E-02 -4.6813E-03 -3.9431E-03
IGIN = 7
THE NEXT TRY FOR PVRDOT = 1.3759E-01
13 THE VARIABLE IS NO. 12
THIS COLUMN OF X =
2.8648E-01 -8.2890E-01 -4.4691E-02 -5.8131E-03 -1.6268E-01 5.0591E-02 5.2273E-02 -7.7595E-01 -5.7194E-03 -3.3125E-02
-3.8983E-01 -3.5637E-01 -1.0036E-02 4.9539E-02 -7.2368E-03 -6.7187E-03
IGIN = 8
THE NEXT TRY FOR PVRDOT = 1.4288E-01

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13 THE VARIABLE IS NO. 12
THIS COLUMN OF X =
2.9730E-01 -8.7094E-01 -4.6476E-02 -6.0407E-03 -1.6865E-01 5.2700E-02 5.4215E-02 -8.0540E-01 -5.3810E-03 -9.1454E-02
-4.0382E-01 -3.6915E-01 -1.1374E-02 5.0338E-02 -7.5181E-03 -6.2548E-03
IGIN = 0
THE NEXT TRY FOR PVRDOT = 1.4288E-01
14 THE VARIABLE IS NO. 10
THIS COLUMN OF X =
0.0000 -3.6380E-12 -4.1595E-03 -2.5862E-04 -9.1864E-03 -5.2849E-03 -1.1735E-03 1.5527E-02 -2.1499E-04 -3.1190E-03
5.4629E-03 3.1605E-03 -5.0135E-04 -1.1116E-03 -1.9962E-04 -2.8112E-04
IGIN = 1
THE NEXT TRY FOR PVRDOT = 3.0010E-02
14 THE VARIABLE IS NO. 10
THIS COLUMN OF X =
0.0000 -3.6380E-12 -4.1595E-03 -4.0059E-04 -1.2589E-02 -5.2849E-03 -1.1735E-03 2.0333E-02 -2.1499E-04 -3.1190E-03
3.9630E-03 -2.4956E-04 -7.5246E-04 -1.1116E-03 -1.9962E-04 -4.7056E-04
IGIN = 2
THE NEXT TRY FOR PVRDOT = 6.0020E-02
14 THE VARIABLE IS NO. 10
THIS COLUMN OF X =
-5.2617E-01 -6.8938E-01 -1.1250E-02 -5.6169E-04 -3.8006E-03 -2.7031E-02 -7.4835E-03 4.7507E-02 -4.7522E-04 -9.4907E-03
2.5057E-02 2.5627E-02 -1.6906E-03 -7.2159E-03 -4.8537E-04 -6.3162E-04
IGIN = 3
THE NEXT TRY FOR PVRDOT = 2.5994E-01
14 THE VARIABLE IS NO. 10
THIS COLUMN OF X =
-3.4406E-00 -3.4482E-00 -5.1329E-02 -2.3626E-03 1.5491E-03 -1.2425E-01 -3.5967E-02 2.5293E-01 -2.2350E-03 -4.2451E-02
1.5453E-01 1.5466E-01 -7.4286E-03 -3.4580E-02 -2.2773E-03 -2.5063E-03
IGIN = 4
THE NEXT TRY FOR PVRDOT = 3.5684E-01
14 THE VARIABLE IS NO. 10
THIS COLUMN OF X =
-4.7544E-00 -4.7632E-00 -7.0456E-02 -3.2546E-03 2.9223E-03 -1.7068E-01 -4.9563E-02 3.4369E-01 -3.0787E-03 -5.8224E-02
2.1434E-01 2.1422E-01 -1.0229E-02 -4.7645E-02 -3.1374E-03 -3.5904E-03
IGIN = 0
THE NEXT TRY FOR PVRDOT = 3.5684E-01
15 THE VARIABLE IS NO. 4
THIS COLUMN OF X =
0.0000 -1.8190E-12 4.0510E-04 4.3128E-06 3.0482E-03 -5.6843E-14 -1.0658E-14 5.5943E-14 1.0130E-05 -3.1974E-14
1.1369E-13 1.7053E-13 -2.6645E-15 -1.3658E-14 -1.1102E-15 7.5495E-15
IGIN = 1
THE NEXT TRY FOR PVRDOT = 3.0010E-02
15 THE VARIABLE IS NO. 4
THIS COLUMN OF X =
0.0000 -1.8190E-12 1.7331E-03 -3.9492E-05 5.7380E-03 2.2212E-03 -2.1672E-04 9.0435E-03 1.0977E-05 1.3109E-03
7.2173E-03 3.9439E-03 2.3541E-05 -2.0292E-04 -1.1102E-15 -5.8379E-05
IGIN = 2
THE NEXT TRY FOR PVRDOT = 6.0020E-02

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15 THE VARIABLE IS NO. 4
THIS COLUMN OF X =
0.0000 -1.8190E-12 3.4516E-03 -3.0159E-05 1.0774E-02 4.4333E-03 -4.3254E-04 1.5665E-02 2.1972E-05 2.6165E-03
1.3202E-02 6.6952E-03 2.7140E-05 -4.0499E-04 -1.1102E-15 -1.3157E-04
IGIN = 3
THE NEXT TRY FOR PVRDOT = 1.2004E-01
15 THE VARIABLE IS NO. 4
THIS COLUMN OF X =
7.1928E-01 2.2771E-02 2.3292E-03 -2.4320E-04 1.1986E-02 6.9162E-03 -2.0021E-04 1.3209E-02 -3.0479E-04 5.3631E-04
5.6192E-03 9.1895E-04 -2.5950E-04 -1.8868E-04 -3.4477E-04 -2.3794E-04
IGIN = 4
THE NEXT TRY FOR PVRDOT = 1.1032E 00
15 THE VARIABLE IS NO. 4
THIS COLUMN OF X =
6.4595E 00 -5.8194E-01 2.0431E-02 -2.3006E-03 1.3963E-01 6.7292E-02 -4.7452E-03 1.7544E-01 -3.1730E-03 3.3237E-03
9.4424E-02 5.4532E-02 -3.1400E-03 -4.4463E-03 -3.5743E-03 -2.1800E-03
IGIN = 5
THE NEXT TRY FOR PVRDOT = 1.8393E 00
15 THE VARIABLE IS NO. 4
THIS COLUMN OF X =
1.1749E 01 -8.0856E-01 3.5883E-02 -3.7814E-03 2.2837E-01 1.0619E-01 -6.1253E-03 2.5099E-01 -5.3231E-03 6.1838E-03
1.2595E-01 6.4543E-02 -5.0577E-03 -5.7793E-03 -6.0082E-03 -3.5475E-03
IGIN = 0
THE NEXT TRY FOR PVRDOT = 1.8393E 00
16 THE VARIABLE IS NO. 16
THIS COLUMN OF X =
0.0000 -1.8190E-12 -3.9080E-14 5.5080E-07 -1.8722E-04 -5.5843E-14 -1.0658E-14 5.5843E-14 -8.3918E-15 -3.1974E-14
1.1369E-13 1.7053E-13 -2.6645E-15 -1.0658E-14 -1.1102E-15 7.5495E-15
IGIN = 1
THE NEXT TRY FOR PVRDOT = 3.0010E-02
16 THE VARIABLE IS NO. 16
THIS COLUMN OF X =
0.0000 -1.8190E-12 -3.9080E-14 9.2647E-07 -2.8093E-04 -5.6843E-14 -1.0658E-14 5.5843E-14 -8.3918E-16 -3.1974E-14
1.1369E-13 1.7053E-13 -2.6645E-15 -1.0658E-14 -1.1102E-15 7.5495E-15
IGIN = 2
THE NEXT TRY FOR PVRDOT = 6.0020E-02
16 THE VARIABLE IS NO. 16
THIS COLUMN OF X =
0.0000 -1.8190E-12 -3.9080E-14 1.6529E-06 -5.6185E-04 -5.6843E-14 -1.0658E-14 5.5843E-14 -8.3918E-15 -3.1974E-14
1.1369E-13 1.7053E-13 -2.6645E-15 -1.0658E-14 -1.1102E-15 7.5495E-15
IGIN = 3
THE NEXT TRY FOR PVRDOT = 1.2004E-01
16 THE VARIABLE IS NO. 16
THIS COLUMN OF X =
0.0000 -1.8190E-12 -3.9080E-14 3.3059E-06 -1.1237E-03 -5.6843E-14 -1.0658E-14 5.5843E-14 -8.3918E-16 -3.1974E-14
1.1369E-13 1.7053E-13 -2.6645E-15 -1.0658E-14 -1.1102E-15 7.5495E-15
IGIN = 4
THE NEXT TRY FOR PVRDOT = 2.4008E-01

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16 THE VARIABLE IS NO. 16
THIS COLUMN OF X =
0.0000 -1.8190E-12 -3.9080E-14 5.3704E-06 4.8161E-04 -5.6843E-14 -1.0658E-14 5.5943E-14 -8.3918E-15 -3.1974E-14
1.1369E-13 4.5914E-03 -2.6645E-15 -1.0658E-14 -1.1102E-15 7.5495E-15
IGIN = 5
THE NEXT TRY FOR PVRDOT = 4.8016E-01
16 THE VARIABLE IS NO. 16
THIS COLUMN OF X =
0.0000 -1.8190E-12 -3.9080E-14 1.0916E-05 7.9900E-04 -5.6843E-14 -1.0658E-14 5.5943E-14 -8.3918E-16 -3.1974E-14
1.1369E-13 8.9068E-03 -2.6645E-15 -1.0658E-14 -1.1102E-15 7.5495E-15
IGIN = 6
THE NEXT TRY FOR PVRDOT = 9.6032E-01
16 THE VARIABLE IS NO. 16
THIS COLUMN OF X =
3.0830E-01 3.5610E-01 -3.9782E-04 -1.4345E-04 -1.1121E-02 2.6163E-03 5.9942E-04 -5.8535E-03 -5.5501E-05 3.1574E-04
-7.2489E-03 6.6445E-03 -7.4446E-05 5.5387E-04 -3.9586E-05 -1.8619E-04
IGIN = 7
THE NEXT TRY FOR PVRDOT = 1.4345E 01
16 THE VARIABLE IS NO. 16
THIS COLUMN OF X =
4.3807E 00 4.7079E 00 -6.1342E-04 -2.5272E-03 -1.4436E-01 4.8174E-02 5.6199E-03 -2.5284E-02 -1.2350E-03 1.0124E-02
-5.6371E-02 1.3582E-01 -1.9184E-03 5.1781E-03 -8.6925E-04 -3.2296E-03
IGIN = 8
THE NEXT TRY FOR PVRDOT = 2.3735E 01
16 THE VARIABLE IS NO. 16
THIS COLUMN OF X =
7.2121E 00 7.7767E 00 -8.6033E-04 -4.2119E-03 -2.3882E-01 7.9947E-02 9.0461E-03 -3.9192E-02 -2.0534E-03 1.7001E-02
-9.0033E-02 2.2739E-01 -3.2342E-03 3.3327E-03 -1.4523E-03 -5.3824E-03
IGIN = 0
THE NEXT TRY FOR PVRDOT = 2.3785E 01

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Y INVERSE =
1.2744E-02  5.2152E-03  4.4875E-02  1.2138E-00  2.7403E-02  5.4851E-03  2.0902E-01  1.7503E-03  4.3163E-01  1.9355E-03
4.7238E-04  3.3395E-04  1.2351E-02  1.1710E-01  1.8145E-01  1.5640E-02

AINV =
-3.0361E-01 -1.2767E-01 -1.3682E-03 -4.9360E-05 1.6744E-03 -2.6140E-03 -1.0199E-03 1.2731E-02 -3.3805E-05 -3.5354E-04
9.0641E-03 8.7402E-03 -2.0272E-04 -9.4552E-04 -3.7131E-05 -5.5965E-05
9.5122E-02 -1.0299E-01 -8.5334E-04 -3.5200E-05 3.9588E-04 -9.5795E-04 7.0880E-05 -2.3999E-03 -5.5239E-05 -1.1921E-03
-2.4953E-03 -2.6258E-03 -4.0857E-05 6.7086E-05 -6.3368E-05 -3.2366E-05
2.4067E-02 2.4475E-02 -1.2003E-02 -1.3310E-05 -5.7922E-03 1.9311E-05 -1.7063E-05 5.0050E-04 -2.0105E-05 -1.2608E-04
2.8034E-04 1.0473E-06 -4.4543E-06 -1.5491E-05 -1.7226E-05 -1.0021E-05
9.8543E-00 1.0060E-01 -1.4693E-02 -5.1949E-03 -3.8106E-02 9.3286E-02 9.1359E-03 -1.5155E-02 -3.5134E-03 1.1657E-02
-8.8330E-02 -2.2562E-01 -4.2708E-03 8.4653E-03 -2.7753E-03 -6.7390E-03
5.7015E-02 5.7822E-02 -9.1418E-05 -3.4442E-05 -1.3910E-02 5.1855E-04 5.8330E-05 -2.0911E-04 -2.0255E-05 5.6829E-05
-6.0880E-04 -1.3630E-03 -2.2730E-05 5.3773E-05 -1.5490E-05 -3.7353E-05
3.5922E-01 1.2309E-01 1.1015E-03 3.7344E-05 -3.6619E-03 -2.9508E-03 9.7730E-04 -1.9479E-02 2.1490E-05 7.8958E-04
-1.3470E-02 -1.2703E-02 1.9601E-04 9.1192E-04 2.1345E-05 4.5445E-05
-1.7685E-00 -1.3579E-00 -1.3803E-02 -5.1475E-04 2.1270E-02 -1.7023E-02 -1.0554E-02 1.4991E-01 -3.3840E-04 -3.9943E-03
1.0314E-01 9.8943E-02 -2.1542E-03 -9.7930E-03 -3.7944E-04 -5.9570E-04
-3.6525E-02 -2.7554E-02 -3.7105E-04 -1.5604E-05 -1.1031E-03 -8.0066E-04 -2.1677E-04 -2.0539E-03 -1.4746E-05 -2.9617E-04
-1.3507E-03 -1.0125E-03 -4.4391E-05 -2.0480E-04 -1.4931E-05 -1.7366E-05
3.3066E-00 2.7855E-00 1.3323E-01 -1.7706E-03 1.4572E-01 1.3907E-02 -1.8593E-03 5.2804E-02 -2.4350E-03 -1.2420E-02
1.9491E-02 -1.3591E-02 -1.4001E-03 -1.7258E-03 -2.1143E-03 -1.7054E-03
-9.9333E-02 7.3039E-02 -6.7760E-04 1.9886E-05 -1.9017E-03 -1.5236E-03 2.9059E-05 -2.6553E-03 2.8551E-05 -4.9141E-04
-1.4304E-03 -1.1065E-03 3.7873E-05 2.8070E-05 3.2223E-05 1.8570E-05
2.8448E-03 -6.3663E-04 -1.1823E-05 -9.1399E-07 -1.7424E-04 -4.4153E-06 3.8193E-05 -5.7023E-05 -1.0544E-06 -1.5209E-05
-3.7997E-04 -3.2999E-04 -1.0649E-06 3.5591E-06 -1.1261E-06 -9.6402E-07
5.3301E-04 6.6855E-04 -3.0419E-07 -3.3709E-07 -1.4566E-04 6.5718E-06 8.3259E-07 -4.2551E-06 -1.3119E-07 1.2139E-06
-8.5734E-06 -2.2342E-04 -2.5372E-07 7.6788E-07 -1.2923E-07 -4.4068E-07
3.5719E-01 -1.0757E-02 -5.7402E-04 -7.4508E-05 -2.0830E-03 6.5090E-04 6.6961E-04 -9.9474E-03 -8.5222E-05 -1.1297E-03
-4.9875E-03 -4.5593E-03 -1.4048E-04 6.2172E-04 -9.2856E-05 -7.7253E-05
-5.5675E-01 -5.5779E-01 -8.2506E-03 -3.8112E-04 3.4221E-04 -1.9987E-02 -5.8039E-03 4.0950E-02 -3.6053E-04 -6.8182E-03
2.5099E-02 2.5085E-02 -1.1978E-03 -5.5794E-03 -3.6740E-04 -4.2045E-04
2.1319E-00 -1.4672E-01 6.5111E-03 -5.8616E-04 4.1439E-02 1.9268E-02 -1.1115E-03 4.5523E-02 -9.6591E-04 1.1221E-03
2.2853E-02 1.1712E-02 -9.1774E-04 -1.0487E-03 -1.0902E-03 -6.4372E-04
1.1280E-01 1.2163E-01 -1.3456E-05 -6.5875E-05 -3.7351E-03 1.2504E-03 1.4149E-04 -5.9733E-04 -3.2193E-05 2.6539E-04
-1.4081E-03 3.5564E-03 -5.0583E-05 1.3032E-04 -2.2714E-05 -8.4181E-05

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A =

```

-5.0565E 00 -3.0710E-02 -2.9468E-01 3.9335E 01 -5.3391E-01 -2.6047E 02 2.0381E 03 2.7527E 01 -5.5545E 01 5.9342E 02
8.3973E-02 -5.7299E-02 -3.4526E 03 4.5147E 02 -1.4176E 04 4.3767E 00
2.3346E-02 -4.8023E 00 3.0603E 00 -2.2896E 02 -3.1802E-02 -7.0417E-01 -5.2383E 02 6.5972E-01 3.1051E 03 -5.0291E 02
3.5671E 01 -4.3288E-02 1.1222E 04 5.3972E 02 -1.3135E 03 -1.6550E 04
1.0294E-02 1.6695E-02 -7.5582E 01 1.0153E 04 2.2164E-01 2.3439E 00 2.4440E 02 1.9153E-01 -2.4007E 04 7.0109E 01
2.1929E-02 8.1418E-01 3.5630E 01 -2.3794E 02 1.6168E 04 -2.7766E 03
-2.9561E-04 -8.3654E-04 -4.4383E-02 -1.2232E 03 4.1008E-01 8.5963E-03 3.2784E 00 -5.3816E-03 3.5745E 02 3.1630E-02
-5.4918E-04 -2.7182E-01 -7.5532E-01 -3.4222E 00 -9.0175E 00 7.8874E 02
5.0849E-03 7.9130E-03 4.9072E 01 -4.6135E 04 -7.3045E 01 3.5386E-01 -5.9434E 01 5.0753E-02 3.3201E 03 -2.7018E 00
7.3962E-02 3.6321E 01 4.3765E 01 5.1096E 01 3.3498E 02 3.9300E 04
1.1725E 00 -2.0090E-01 6.2355E-01 6.1426E 02 -4.8913E-02 -1.6955E 02 -8.0099E 03 3.2409E 00 -1.3497E 01 2.6140E 02
7.1633E-01 4.1844E-02 1.2136E 02 8.5777E 03 1.3736E 03 -8.0441E 02
6.6468E-01 -3.6682E-03 3.8230E-03 5.9720E 00 -2.2886E-03 7.3205E 00 -3.0473E 03 2.5755E-02 -3.2135E 01 -4.6793E 01
-1.0932E-03 4.6000E-04 9.8476E-02 3.0318E 03 1.6012E 03 -6.1656E 00
2.2990E-01 -7.2786E-02 -2.3702E 00 -9.7965E 02 4.5040E-02 3.7147E 02 -3.4792E 04 -2.5199E 02 -1.2709E 03 8.5757E 00
2.3863E-01 -3.5829E-01 2.4379E 01 3.2969E 04 1.4294E 03 9.3226E 02
7.7884E-04 1.1386E-03 6.2887E-01 7.5500E 02 1.6265E-02 -7.4471E-02 -1.2388E 01 1.4297E-02 -2.0390E 03 -9.2605E-01
9.0396E-04 6.0542E-02 2.5044E 00 1.2848E 01 1.4551E 03 -2.0622E 02
1.2849E-01 9.5445E 00 1.1839E 00 -1.4713E 02 6.3233E-01 1.9940E 01 -1.5712E 04 1.8281E 00 7.2239E 04 -7.8616E 02
1.0101E-01 1.1290E-01 -2.9718E 02 1.5921E 04 -6.4339E 04 6.9441E 00
-3.9575E 00 1.9362E 01 -3.8123E 01 1.5028E 03 8.1694E 00 -7.7309E 01 -4.3532E 04 1.9189E 03 -2.0335E 04 7.5004E 02
-3.0769E 03 2.1250E 00 -8.5180E 04 5.2646E 04 1.4233E 04 1.2376E 05
-2.2171E-01 -1.6654E 01 -5.2295E 02 2.3339E 06 -1.1979E 01 1.0143E 02 -5.8164E 03 1.9571E 00 -4.0040E 05 -9.2325E 01
3.7857E 03 -4.0282E 03 7.1729E 04 5.3449E 03 -6.6422E 04 -2.3473E 06
-8.0010E-02 9.6115E-01 -2.4339E 00 1.4322E 02 1.5497E-01 -7.9874E 00 1.6109E 03 -1.2131E 01 -2.2242E 03 1.1273E 01
3.4646E 00 7.1001E-02 -6.8456E 03 -8.3737E 02 2.0386E 03 6.8357E 03
3.2134E-02 -1.8142E-02 -3.5590E-02 5.1426E-01 1.6311E-02 -1.1417E 01 5.2277E 03 4.9554E 00 -2.1763E 02 -1.8499E 00
-1.7387E-02 -2.7979E-03 3.5362E 01 -5.5485E 03 2.3932E 02 -9.6110E-01
-3.5033E-03 4.7999E-01 -3.0407E-02 5.1570E 00 -2.1147E-02 3.1878E 00 -9.6545E 02 -5.1237E-02 5.8749E 03 3.2905E 00
3.2289E-03 -2.6589E-03 8.2812E 00 9.6004E 02 -6.0850E 03 -2.4889E 00
-9.6409E-03 -6.5289E-01 -1.5944E 01 8.7379E 04 -3.7206E-01 1.6765E 00 8.2207E 01 3.3614E-02 -1.2211E 04 -4.1532E 00
-6.6185E 00 2.5525E 01 4.6443E 03 -1.0187E 02 -2.1588E 03 -7.7551E 04

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C =

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-6.4699E-07 -2.0282E-06 6.8625E-05 -4.4260E-01 6.5684E-06 2.3009E-05 6.6218E-03 -2.1431E-05 2.2795E-02 3.1351E-05
-8.7537E-07 9.5610E-08 -1.9250E-03 -6.8742E-03 -7.9298E-03 1.1598E-02
1.1987E-02 4.6434E-02 -1.2509E 00 8.0195E 03 -7.7002E-02 -5.9215E-01 -1.6055E 02 2.8252E-01 -3.1748E 02 -1.1673E 00
4.8001E-02 -5.6520E-03 3.6014E 01 1.6665E 02 6.3557E 01 -2.0253E 02
1.1937E-02 4.6434E-02 -1.2509E 00 8.0195E 03 -7.7002E-02 -5.9215E-01 -1.6055E 02 2.8252E-01 -3.1748E 02 -1.1673E 00
4.8001E-02 -5.6520E-03 3.6014E 01 1.6665E 02 6.3557E 01 -2.0253E 02

```


OUTPUT AM= 0.000 ALTP= 0. T4= 2900.59 ETAR= 1.0000

MIDDLE SPOOL IS DUMMY

NO AIRFLOW INTO WING
THE OUTPUT IS IN ENGLISH UNITS

PCNP 0.102552E 03	CNP 0.102551E 01	ZP 0.834571E 00	PRP 0.300924E 01	WAPC 0.222300E 03	WAP 0.222300E 03
PCNC 0.118482E 03	CNC 0.998871E 00	ZC 0.814720E 00	PRC 0.848852E 01	WACC 0.551328E 02	WAC 0.138470E 03
T2 0.518670E 03	P2 0.100000E 01	T21 0.744583E 03	P21 0.300924E 01	T3 0.147146E 04	P3 0.255440E 02
PCBLP 0.000000	BLP 0.000000	PCBLC 0.160000E 00	BLC 0.221552E 02	PCBLCB 0.000000	BLOB 0.000000
PCBLHP 0.726000E 00	BLHP 0.160847E 02	PCBLLP 0.660000E-01	BLLP 0.146224E 01	T4 0.290059E 04	P4 0.241114E 02
WA3 0.115315E 03	WFB 0.277750E 01	WG4 0.119092E 03	PAR4 0.238793E-01	ETAB 0.100000E 01	DPC04 0.560953E-01
TFPHF 0.499981E 02	CNHP 0.200241E 01	DHTCHP 0.734620E-01	DHTC 0.213088E 03	T5 0.210970E 04	P5 0.570544E 01
TFPLP 0.130079E 03	CNLP 0.230199E 01	DHTCLP 0.423525E-01	DHTF 0.893510E 02	T55 0.179415E 04	P55 0.270347E 01
PCBLDU 0.208000E 00	BLDU 0.460828E 01	T24 0.743940E 03	P24 0.283418E 01	T25 0.793940E 03	P25 0.283418E 01
WAD 0.884383E 02	WFD 0.000000	WG24 0.884393E 02	PAR24 0.000000	ETAD 0.000000	DPDUC 0.581737E-01
ETAF 0.847718E 00	ETAC 0.313972E 00	ETATHP 0.871273E 00	ETATLP 0.902172E 00	AM55 0.283351E 00	AM25 0.391747E 00
T6 0.141910E 04	P6 0.272825E 01	PS6 0.262221E 01	AM6 0.243037E 00	V6 0.438078E 03	WG6 0.225077E 03
T7 0.141910E 04	WPA 0.000000	WG7 0.225077E 03	PAR7 0.124944E-01	ETAA 0.000000	DPAFT 0.598972E-01
PS8 0.139397E 01	AM8 0.100000E 01	V8 0.167738E 04	PS9 0.138387E 01	AM9 0.100000E 01	V9 0.157739E 04
PS28 0.000000	AM28 0.000000	V28 0.000000	PS29 0.000000	AM29 0.000000	V29 0.000000
BYPASS 0.605403E 00	HPEXT 0.000000	WPT 0.277750E 01	WST 0.225077E 03	VA 0.000000	FRD 0.000000
CVMNOZ 0.949400E 00	VJM 0.159250E 04	CVDNZZ 0.000000	VJD 0.000000	FGM 0.111405E 05	F3P 0.239544E 04

MAIN SONIC CONVERGENT NOZZLE

FG= 13536.00

FN= 13536.00

SFC= 0.73370

CONVERGED AFTER 9 LOOPS

OUTPUT AM= 0.000 ALTP= 0. T4= 2891.96 ETAP= 1.0000

MIDDLE SPOOL IS DUMMY

NO AIRFLOW INTO WING
THE OUTPUT IS IN ENGLISH UNITS

PCNF 0.102579E 03	CNF 0.102579E 01	ZF 0.825774E 00	PRF 0.298893E 01	WAF 0.222785E 03	WAF 0.222784E 03
PCNC 0.118421E 03	CNC 0.989320E 00	ZC 0.814219E 00	PRC 0.849040E 01	WACC 0.551772E 02	WAC 0.137779E 03
T2 0.518670E 03	P2 0.100000E 01	T21 0.743148E 03	P21 0.298893E 01	T3 0.146874E 04	P3 0.253772E 02
PCBLF 0.000000	BLF 0.000000	PCBLC 0.160000E 00	BLC 0.220446E 02	PCBLOB 0.000000	BLOB 0.000000
PCBLHP 0.726000E 00	BLHP 0.160044E 02	PCBLLP 0.660000E-01	BLLP 0.145494E 01	T4 0.289196E 04	P4 0.239530E 02
WA3 0.115734E 03	WFB 0.275000E 01	WG4 0.118484E 03	PAR4 0.237613E-01	ETAB 0.100000E 01	DPCOM 0.551209E-01
TFHP 0.499974E 02	CNHP 0.200437E 01	DHTCHP 0.735434E-01	DHTC 0.212685E 03	T5 0.210247E 04	P5 0.555582E 01
TFPLP 0.130333E 03	CNLP 0.230656E 01	DHTCLP 0.425347E-01	DHTF 0.894282E 02	T55 0.178644E 04	P55 0.267101E 01
PCBLDU 0.208000E 00	BLDU 0.458528E 01	T24 0.781733E 03	P24 0.281184E 01	T25 0.791733E 03	P25 0.281184E 01
WAD 0.895909E 02	WFD 0.000000	WG24 0.895909E 02	PAR24 0.000000	ETAD 0.000000	DPDUC 0.592483E-01
ETAP 0.847070E 03	ETAC 0.914197E 00	ETATHP 0.871218E 00	ETATLP 0.902435E 00	AM55 0.285327E 00	AM25 0.399315E 03
T6 0.140908E 04	P6 0.269846E 01	PS6 0.259177E 01	AM6 0.245431E 03	V6 0.440998E 03	WG6 0.225534E 03
T7 0.140908E 04	WFA 0.000000	WG7 0.225534E 03	PAR7 0.123437E-01	ETAA 0.000000	DPART 0.604555E-01
PS8 0.136756E 01	AM8 0.100000E 01	V8 0.167161E 04	PS9 0.136756E 01	AM9 0.100000E 01	V9 0.157151E 04
PS28 0.000000	AM28 0.000000	V28 0.000000	PS29 0.000000	AM29 0.000000	V29 0.000000
BYPASS 0.616972E 00	HPEXT 0.000000	WPT 0.275000E 01	WGT 0.225534E 03	VA 0.000000	PRD 0.000000
CVMNOZ 0.949400E 00	VJM 0.158703E 04	CVDN0Z 0.000000	VJD 0.000000	FGM 0.111248E 05	F3P 0.231661E 04

MAIN SONIC CONVERGENT NOZZLE

PG= 13441.39

PN= 13441.39

SFC= 0.73653

CONVERGED AFTER 10 LOOPS

```

B =
-3.3971E 02 -1.8844E 01
-7.6357E 00 8.1031E 01
2.7458E 01 -3.6972E 01
-7.3679E-01 -7.4372E 01
2.5007E 01 -2.0494E 03
8.0562E 01 -5.9852E 01
4.4730E 00 -1.0116E 00
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1.9901E 00 -2.8772E 00
5.3471E 02 -1.2480E 01
5.3638E 03 -1.0988E 02
2.0804E 03 1.1746E 03
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4.1724E-01 8.1581E-02 -2.9698E 00 4.3834E 02 1.3473E-01 3.0396E 02 -3.7220E 03 -2.2243E 02 -5.7708E 01
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-6.7336E-01 -7.4075E 01
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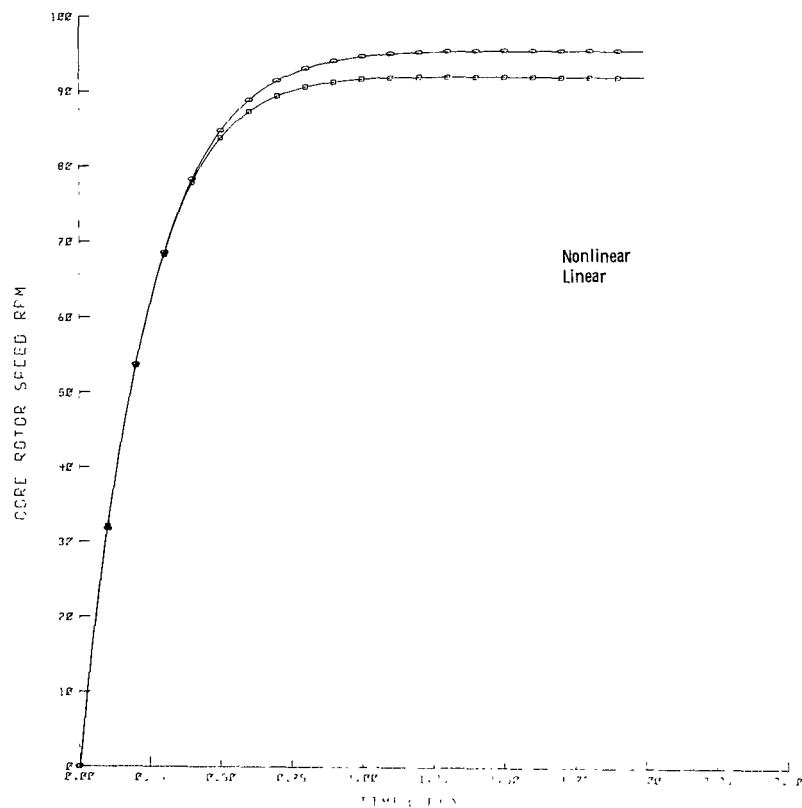
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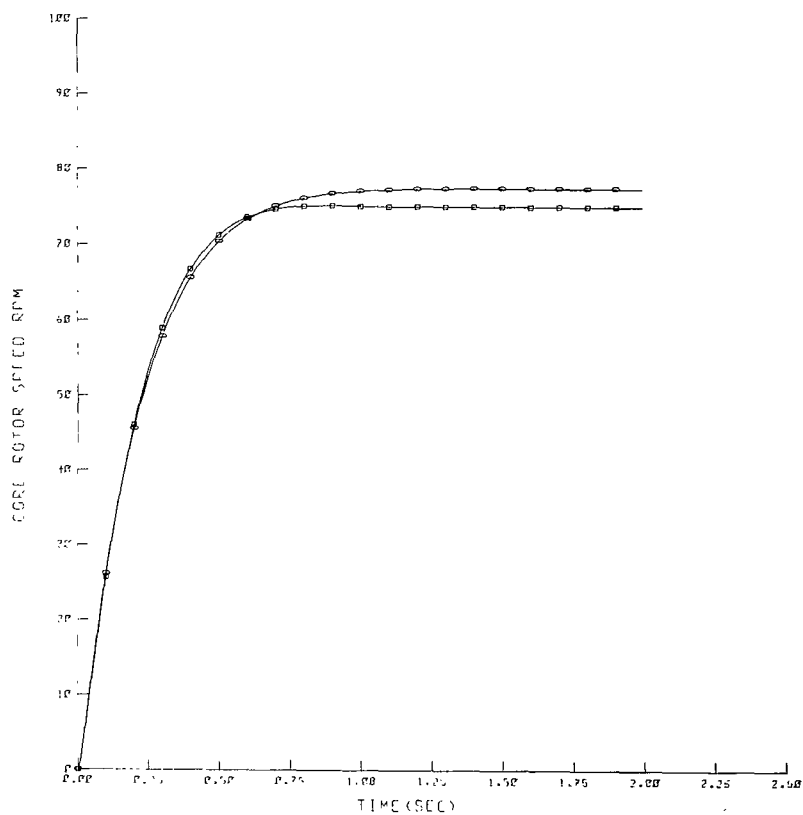
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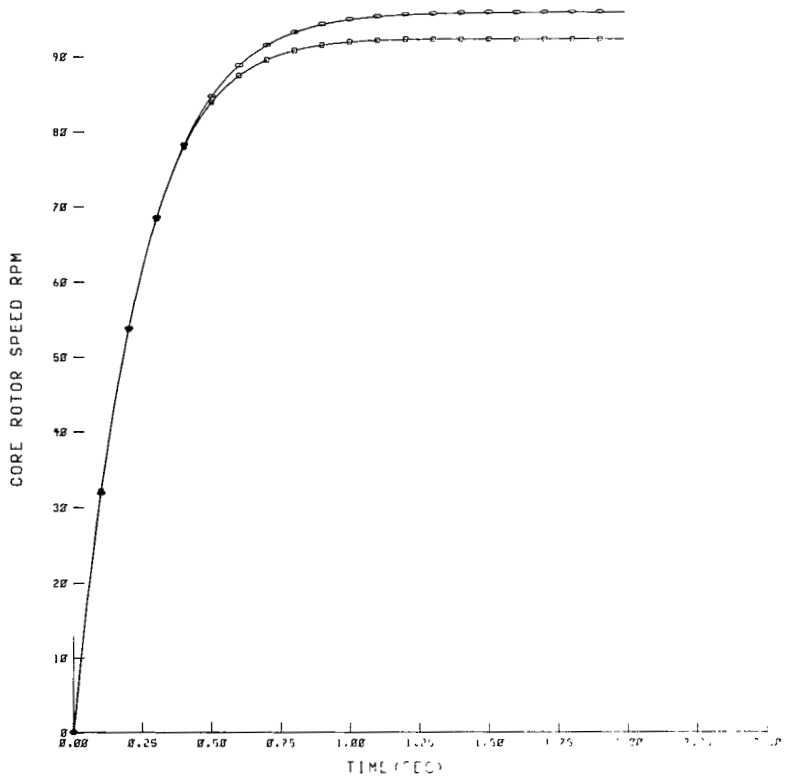
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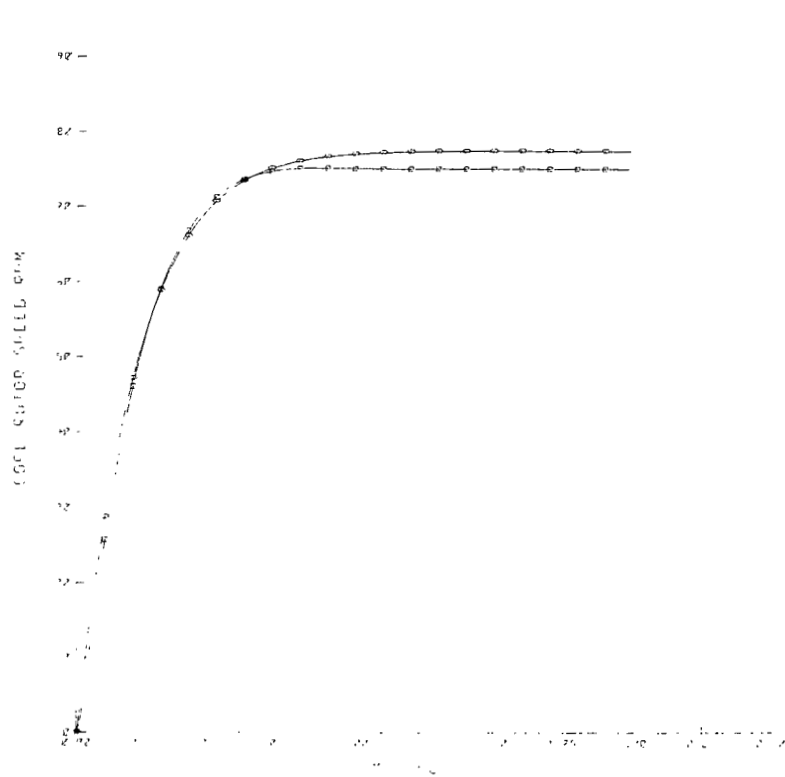
(a-1) With 3-percent step change in main fuel flow.



(a-2) With 3-percent step change in nozzle area.



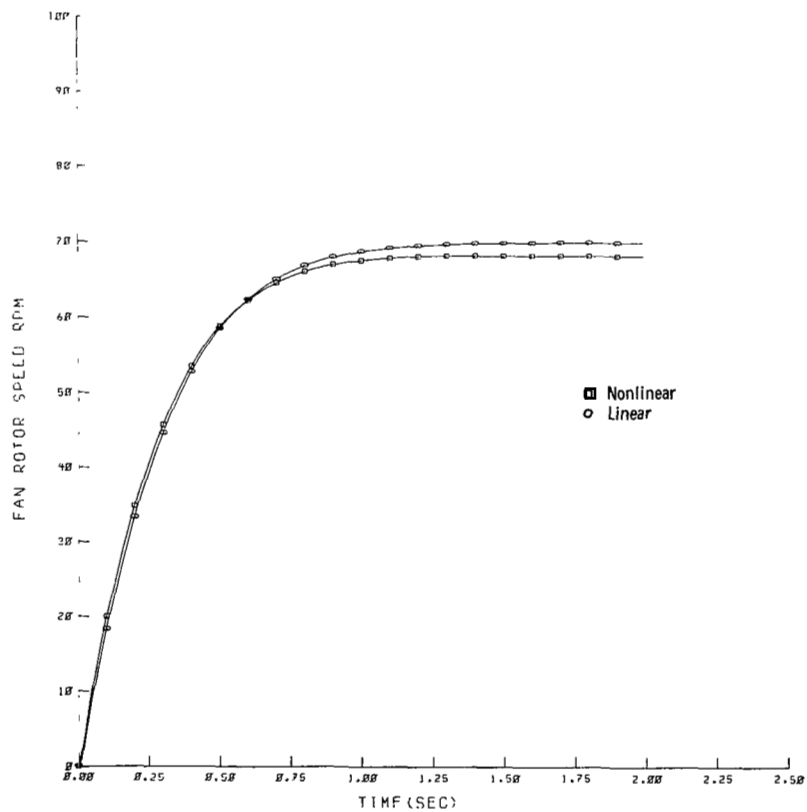
(b-1) With 3-percent step change in main fuel flow.



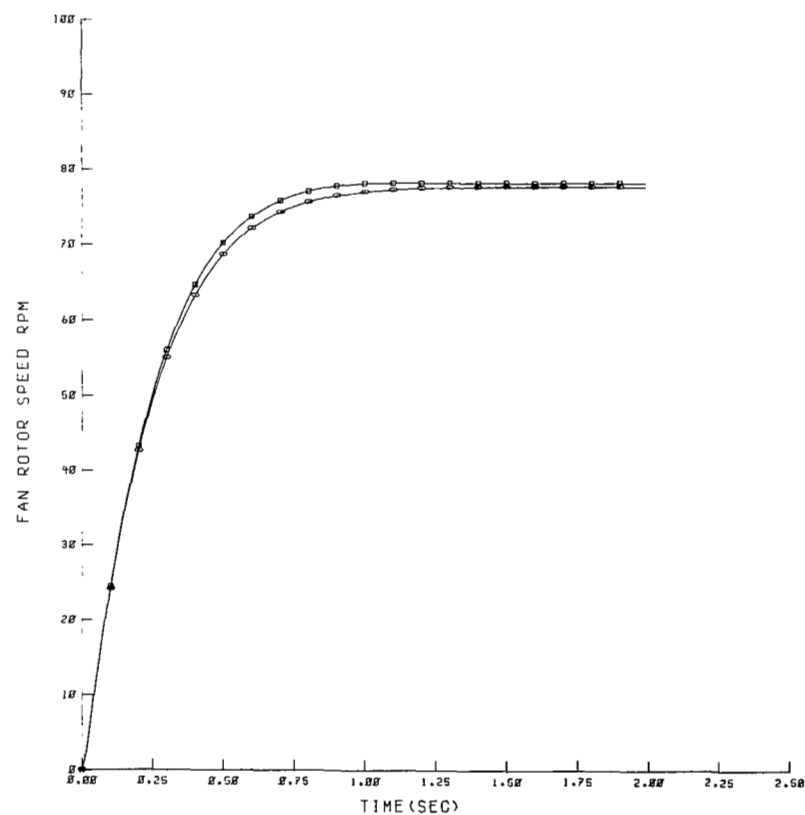
(b-2) With 3-percent step change in nozzle area.

(b) Comparison of reduced-order linear and nonlinear runs.

Figure 1. - Response of state 1 - core rotor speed.

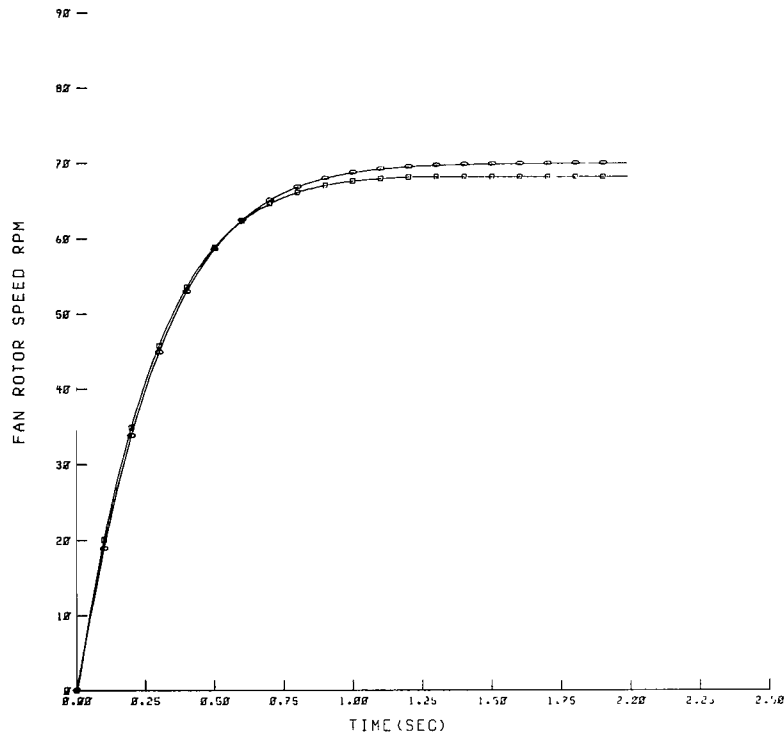


(a-1) With 3-percent step change in main fuel flow.

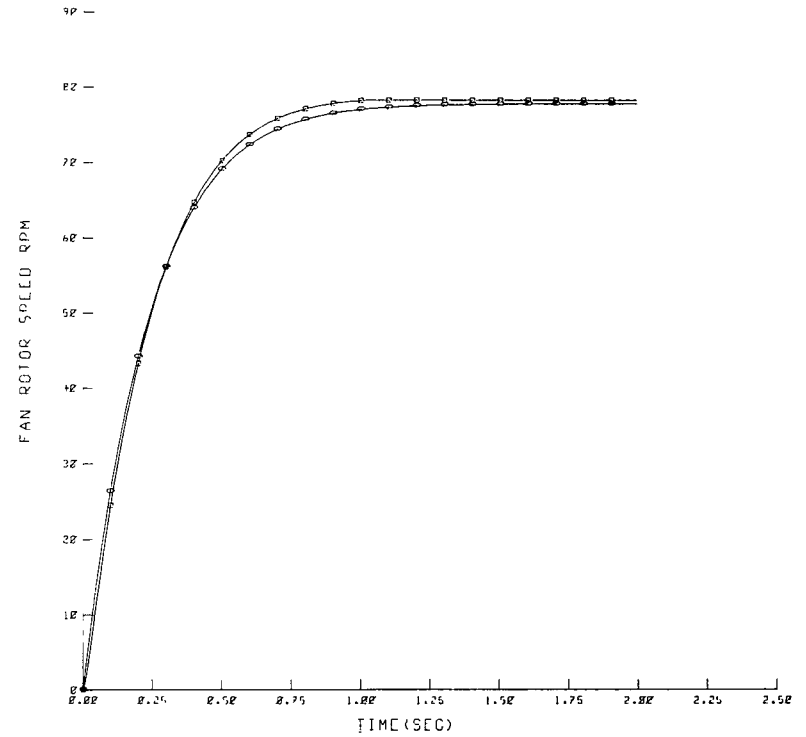


(a-2) With 3-percent step change in nozzle area.

(a) Comparison of full-order linear and nonlinear runs.



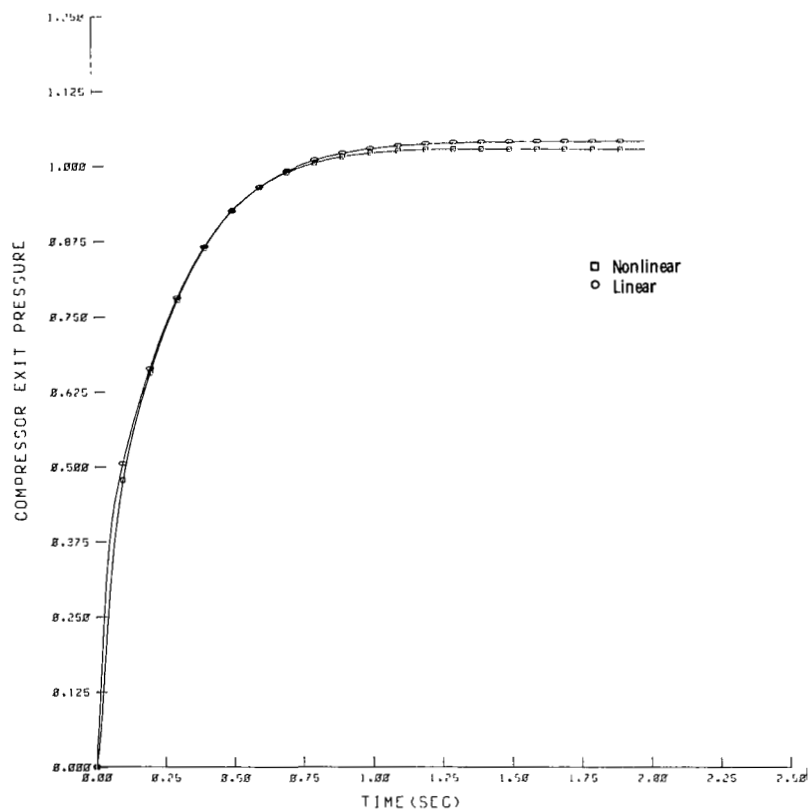
(b-1) With 3-percent step change in main fuel flow.



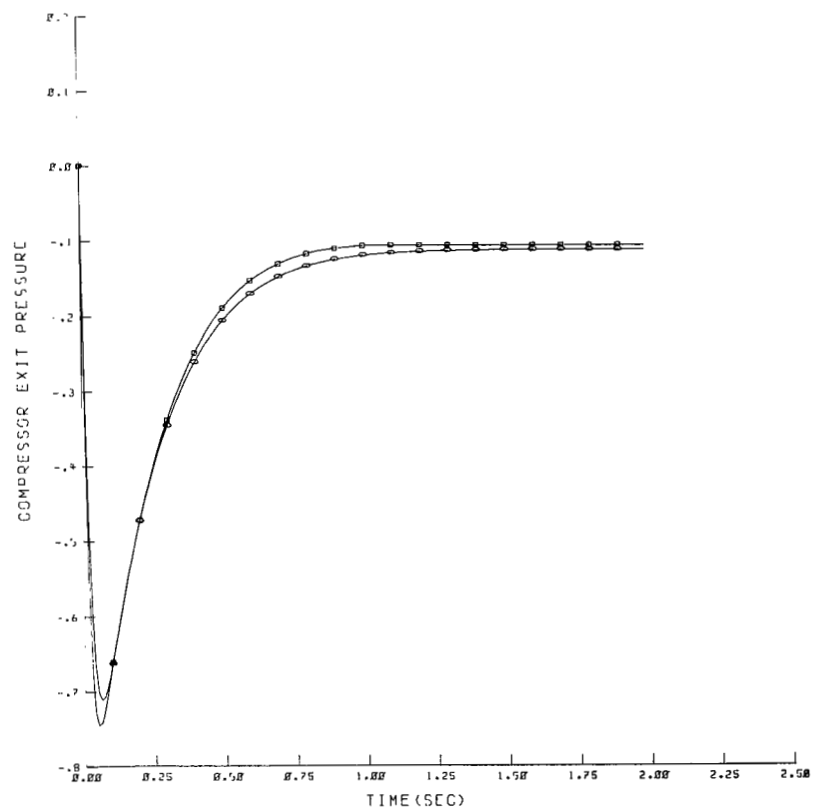
(b-2) With 3-percent step change in nozzle area.

(b) Comparison of reduced-order linear and nonlinear runs.

Figure 2 - Response of state 2 - fan rotor speed.

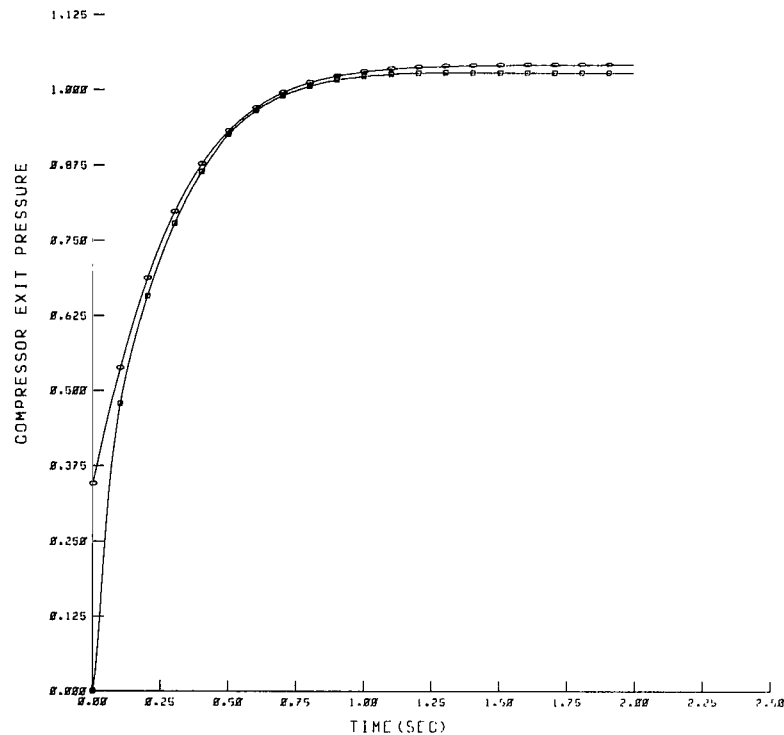


(a-1) With 3-percent step change in main fuel flow.

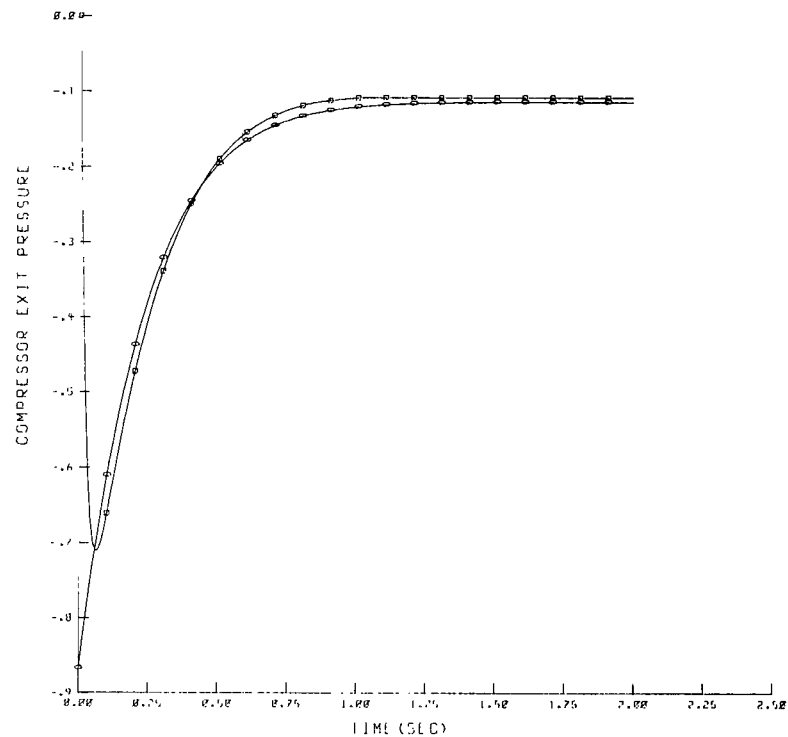


(a-2) With 3-percent step change in nozzle area.

(a) Comparison of full-order 1. bar and nonlinear runs



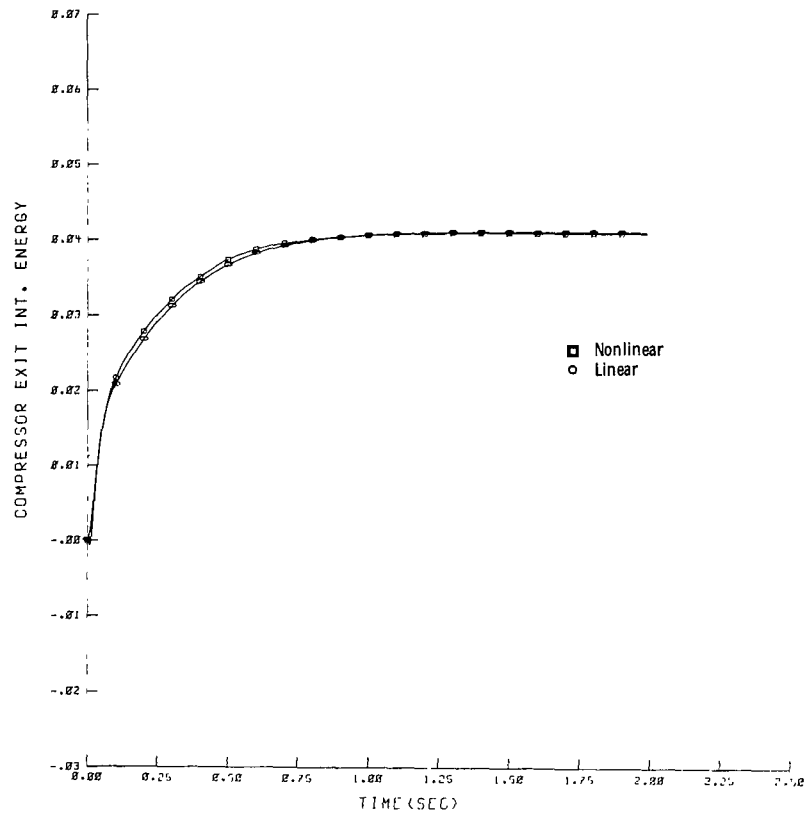
(b-1) With 3-percent step change in main fuel flow.



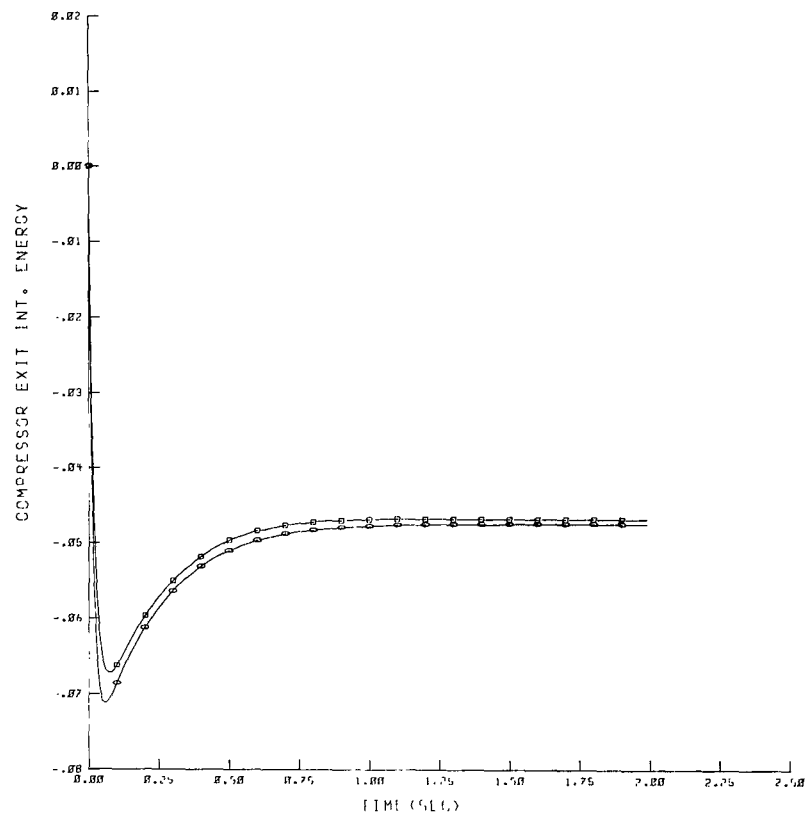
(b-2) With 3-percent step change in nozzle area.

(b) Comparison of reduced-order linear and nonlinear runs.

Figure 3. - Response of state 3 - compressor-exit pressure.

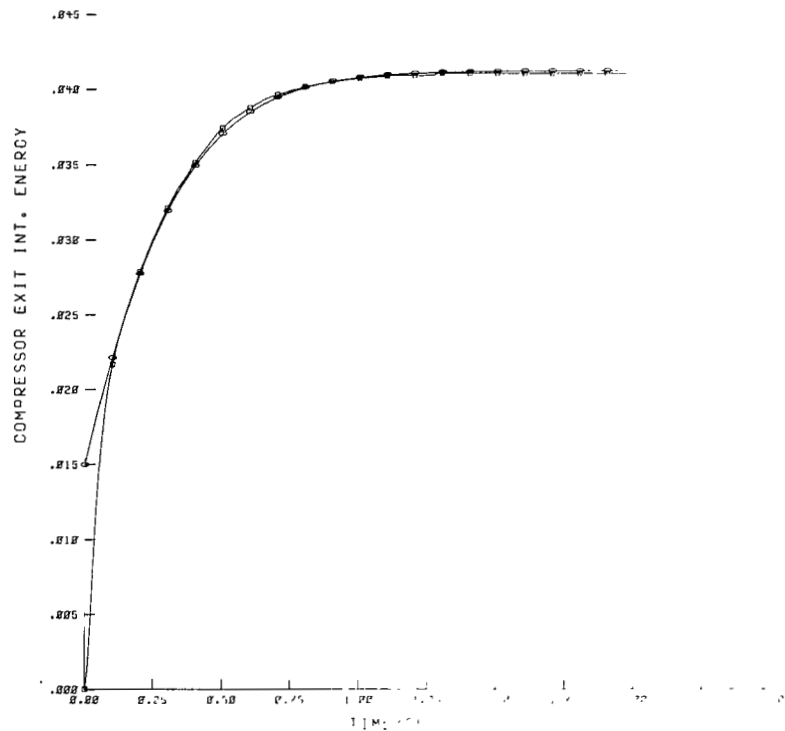


(a-1) With 3-percent step change in main fuel flow.

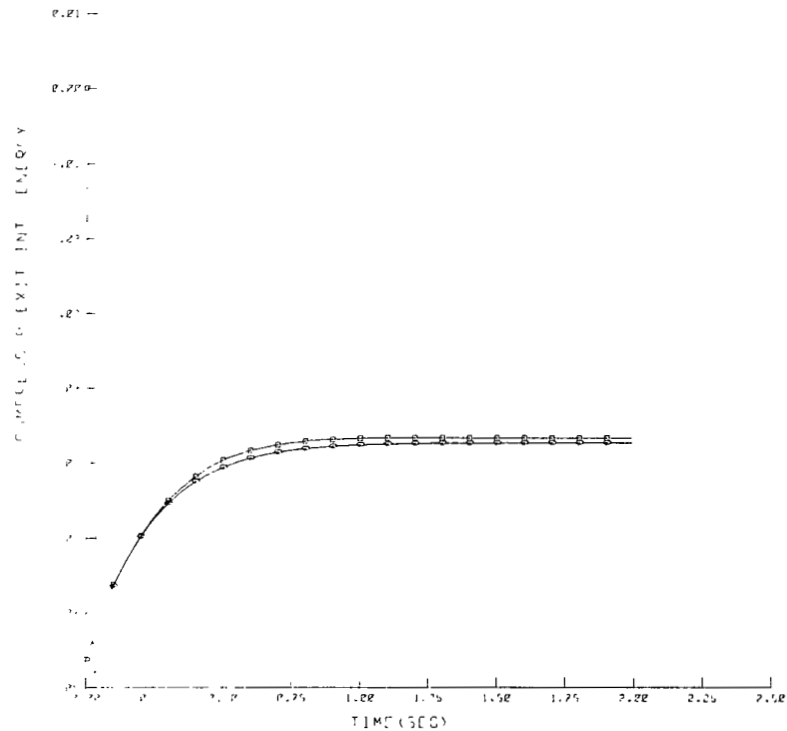


(a-2) With 3-percent step change in nozzle area.

(a) Comparison of full-order linear and nonlinear runs.



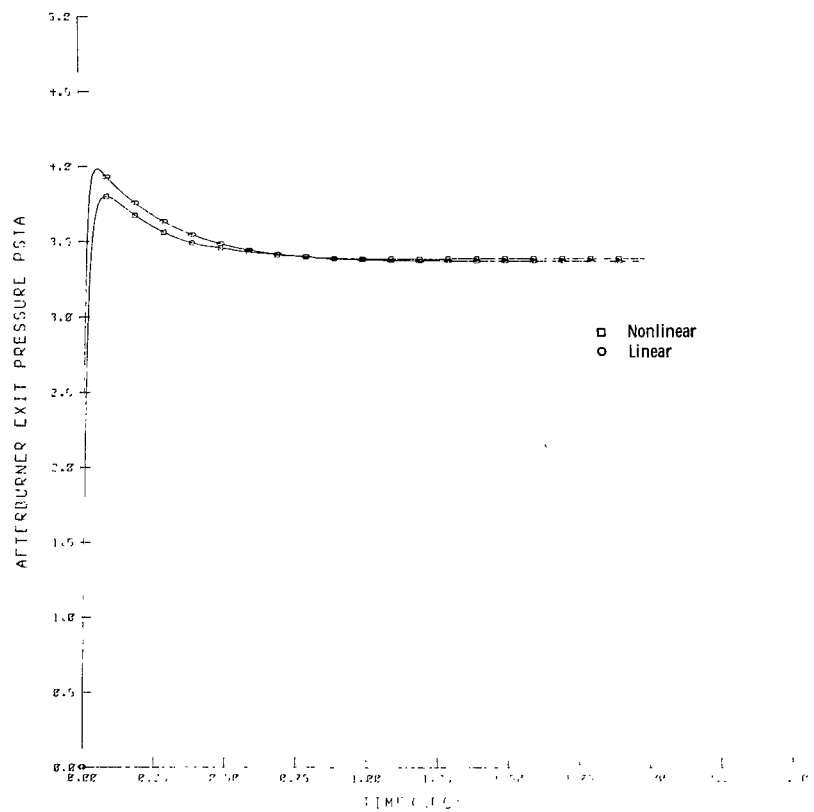
(b-1) With 3-percent step change in main fuel flow.



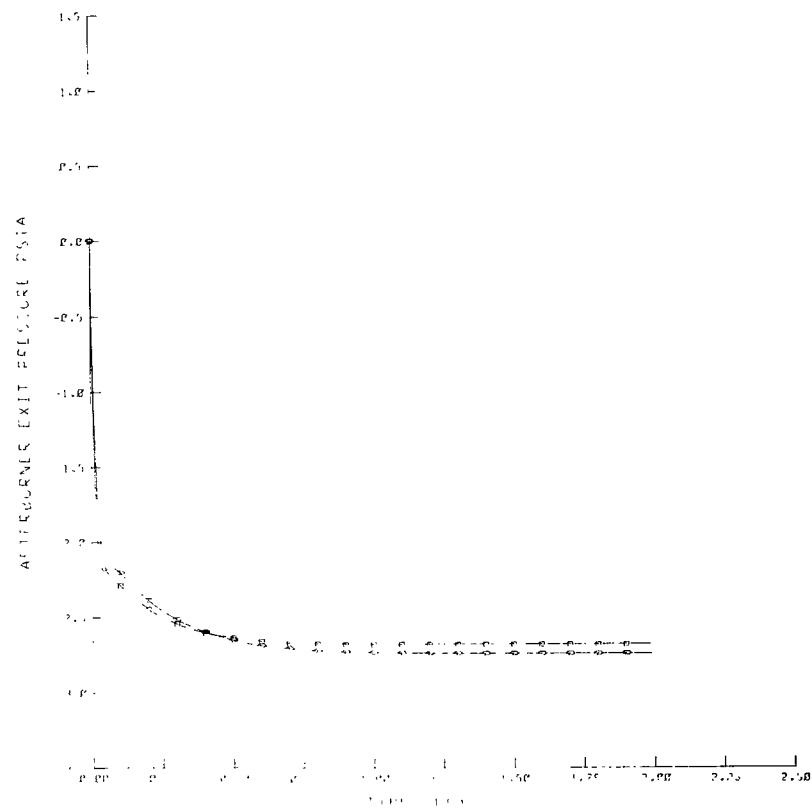
(b-2) With 3-percent step change in nozzle area.

(b) Comparison of reduced-order linear and nonlinear runs.

Figure 4. - Response of state 4 - compressor-exit internal energy.

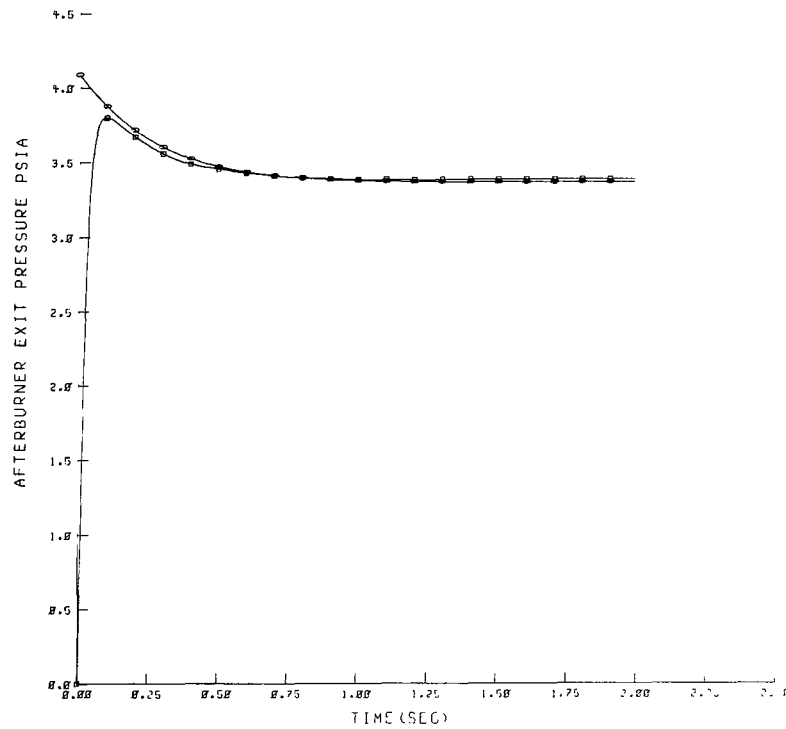


(a-1) With 3-percent step change in main fuel flow.

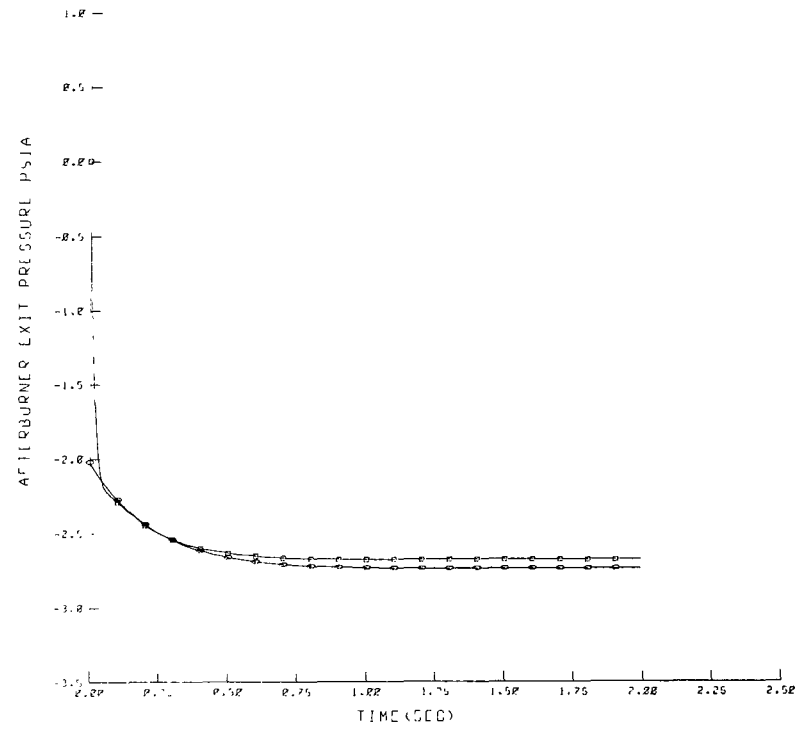


(a-2) With 3-percent step change in nozzle area.

(a) Comparison of full-order linear and nonlinear runs.



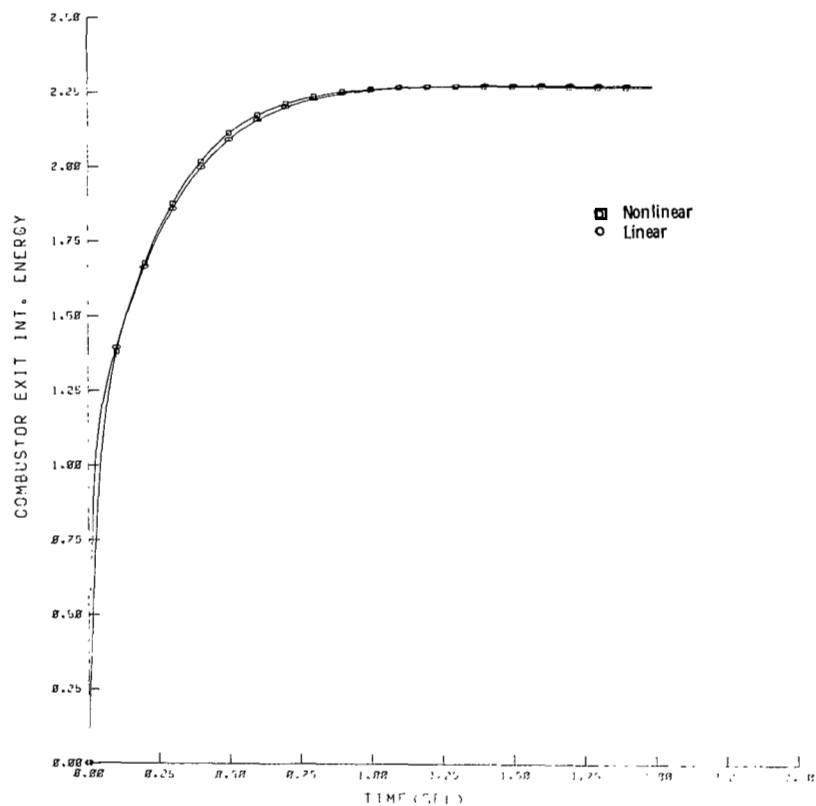
(b-1) With 3-percent step change in main fuel flow.



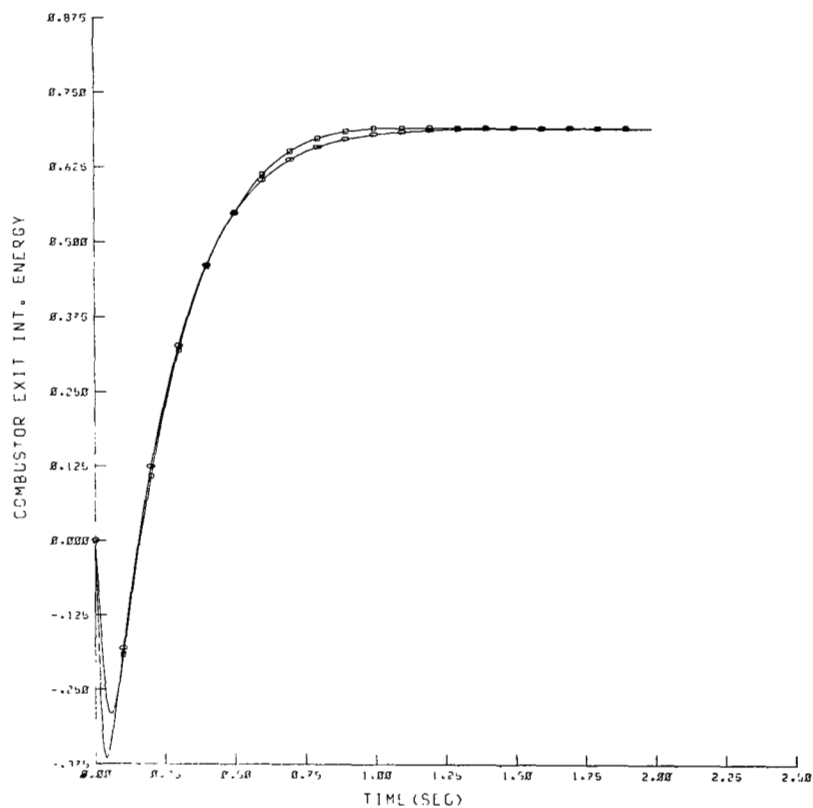
(b-2) With 3-percent step change in nozzle area.

(b) Comparison of reduced-order linear and nonlinear runs.

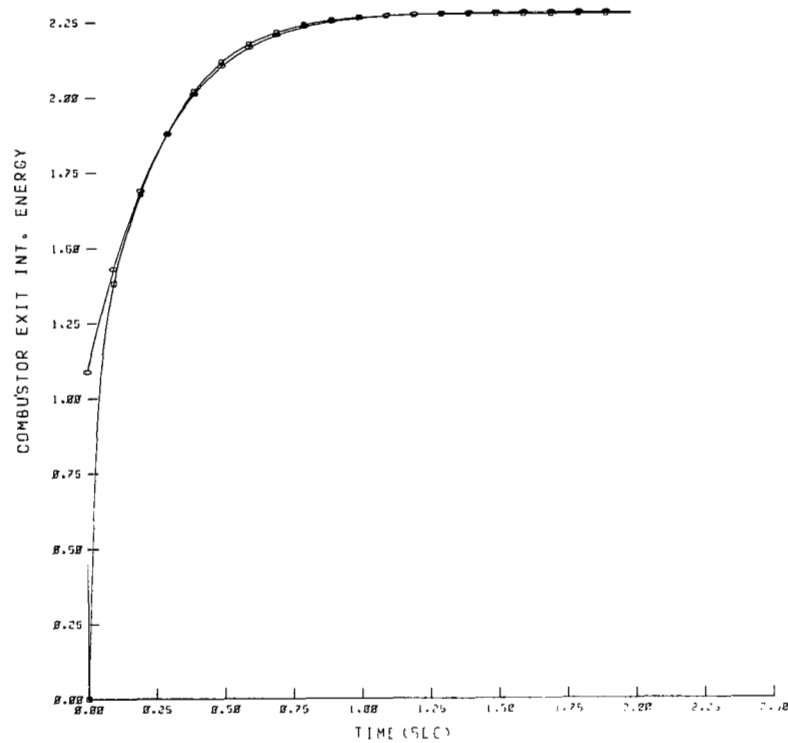
Figure 5. - Response of state 5 - afterburner-exit pressure.



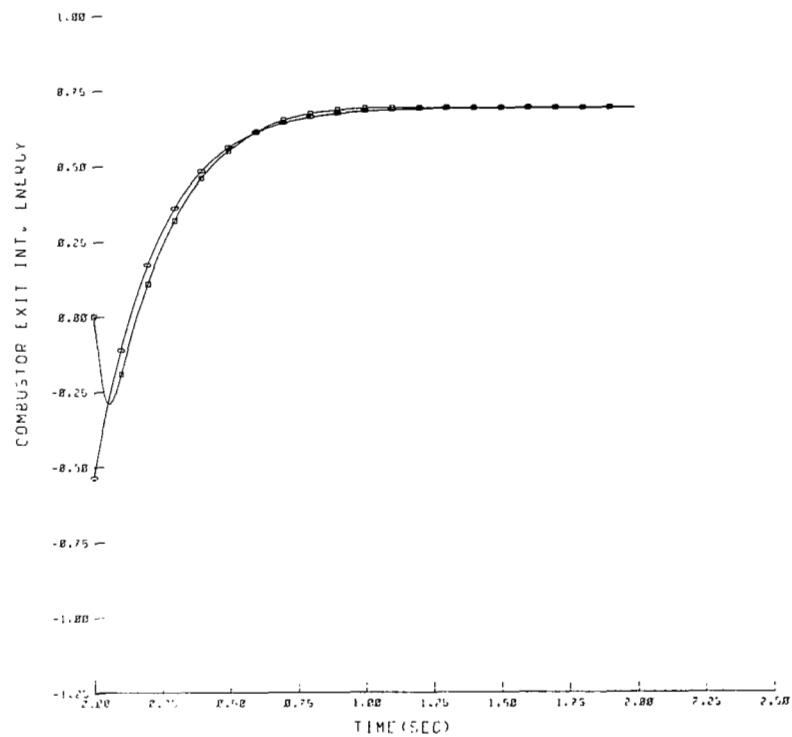
(a-1) With 3-percent step change in main fuel flow.



(a-2) With 3-percent step change in nozzle area.



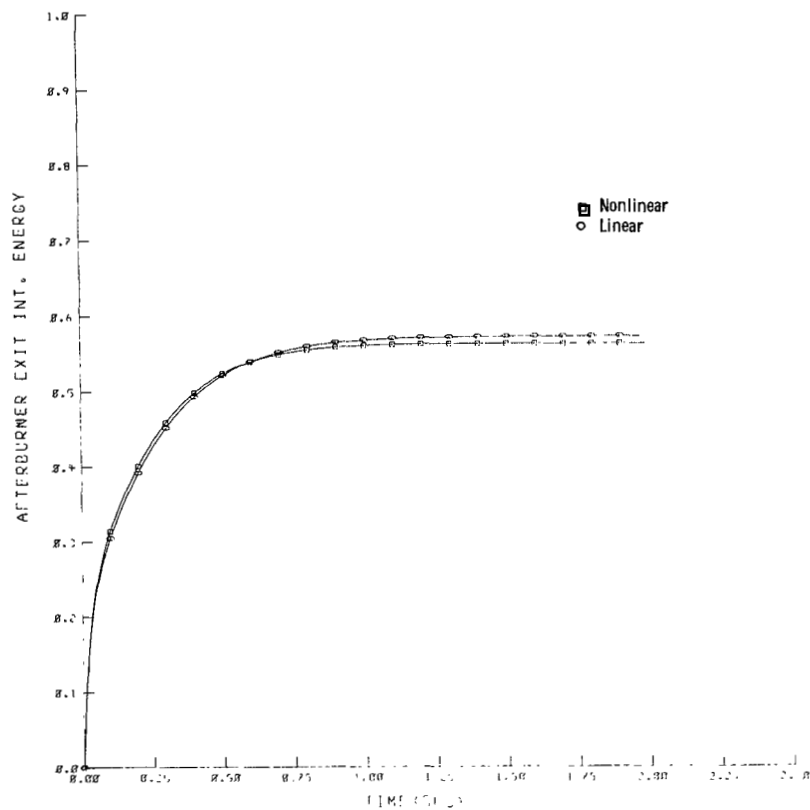
(b-1) With 3-percent step change in main fuel flow.



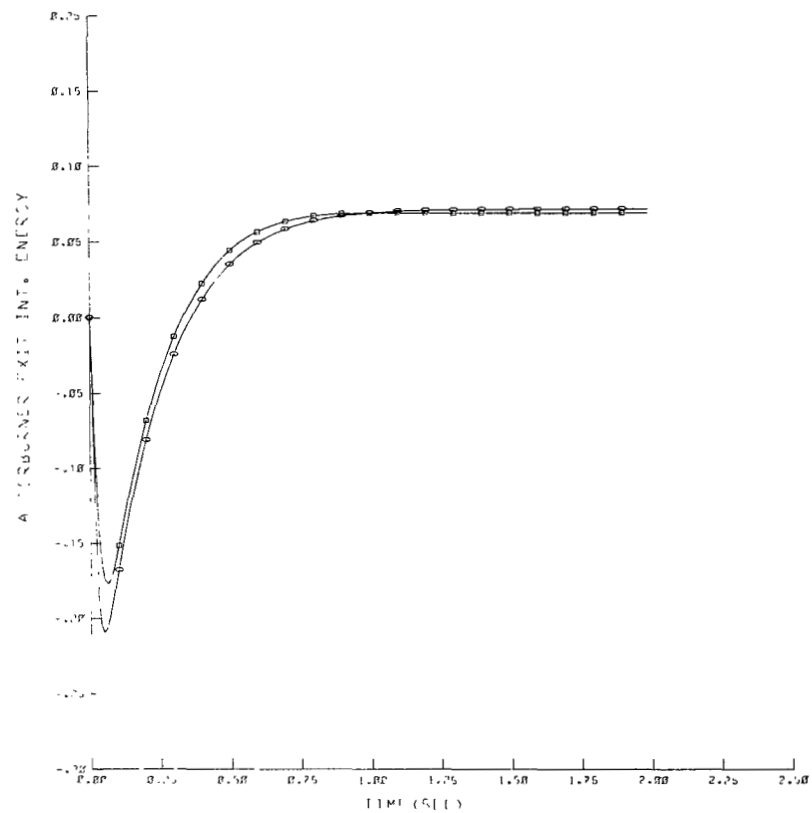
(b-2) With 3-percent step change in nozzle area.

(b) Comparison of reduced-order linear and nonlinear runs.

Figure 6. - Response of state 6 - combustor-exit internal energy.

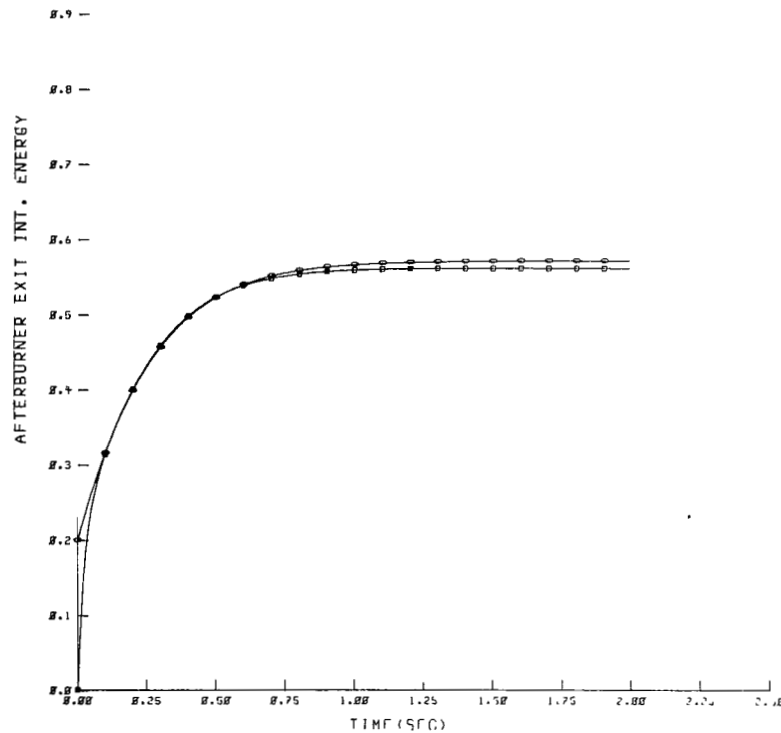


(a-1) With 3-percent step change in main fuel flow.

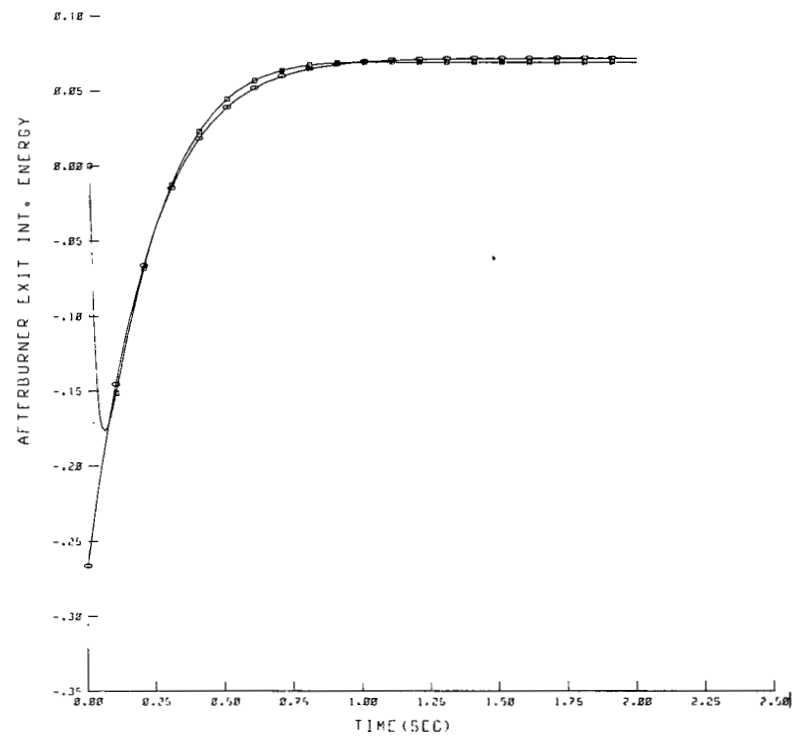


(a-2) With 3-percent step change in nozzle area.

(a) Comparison of full-order linear and nonlinear response



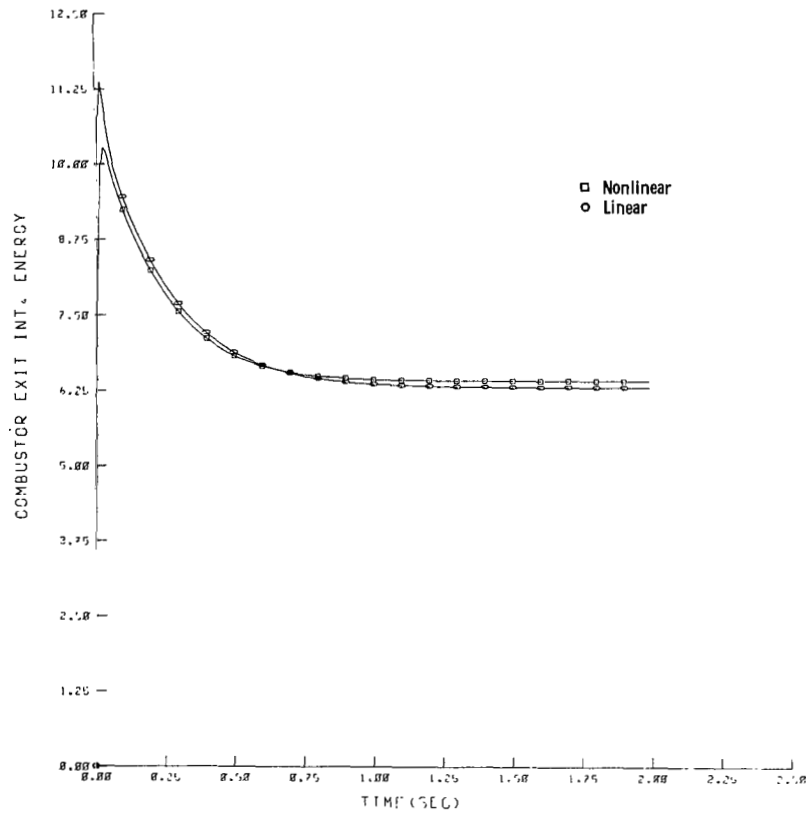
(a-1) With 3-percent step change in main fuel flow.



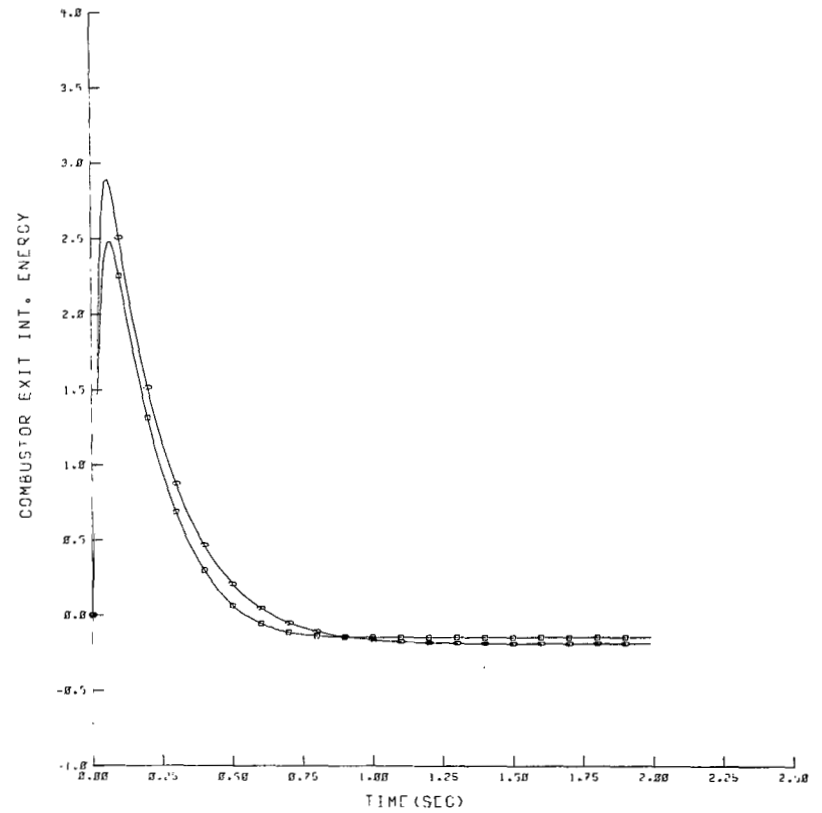
(a-2) With 3-percent step change in nozzle area.

(b) Comparison of reduced-order linear and nonlinear runs.

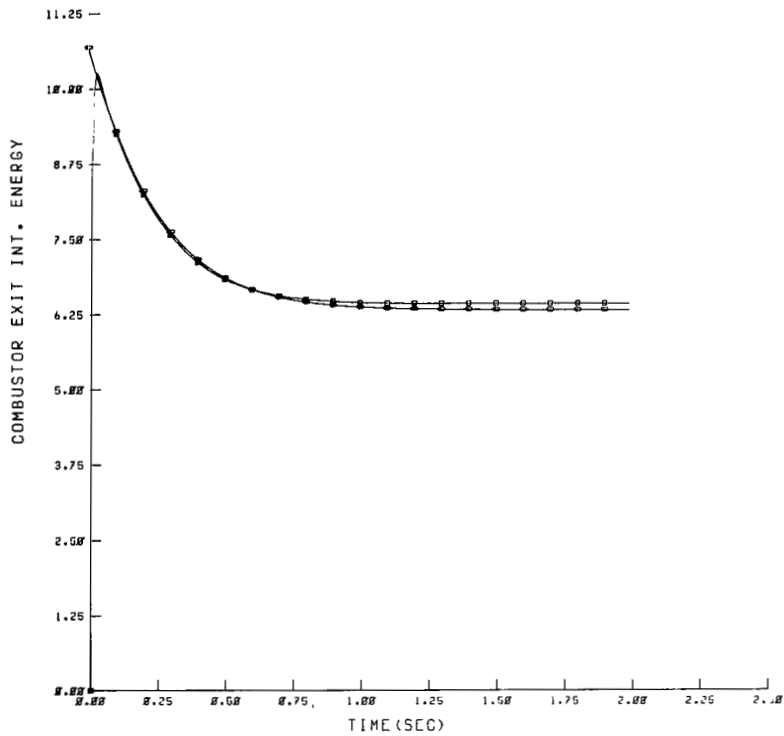
Figure 7. - Response of state 7 - afterburner-exit internal energy.



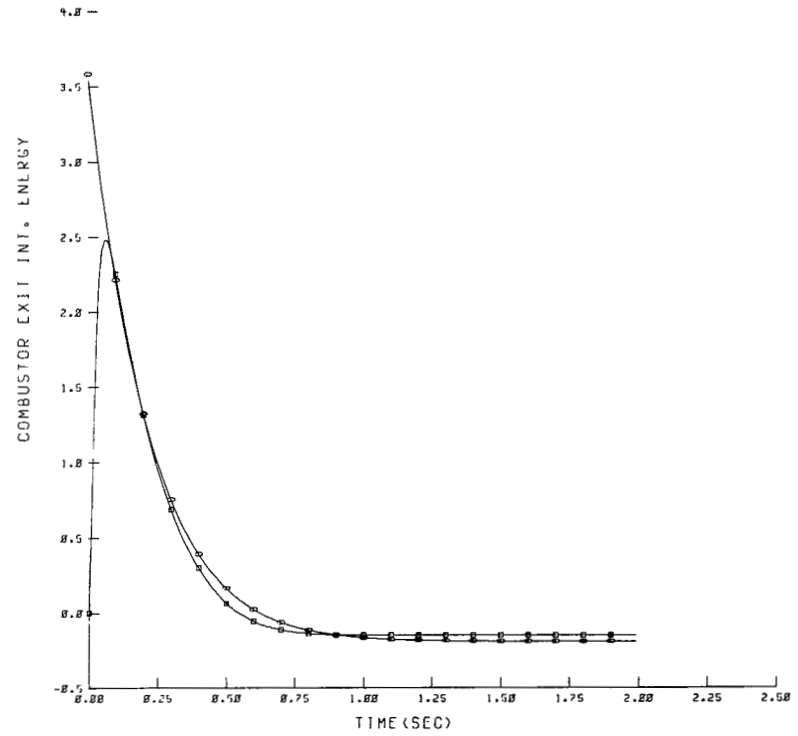
(a-1) With 3-percent step change in main fuel flow.



(a-2) With 3-percent step change in nozzle area.



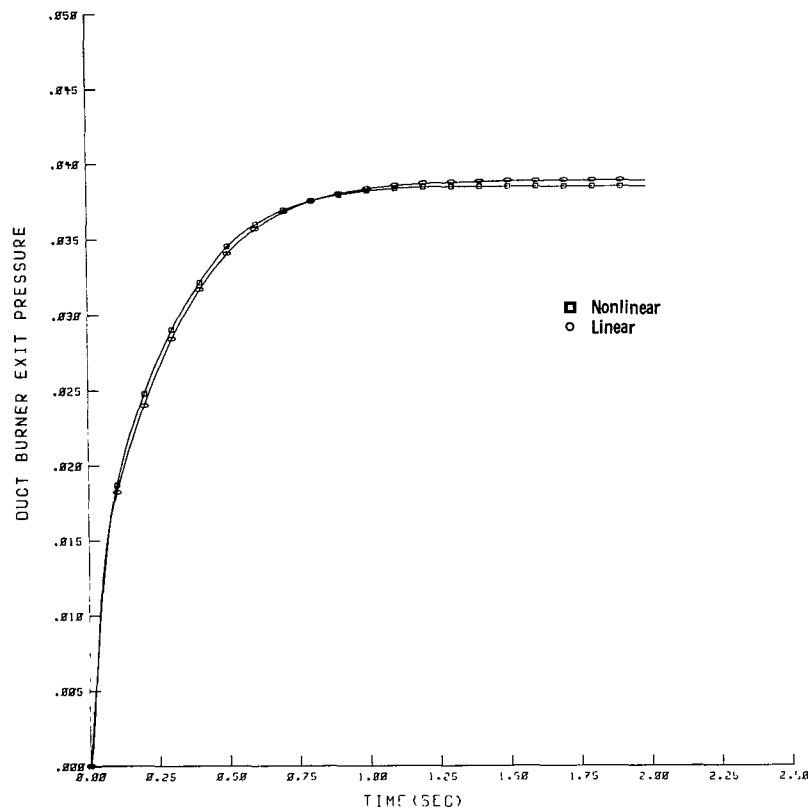
(b-1) With 3-percent step change in main fuel flow.



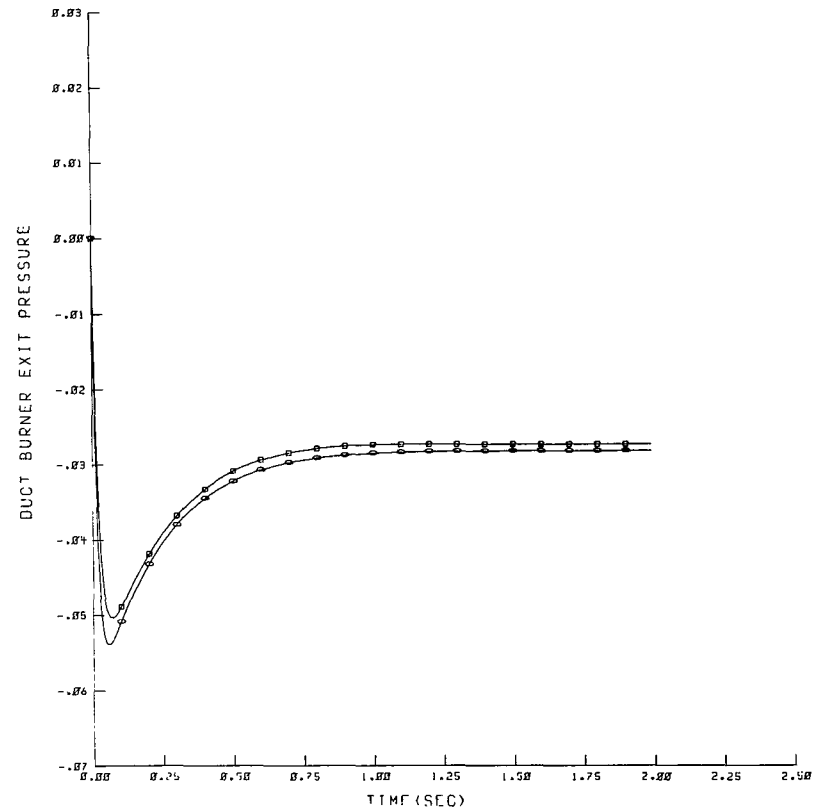
(b-2) With 3-percent step change in nozzle area.

(b) Comparison of reduced-order linear and nonlinear runs.

Figure 8. - Response of state 8 - combustor-exit internal energy.

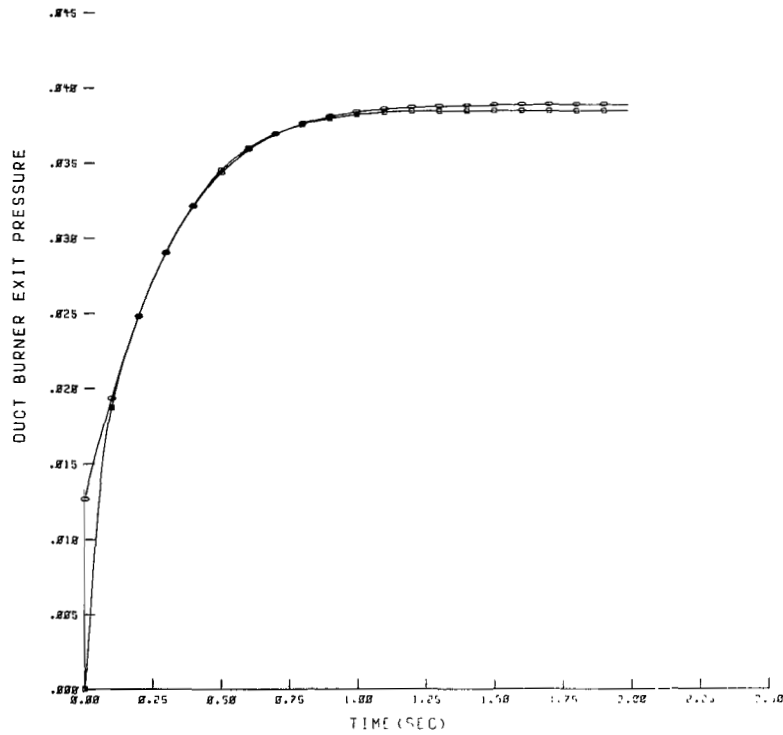


(a-1) With 3-percent step change in main fuel flow.

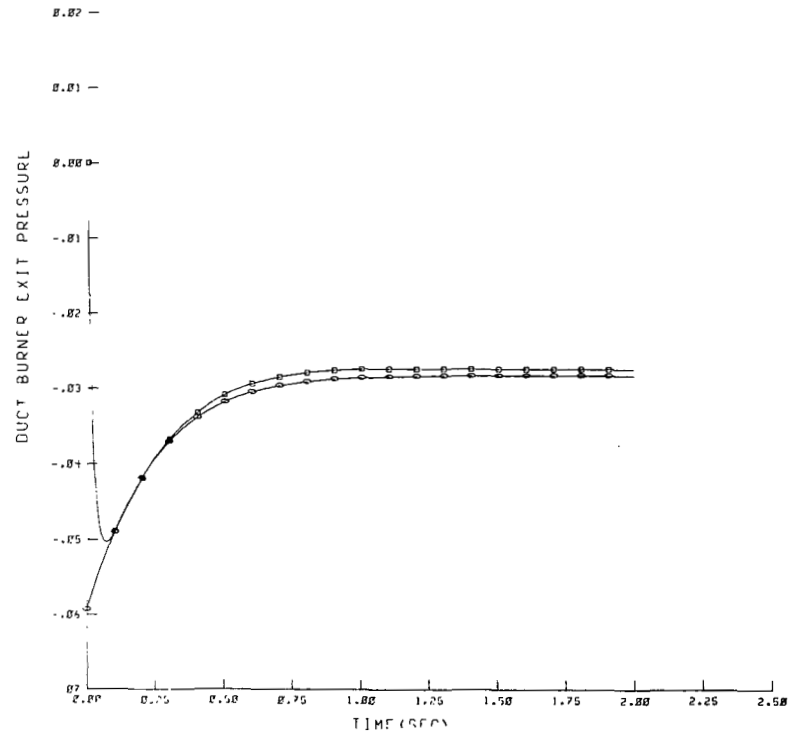


(a-2) With 3-percent step change in nozzle area.

(a) Comparison of full-order linear and nonlinear runs.



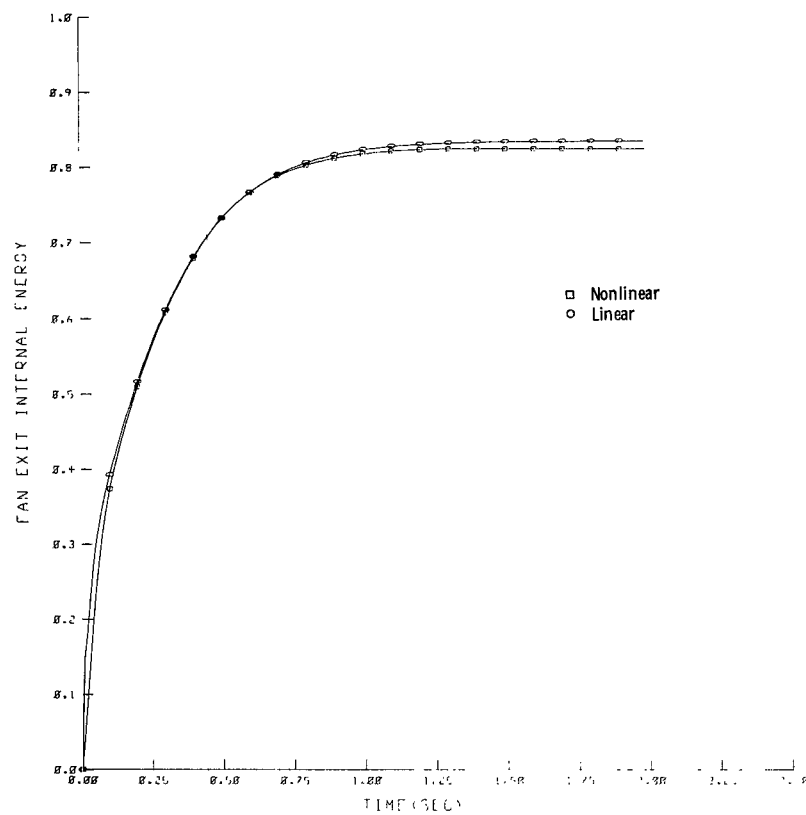
(b-1) With 3-percent step change in main fuel flow.



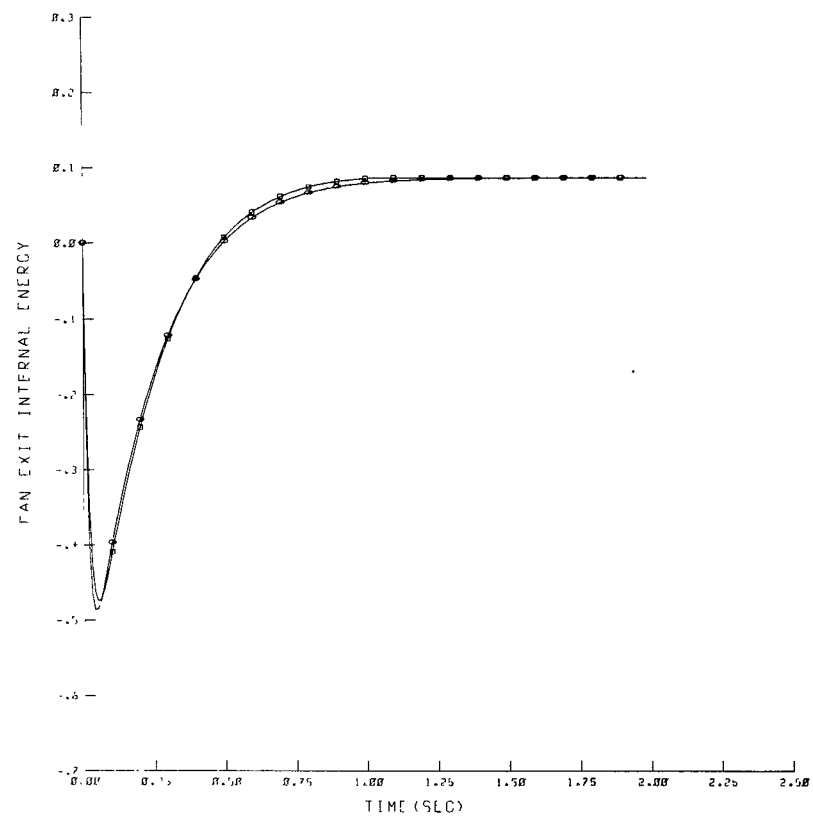
(b-2) With 3-percent step change in nozzle area.

(b) Comparison of reduced-order linear and nonlinear runs.

Figure 9. - Response of state 9 - duct-burner-exit pressure.

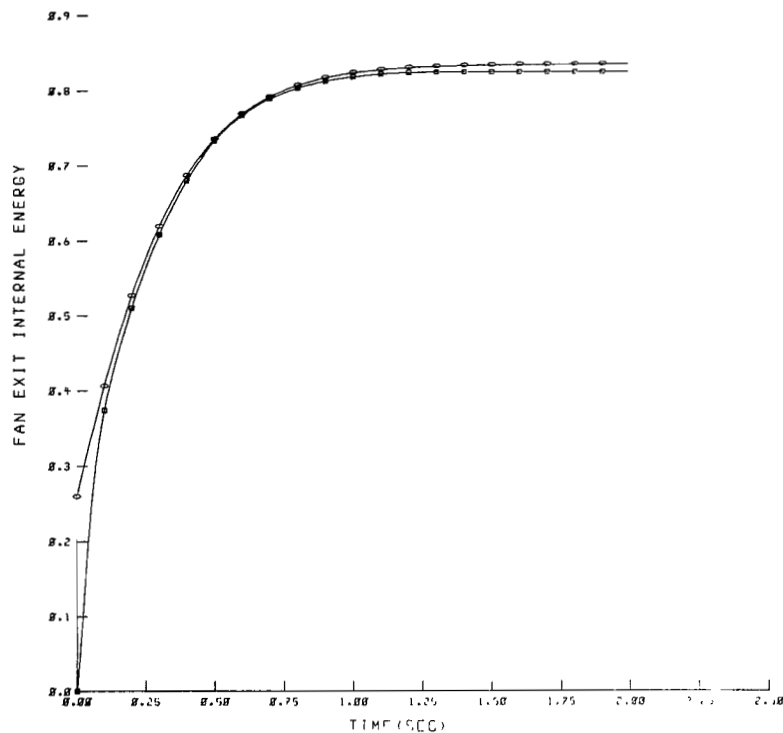


(a-1) With 3-percent step change in main fuel flow.

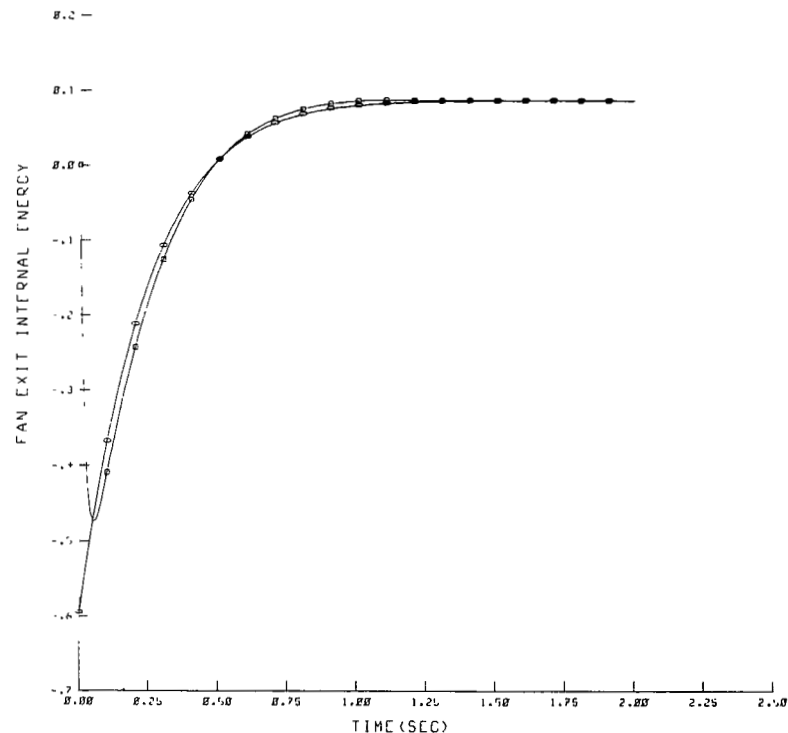


(a-2) With 3-percent step change in nozzle area.

(a) Comparison of full-order linear and nonlinear runs.



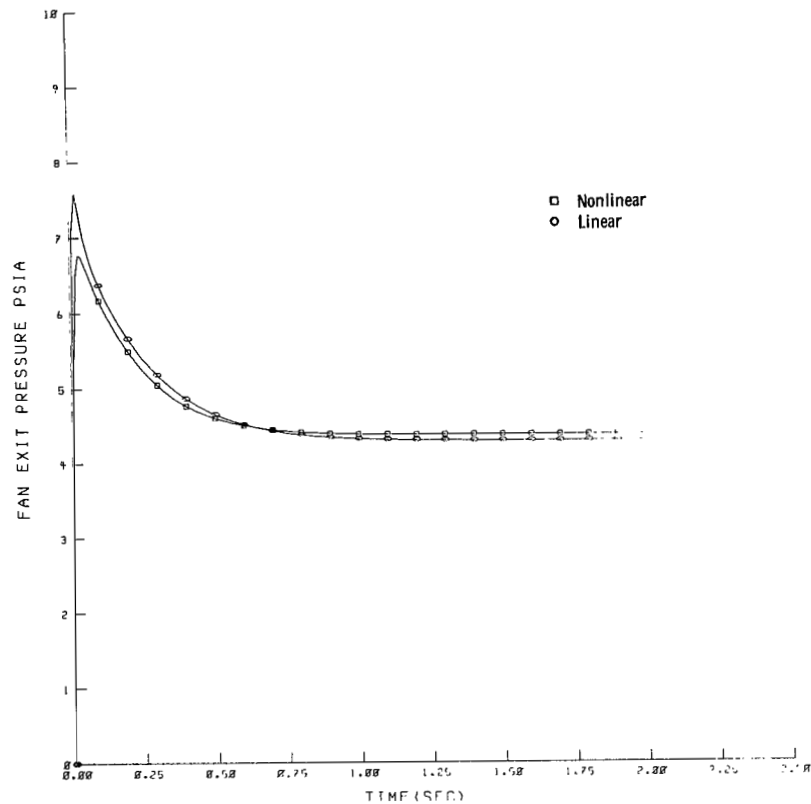
(b-1) With 3-percent step change in main fuel flow.



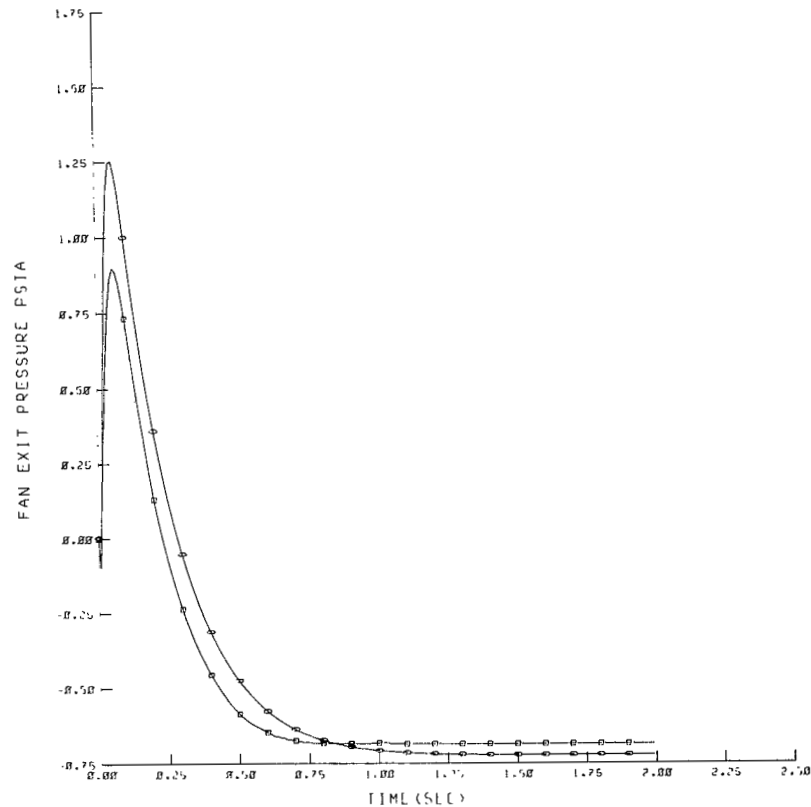
(b-2) With 3-percent step change in nozzle area.

(b) Comparison of reduced-order linear and nonlinear runs.

Figure 10. - Response of state 10 - fan-exit internal energy.

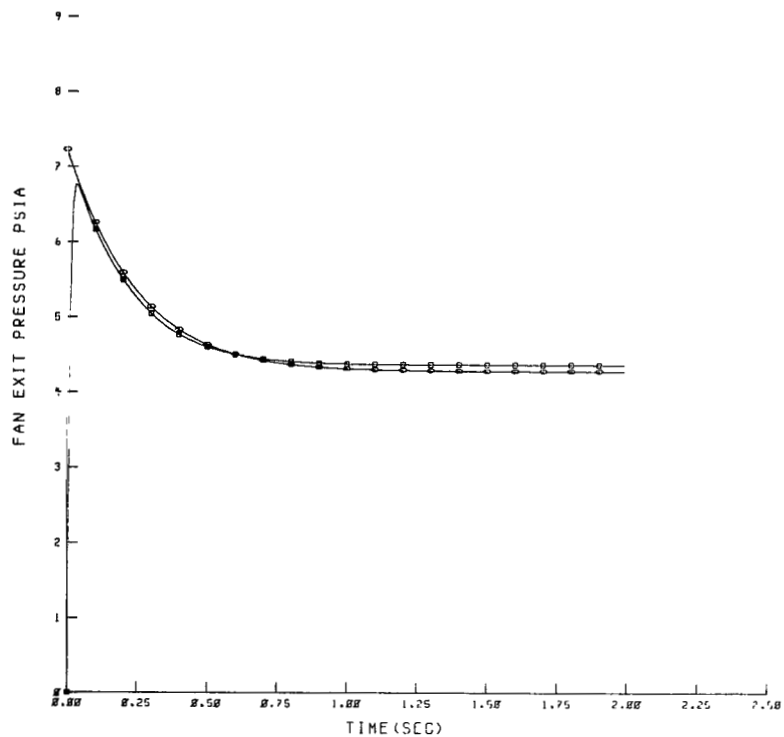


(a-1) With 3-percent step change in main fuel flow.

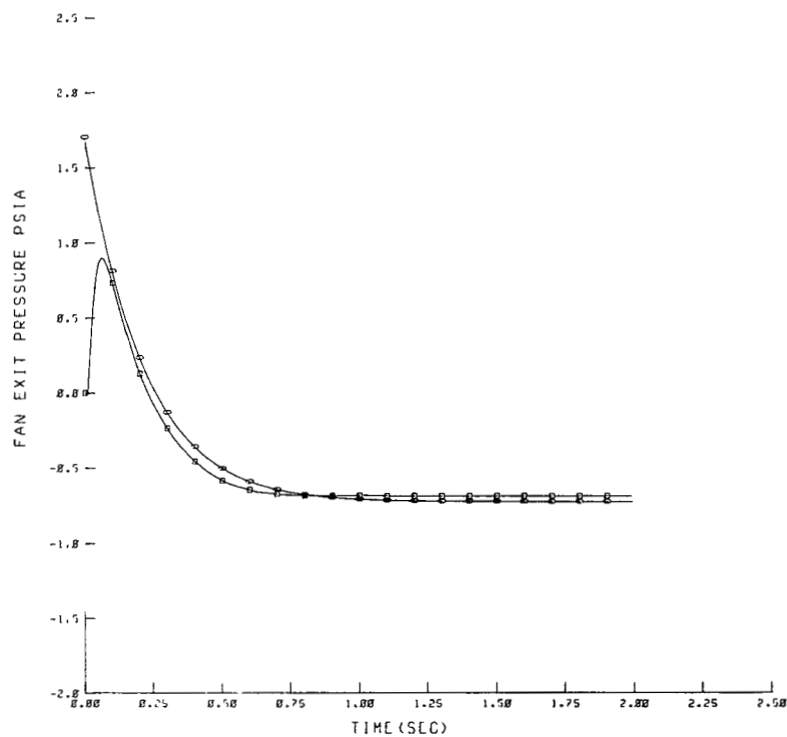


(a-2) With 3-percent step change in nozzle area.

(a) Comparison of full-order linear and nonlinear runs.



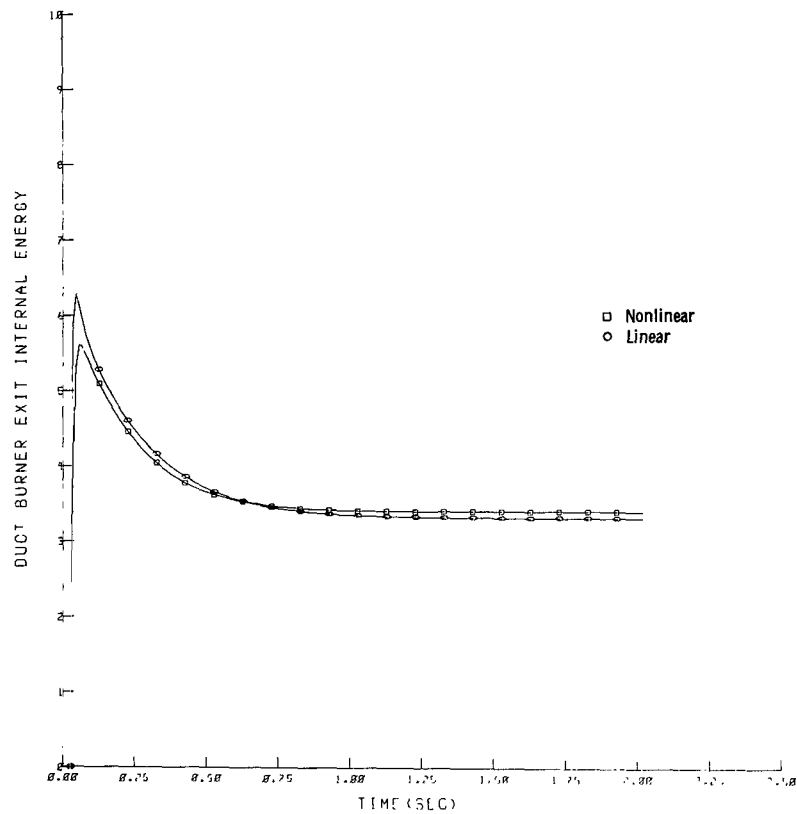
(b-1) With 3-percent step change in main fuel flow.



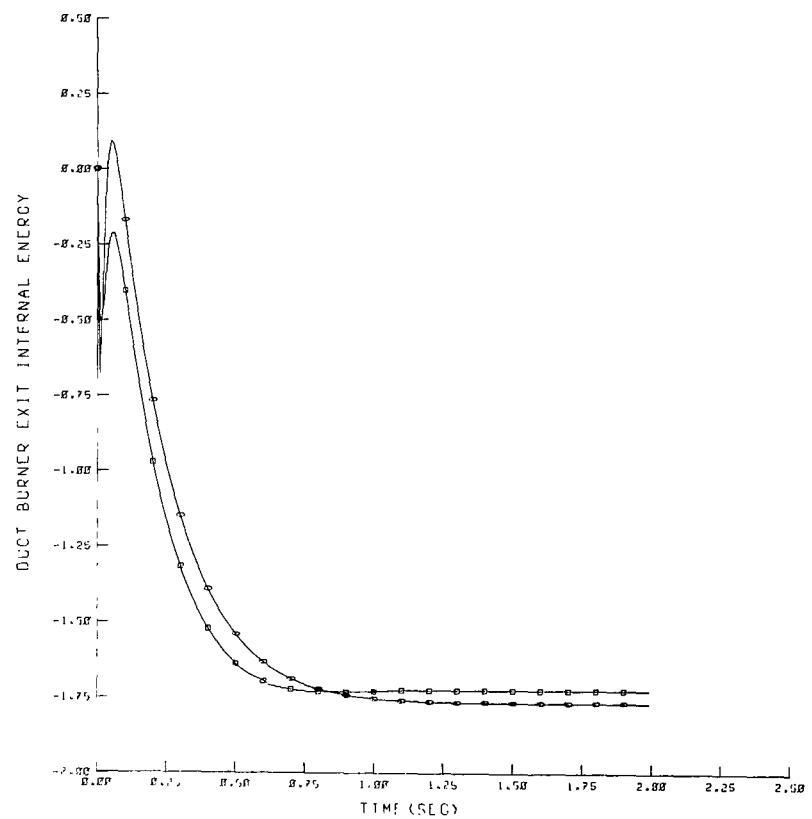
(b-2) With 3-percent step change in nozzle area.

(b) Comparison of reduced-order linear and nonlinear runs.

Figure 11. - Response of state 11 - fan-exit pressure.

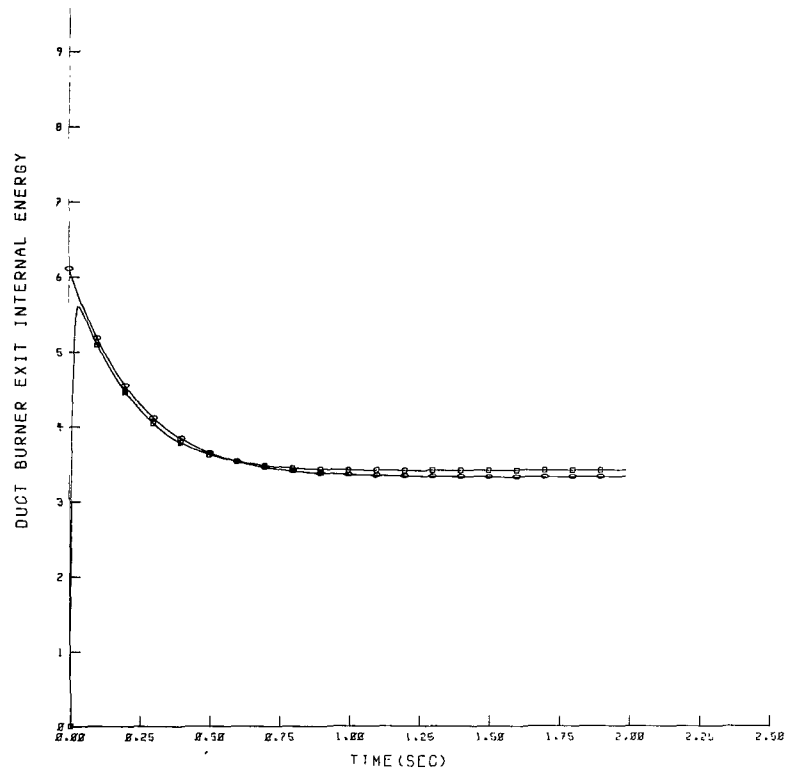


(a-1) With 3-percent step change in main fuel flow.

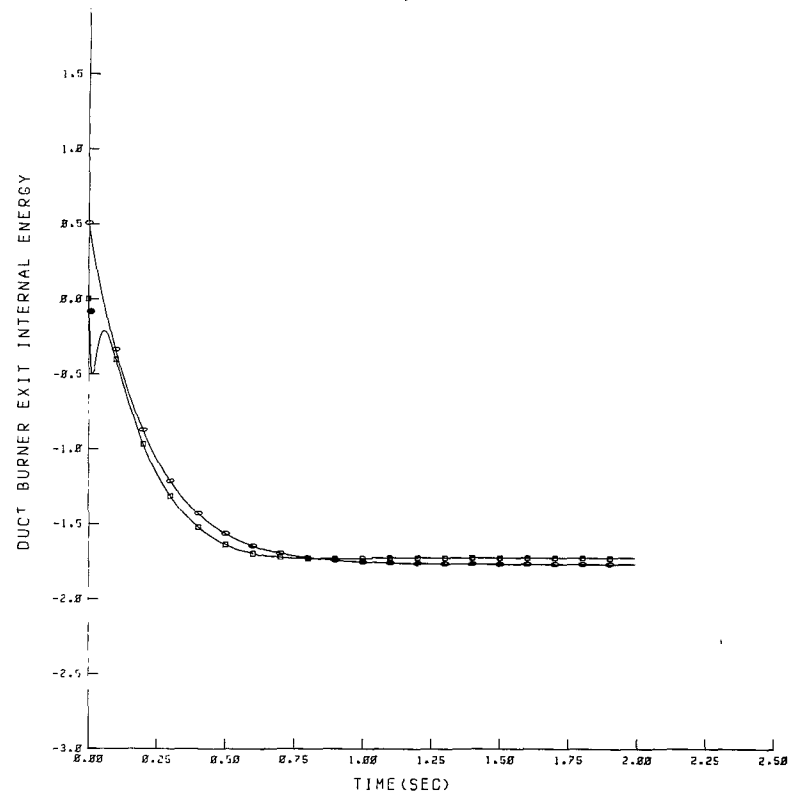


(a-2) With 3-percent step change in nozzle area.

(a) Comparison with 11-order linear and nonlinear runs.



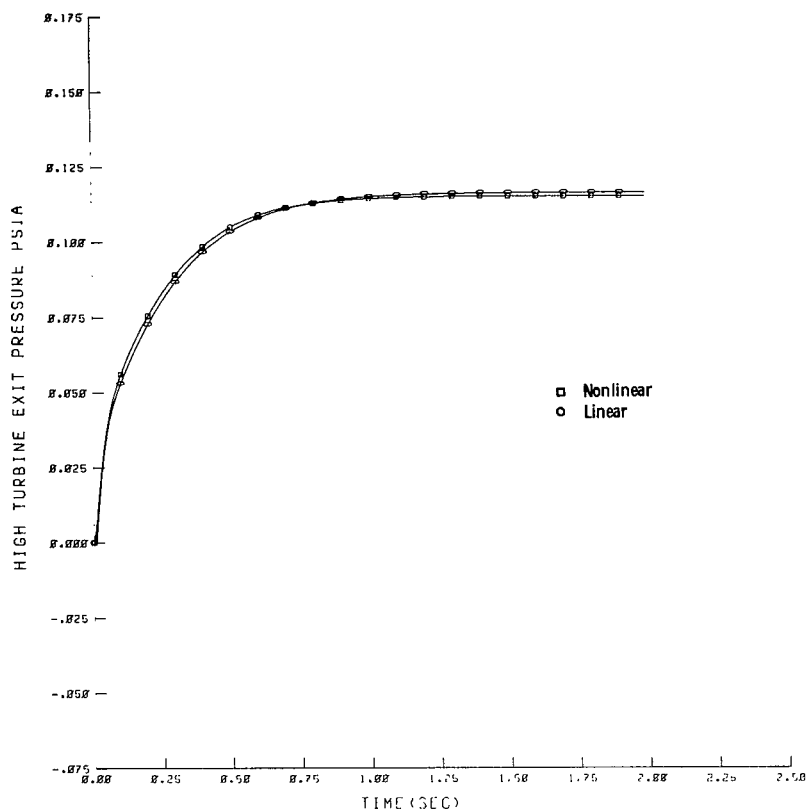
(b-1) With 3-percent step change in main fuel flow.



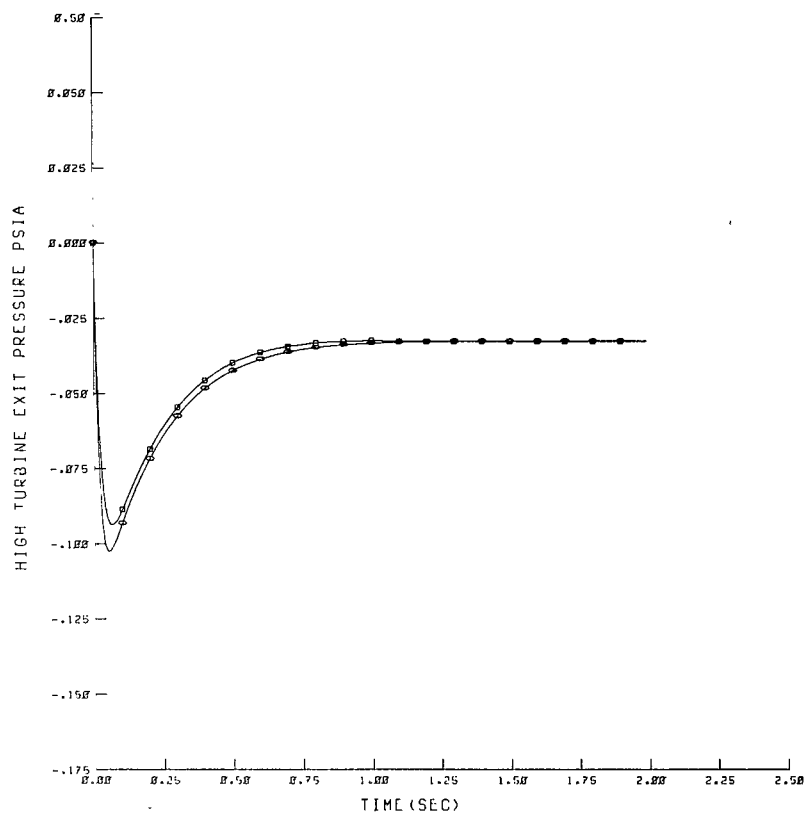
(b-2) With 3-percent step change in nozzle area.

(b) Comparison of reduced-order linear and nonlinear runs.

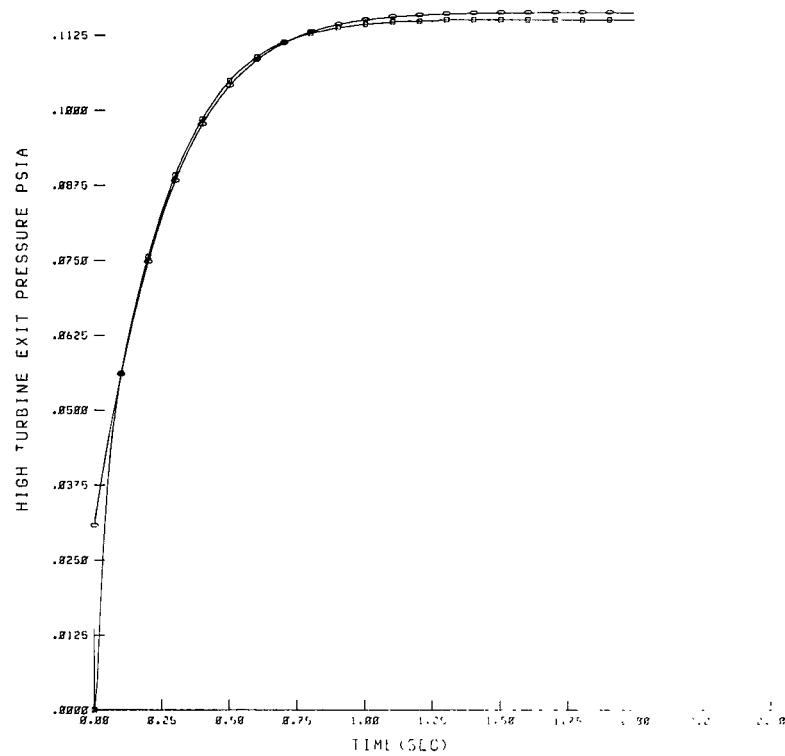
Figure 12. - Response of state 12 - duct-burner-exit internal energy.



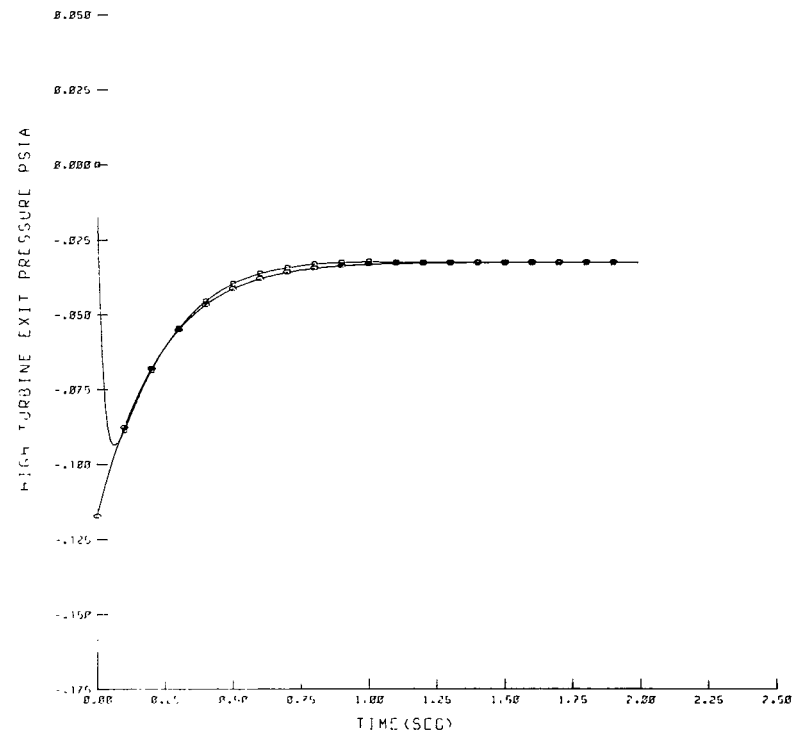
(a-1) With 3-percent step change in main fuel flow.



(a-2) With 3-percent step change in nozzle area.

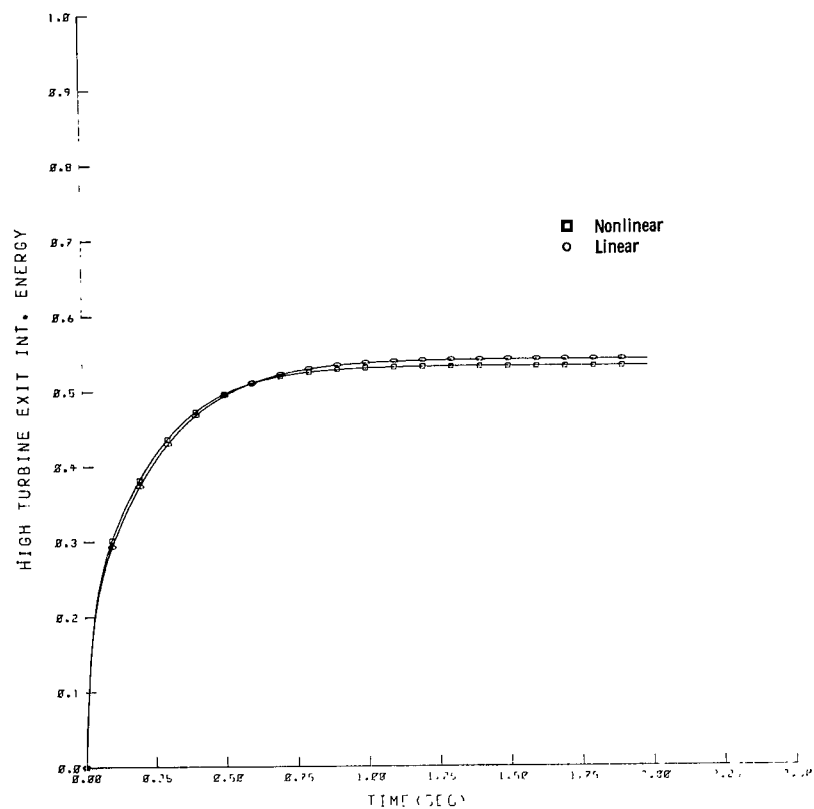


(b-1) With 3-percent step change in main fuel flow.

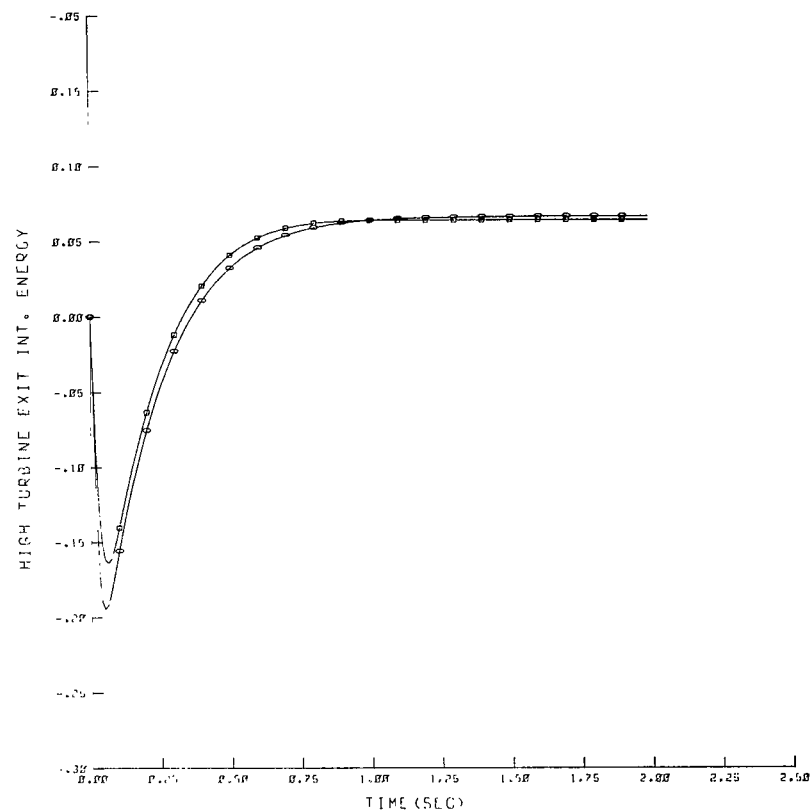


(b-2) With 3-percent step change in nozzle area.

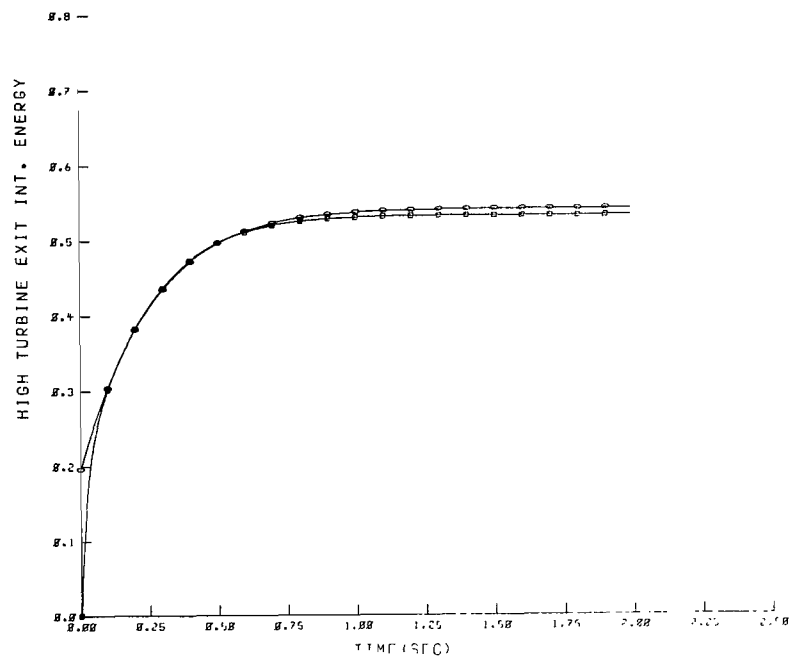
(b) Comparison of reduced-order linear and nonlinear runs.
Figure 13. - Response of state 13 - high turbine-exit pressure.



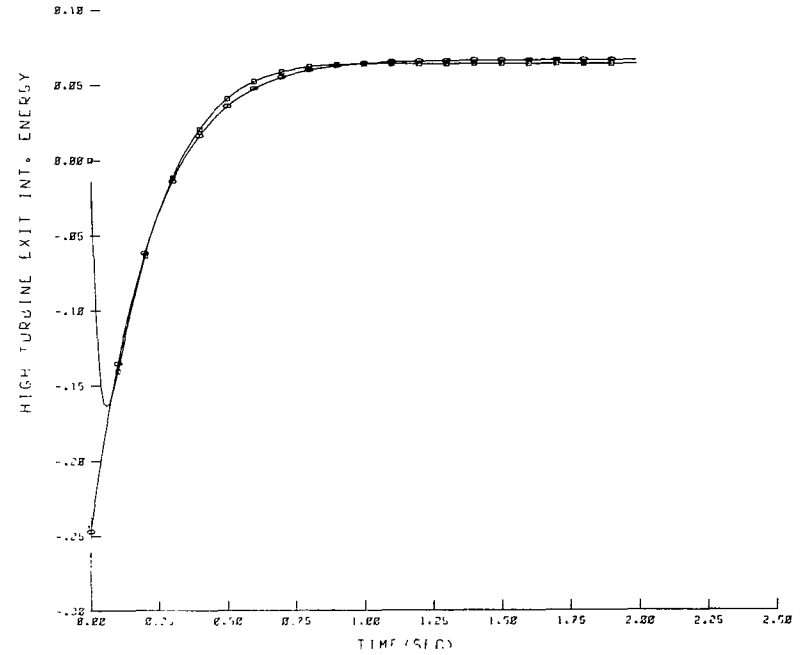
(a-1) With 3-percent step change in main fuel flow.



(a-2) With 3-percent step change in nozzle area.



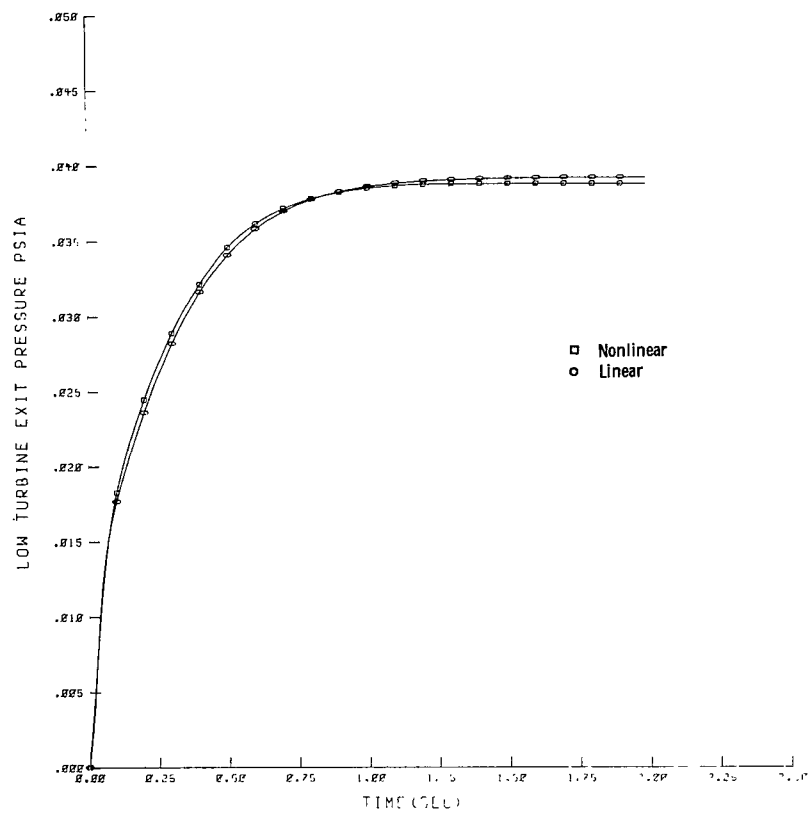
(b-1) With 3-percent step change in main fuel flow.



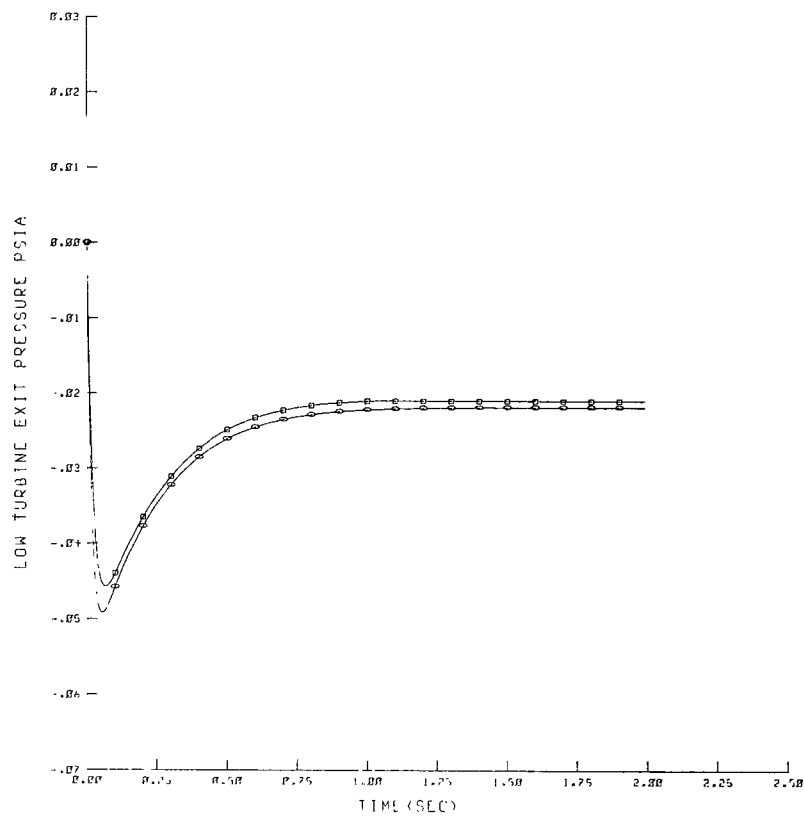
(b-2) With 3-percent step change in nozzle area.

(b) Comparison of reduced-order linear and nonlinear runs.

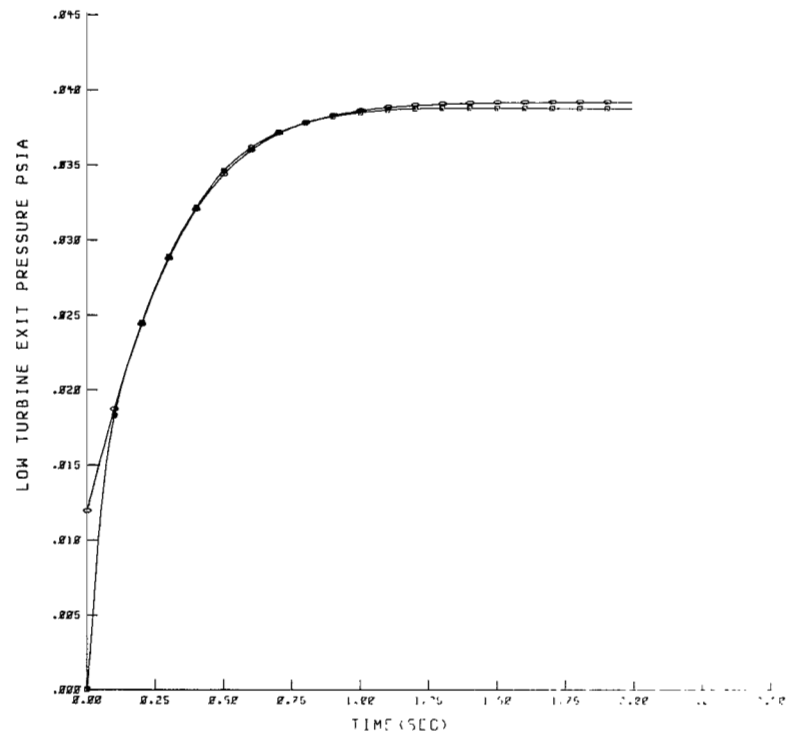
Figure 14. - Response of state 14 - high turbine-exit internal energy.



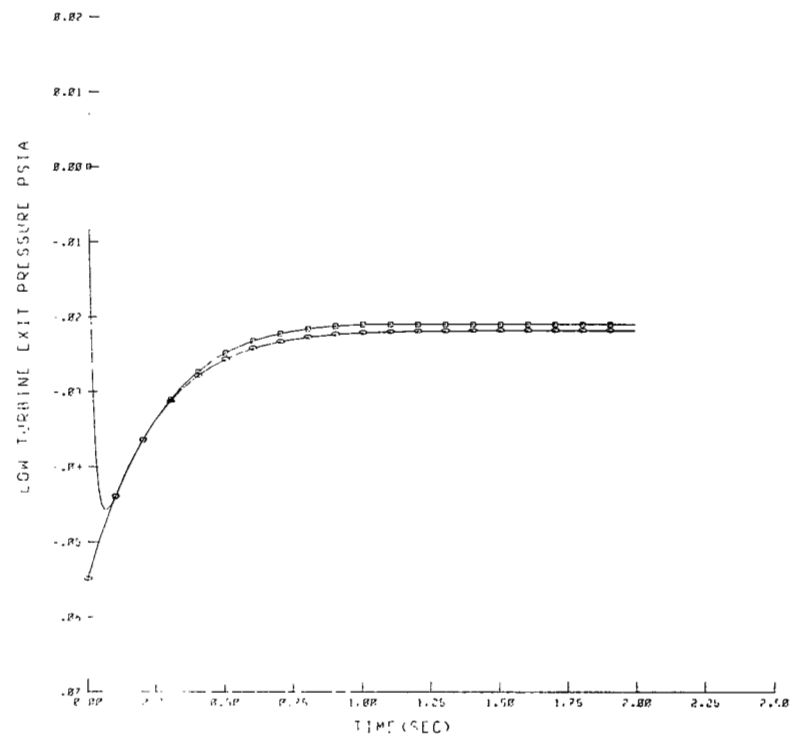
(a-1) With 3-percent step change in main fuel flow.



(a-2) With 3-percent step change in nozzle area.



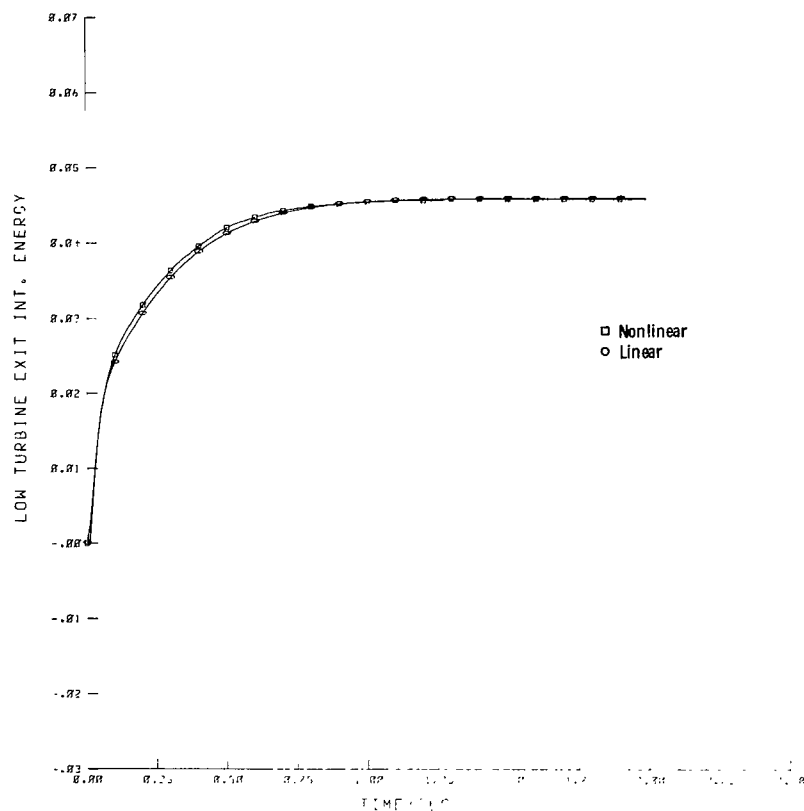
(b-1) With 3-percent step change in main fuel flow.



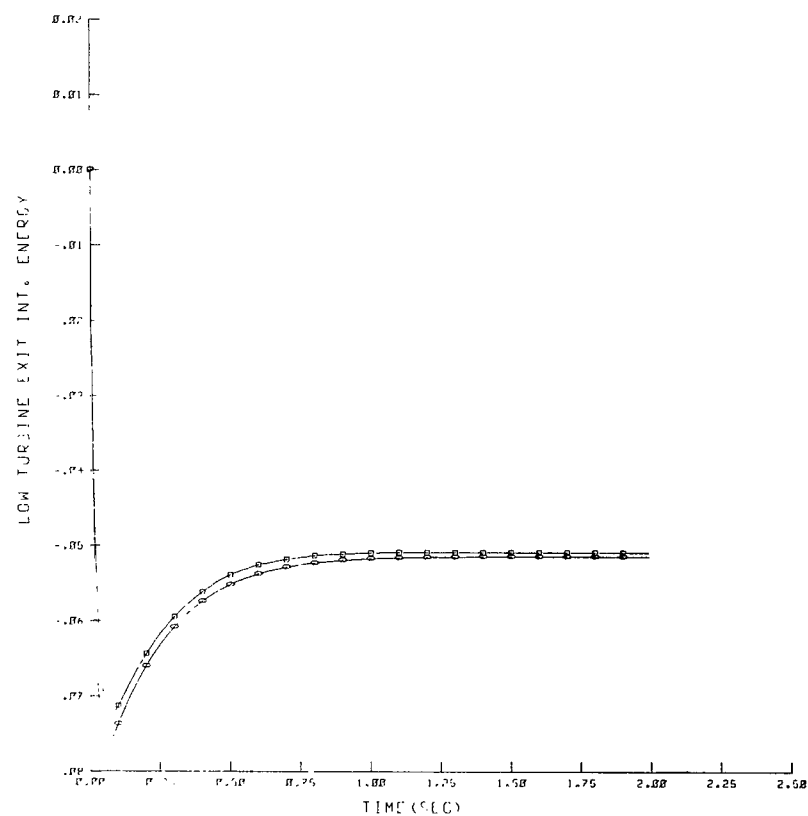
(b-2) With 3-percent step change in nozzle area.

(b) Comparison of reduced-order linear and nonlinear runs.

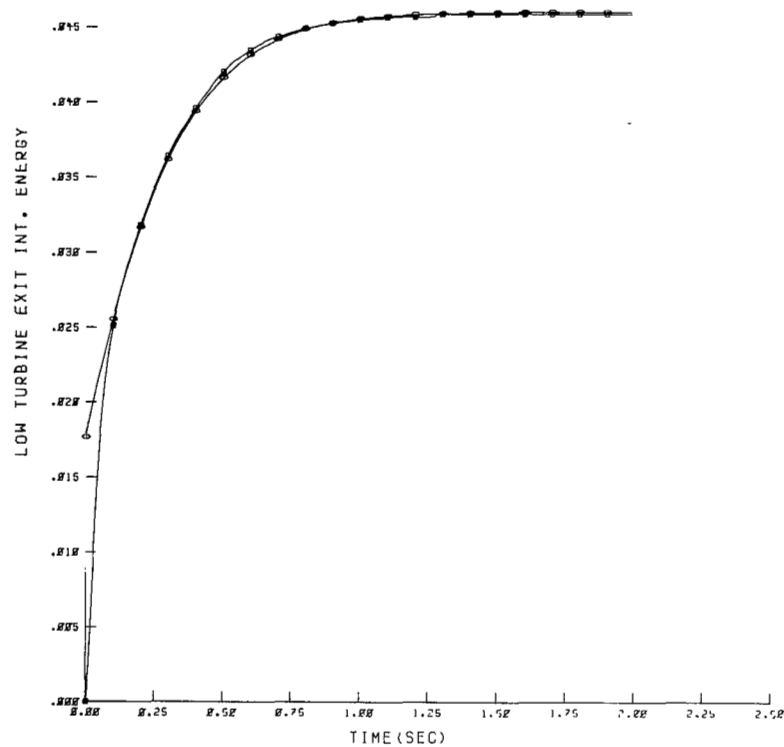
Figure 15. - Response of state 15 - low turbine-exit pressure.



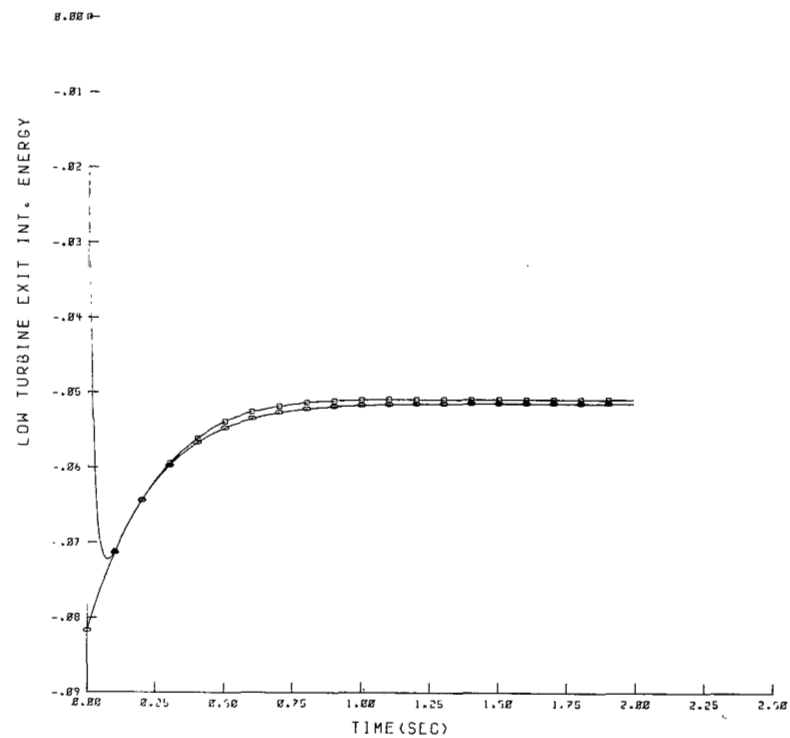
(a-1) With 3-percent step change in main fuel flow.



(a-2) With 3-percent step change in nozzle area.



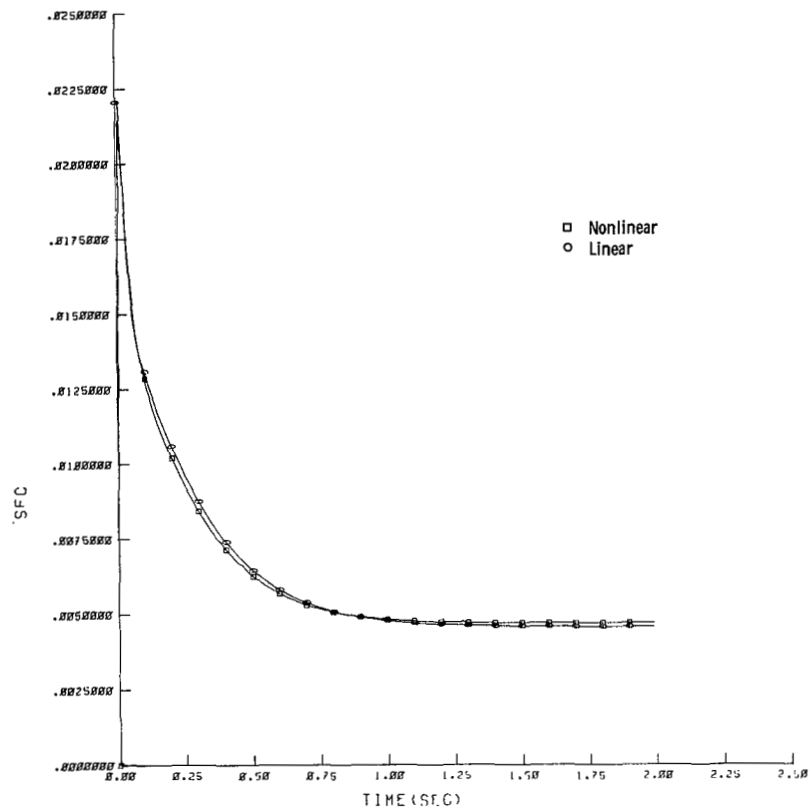
(b-1) With 3-percent step change in main fuel flow.



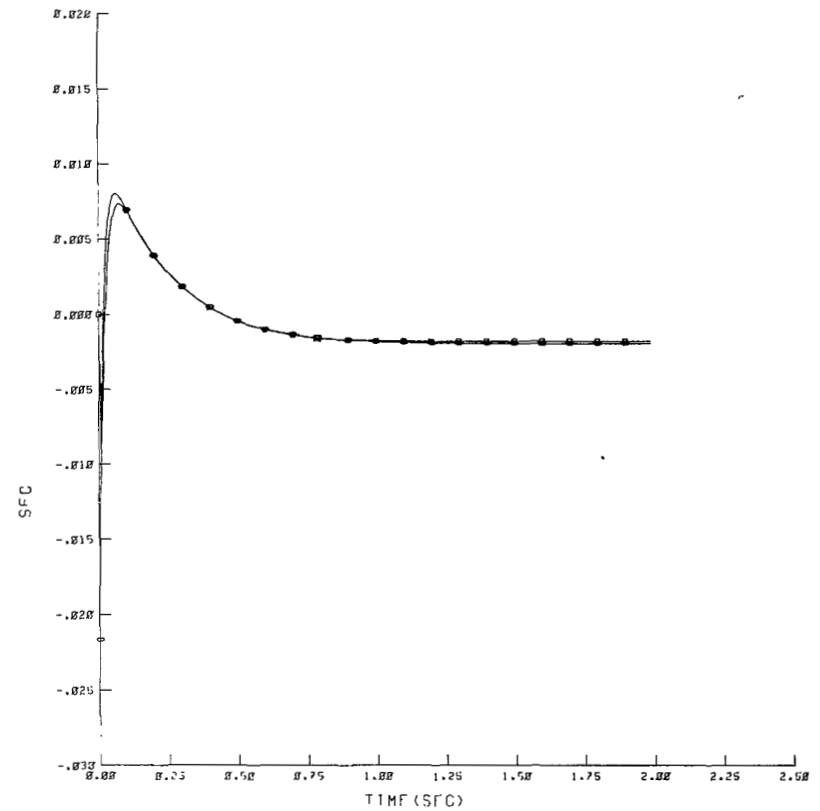
(b-2) With 3-percent step change in nozzle area.

(b) Comparison of reduced-order linear and nonlinear runs.

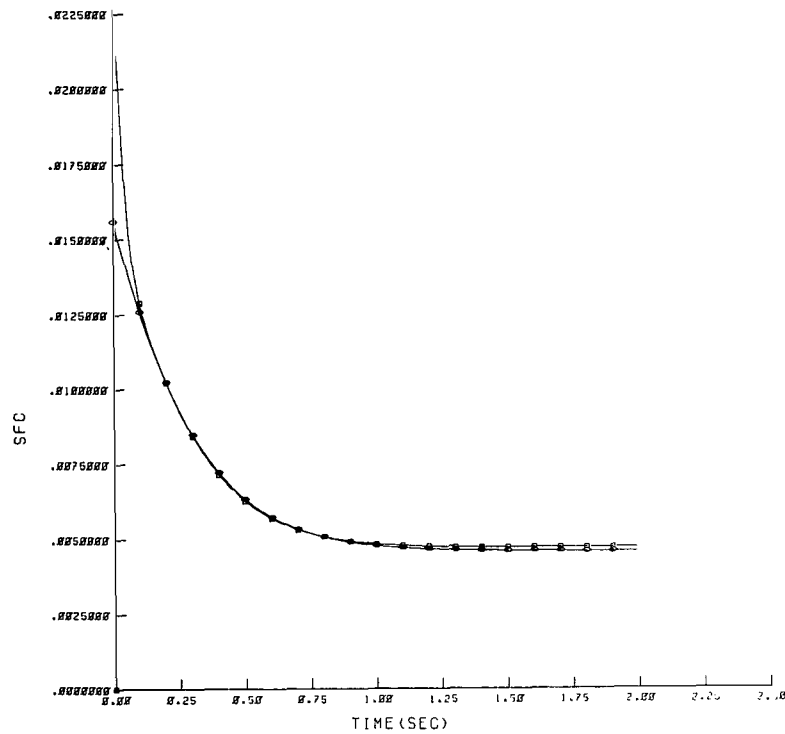
Figure 16. - Response of state 16 - low turbine-exit internal energy.



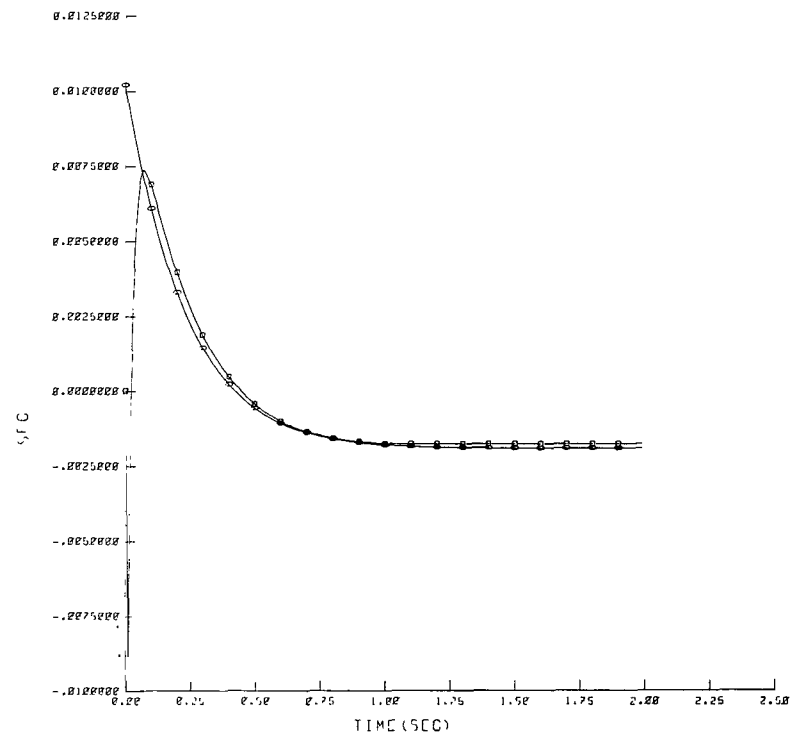
(a-1) With 3-percent step change in main fuel flow.



(a-2) With 3-percent step change in nozzle area.



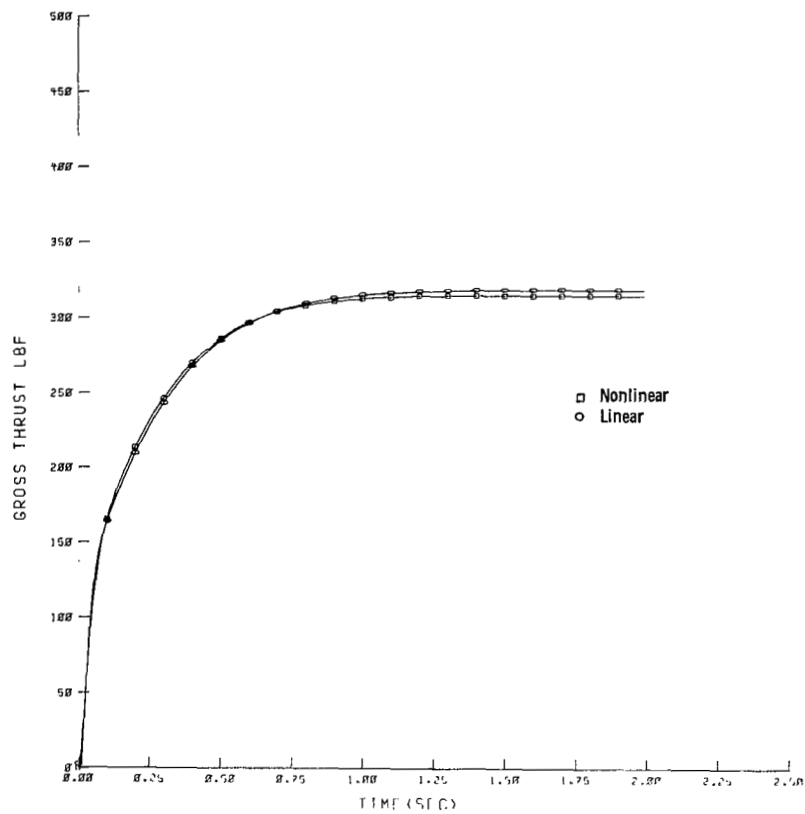
(b-1) With 3-percent step change in main fuel flow.



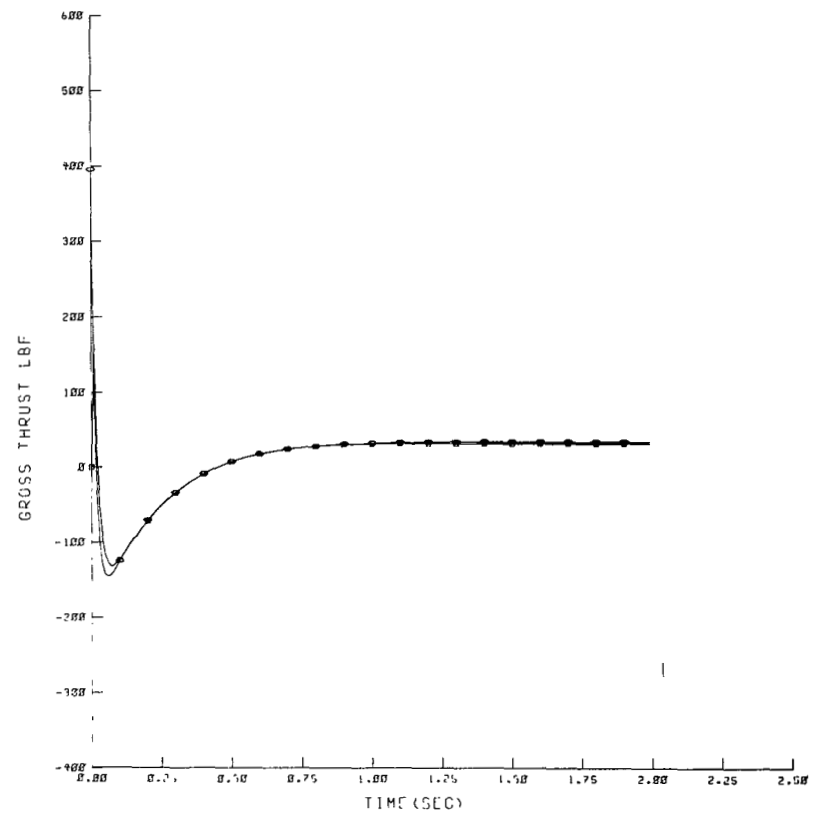
(b-2) With 3-percent step change in nozzle area.

(b) Comparison of reduced-order linear and nonlinear runs.

Figure 17. - Response of output 1 - specific fuel consumption.

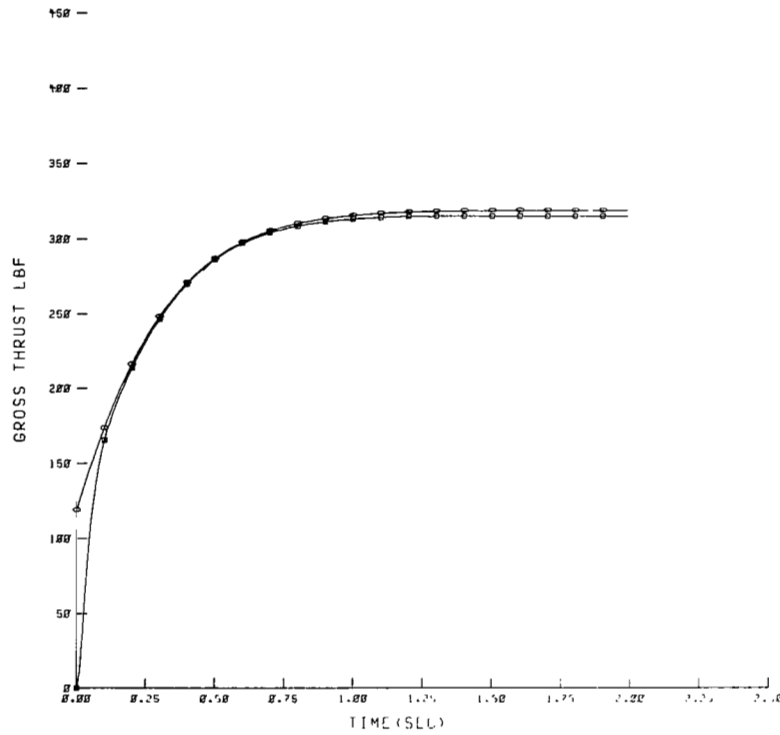


(a-1) With 3-percent step change in main fuel flow.

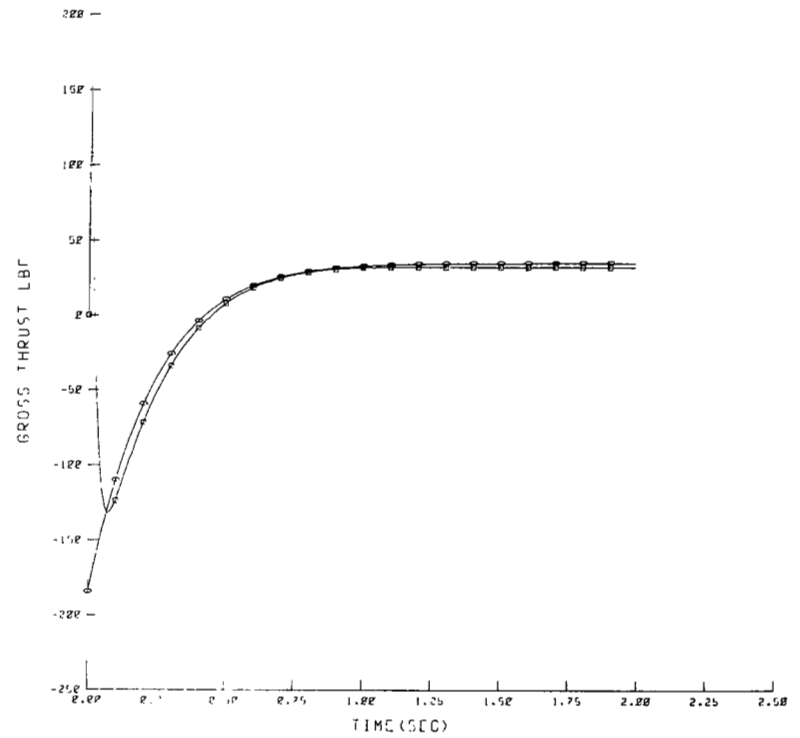


(a-2) With 3-percent step change in nozzle area.

(a) Comparison of full-order linear and nonlinear runs.



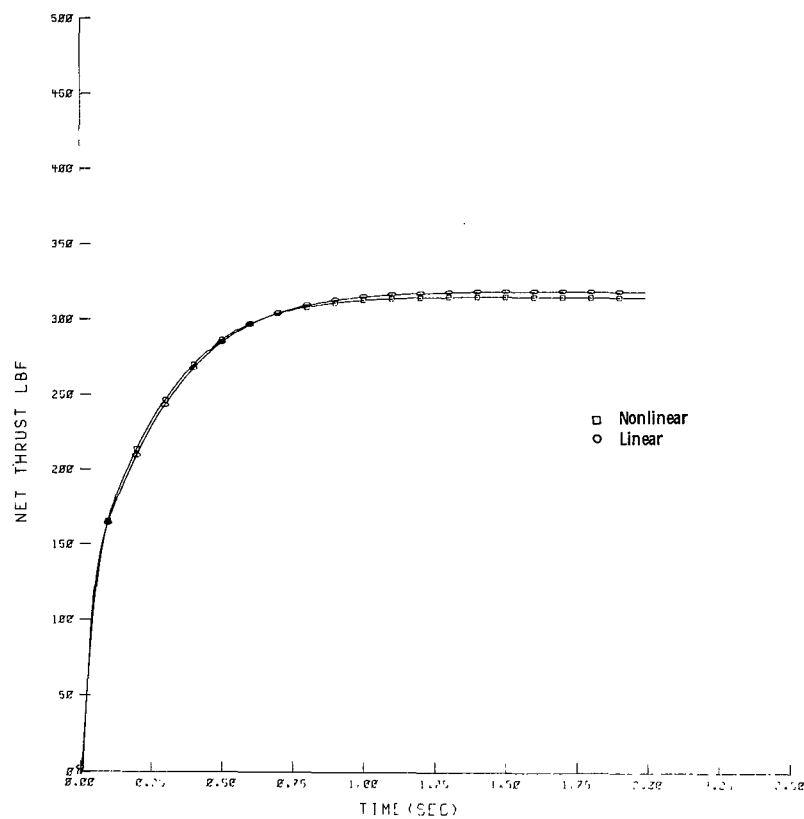
(b-1) With 3-percent step change in main fuel flow.



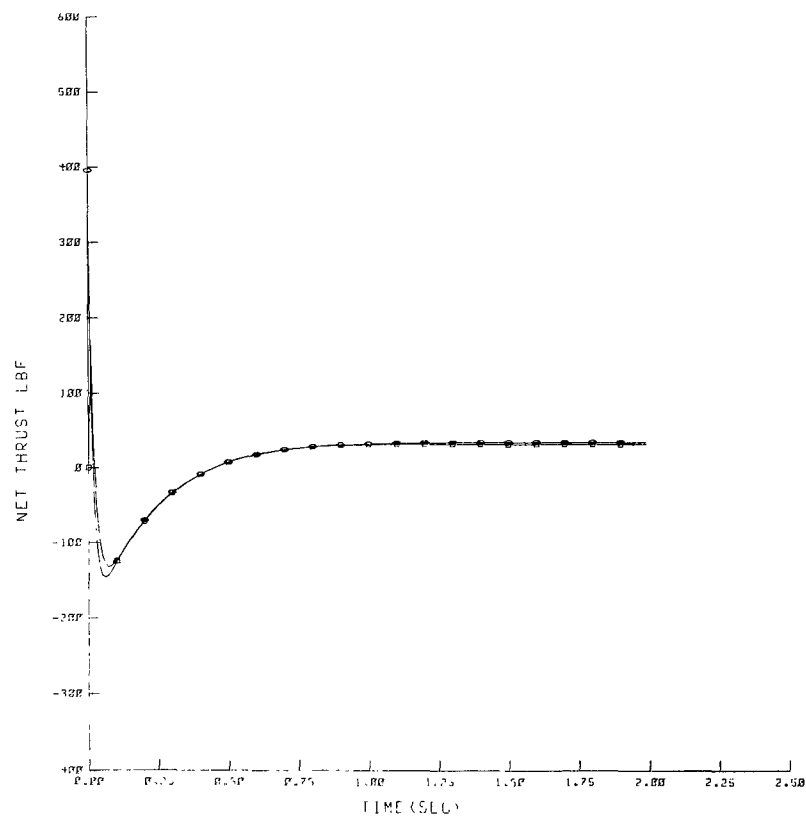
(b-2) With 3-percent step change in nozzle area.

(b) Comparison of reduced-order linear and nonlinear runs.

Figure 18. - Response of output 2 - gross thrust.

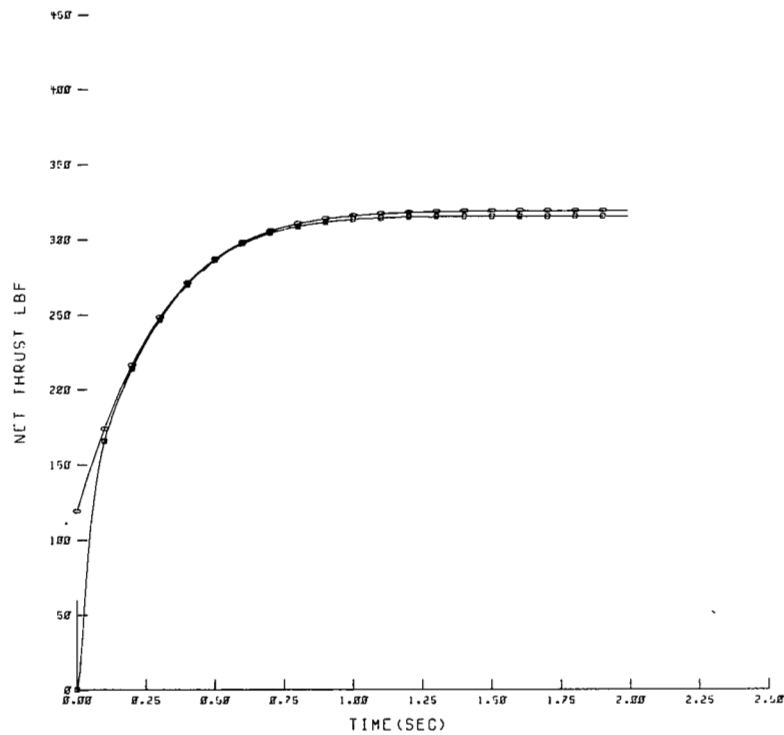


(a-1) With 3-percent step change in main fuel flow.

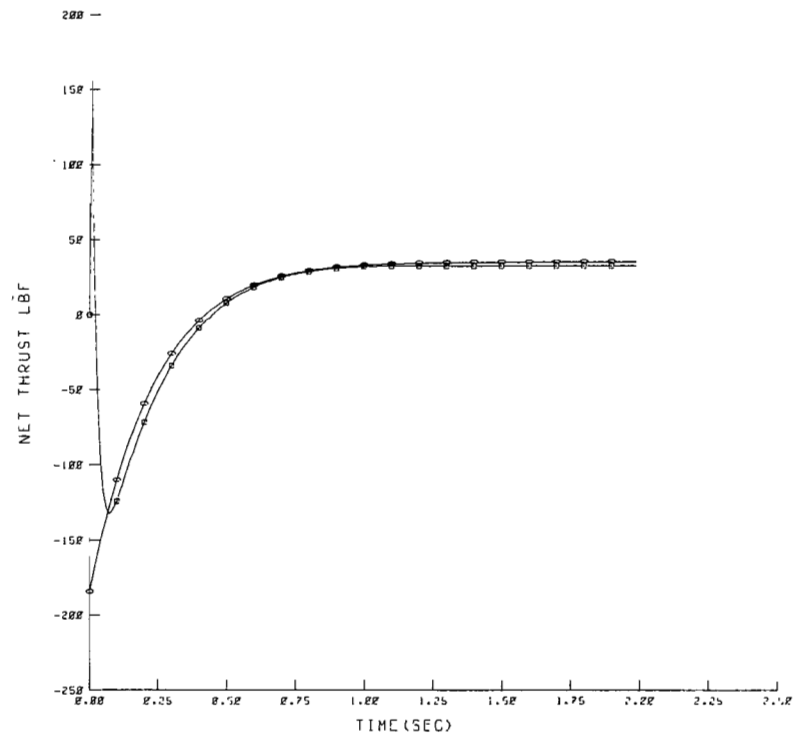


(a-2) With 3-percent step change in nozzle area.

(a) Comparison of full-order linear and nonlinear runs.



(a) With 3-percent step change in main fuel flow.



(b) With 3-percent step change in nozzle area.

(c) Comparison of reduced-order linear and nonlinear runs.

Figure 19. - Response of output 3 - net thrust.

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16. Abstract <p>A digital computer program, DYGABCD, has been developed that will generate linearized, dynamic models of simulated turbofan and turbojet engines. DYGABCD is based on an earlier computer program, DYNGEN, that is capable of calculating simulated nonlinear steady-state and transient performance of one- and two-spool turbojet engines or two- and three-spool turbofan engines. Most control design techniques require linear system descriptions. For multiple-input/multiple-output systems such as turbine engines, state space matrix descriptions of the system are often desirable. DYGABCD computes the state space matrices - commonly referred to as the A, B, C, and D matrices - required for a linear system description. The report discusses the analytical approach and provides a users manual, FORTRAN listings, and a sample case. NASA TN D-7901, describing DYNGEN, is a necessary adjunct to this report.</p>			
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